# Measurements of Sap Flow by the Heat-Pulse Method.

An Instruction Manual for the HPV system

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## **Summary**

Heat-pulse techniques can be used to measure sap flow in plant stems with minimal disruption to the sap stream (Swanson and Whitfield, 1981; Cohen et al., 1981; Green and Clothier, 1988). The measurements are reliable, use inexpensive technology, provide a good time resolution of sap flow, and they are well-suited to automatic data collection and storage. Sequential or simultaneous measurements on numerous trees are possible, permitting the estimation of transpiration from whole stands of trees.

The HPV system described here is based on the 'compensation' Heat-Pulse method (Swanson and Whitfield, 1981) and comprises a set of probes and associated electronics connected to a data logger (model CR10, Campbell Scientific Inc., Utah, USA). Included with the system is a set of computer programs to CAPTURE and ANALYZE the heat-pulse measurements, which are recorded automatically by the data logger. The purpose of this document is to describe how to successfully install and operate the HPV system.

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## 1. Background and Theory

### **1.1 The Origin of Heat-pulse**

Heat-pulse methods date back some 60 years to the work of Huber (1932) who first conceived the idea of using heat as a tracer of sap flow. In his early experiments on tropical liana, Huber found such high rates of sap flow that when heat was applied for one to two seconds it was still recognizable as a pulse at the junctions of a thermocouple sensor some 30 cm downstream from the heater. The time for the first appearance of heat at the sensor was assumed to be the same as the time taken for the sap to move this distance. However in later work, at slower sap speeds, Huber recognized the importance of distinguishing between the effect of convection by the moving sap and the transport of heat by thermal conduction. To separate these two effects, Huber and Schmidt (1937) developed an early version of the 'compensation' heat-pulse method in which one sensor was downstream and the other sensor was upstream of the heater. The time of peak warming of the upstream sensor compared to the downstream one, was used to 'compensate' for the effects of thermal conduction. In both cases the sensor and the heater were external to or just under the bark on the surface of the sapwood and it was assumed that the speed of the sap was identical with that of the heat pulse.

#### **1.2 Idealized Heat-pulse Theory**

Later work by Marshall (1958) developed a theoretical foundation for the heat-pulse technique and showed that Huber's assumptions were not well founded. From a theoretical viewpoint, Marshall showed that the speed of sap is not the same as that of the heat pulse. Rather, the heat pulse velocity is equal to the weighted average of the velocity of the moving sap and the stationary woody matrix, the weighting factor being determined largely by the physical properties of the woody matrix. Marshall (1958) also proposed a new probe arrangement. He advocated the use of a line heater and temperature probe to

be inserted radially into the plant stem, with the temperature being measured at a point far enough below the surface of the stem to avoid the unknown losses of heat which had previously reduced the usefulness of Huber's method. Marshall's (1958) work was based on an analytical solution to the idealized heat flow equation. He used this theory to calculate the temperature rise at any point in the sapwood following the application of an instantaneous line source of heat. Thus, Marshall's contribution was an important first step in establishing a sound theoretical basis for the heat-pulse method.

Swanson (1962) was one of the first to utilize Marshall's analytical solutions, by applying them to the analysis of the 'compensation' heat pulse method in which two temperature sensors are placed asymmetrically either side of a line heater source (Fig. 1). Swanson showed that if the temperature rise following the release of a pulse of heat is measured at distances  $X_u$  [m] upstream and  $X_d$  [m] downstream from the heater, then the heat-pulse velocity can be calculated from

$$V = \left(\frac{X_{\rm d} + X_{\rm u}}{2 t_{\rm z}}\right) \tag{1}$$

where  $t_z$  [s] is the time delay for the temperatures at points  $X_d$  and  $X_u$  to become equal. In effect, Eq. (1) implies that following the application of an instantaneous heat-pulse, the centre of the heat-pulse is convected downstream, from the heater, to reach the point midway between the two temperature sensor after a  $t_z$ . Equation (1) is particularly well suited to data logging since it only requires electronics to detect a null temperature difference and an accurate timer to measure  $t_z$ . The  $t_z$ 's are the only data that need to be recorded, since the distances  $X_u$  and  $X_d$  remain constant. We refer to this estimate of V [m s<sup>-1</sup>] as the 'raw' heat-pulse velocity.

#### **1.3 Wound Corrections to the Heat-Pulse Velocity**

The calculation of V from Eq (1) is based on Marshall's (1958) idealized theory and assumes the heat-pulse probes have no effect on the measured heat flow. In reality, convection of the heat pulse is perturbed by the presence of the heater and temperature



*Figure 1.* Arrangement of sensors within a plant stem for the compensation heatpulse method.

probes, and by the disruption of xylem tissue associated with their placement. These perturbations produce a systematic underestimation in the measured heat-pulse velocity (Cohen et al., 1981; Green and Clothier, 1988). Consequently, the heat-pulse velocity must be corrected for the probe-induced effects of wounding. This correction can be done empirically (e.g. Cohen et al., 1981), or it can be based on sound physical principals, using an equation of the form:

$$V_c = a + bV + cV^2 \tag{2}$$

where  $V_c$  [m s<sup>-1</sup>] is the corrected heat-pulse velocity and V is the raw heat-pulse velocity given by Eq. (1). The correction coefficients *a*, *b*, and *c* have been derived by Swanson and Whitfield (1981) from numerical solutions of Marshall's (1958) equations, for various wound sizes. The full range of correction factors are listed in Table 1. These correction factors can also be seen in the ANALYSIS program, HPV-2000.FOR, which is described later. The use of Eq. (2) puts the heat-pulse method on a sound theoretical basis, and uses physical principals rather than an empirical calibration to obtain the best estimate of the heat-pulse velocity.

Wound	а	b	С
width (mm)			
0.0	0.000	1.000	0.000
1.6	0.393	1.356	0.036
2.0	0.807	1.203	0.058
2.4	1.184	1.072	0.087
2.8	1.524	0.964	0.124
3.2	1.826	0.879	0.169
3.6	2.090	0.818	0.221

 Table 1. Wound corrections for Eq. (2)(From Swanson and Whitfield, 1981)

At this point, we note that *a priori* the wound size is not known, although we might expect it to be a little larger than the size of the drill hole. This is because of additional damage which results from mechanical disruption of vessels at the edges of the drill hole. Anatomical investigations by Barrett et al. (1995) indicated the total wound width is likely to extend about 0.3 mm either side of the drill hole. Thus, a wound correction of  $(1.8 + 2 \times 0.3)$  mm seems appropriate for a drill hole of 1.8 mm (as used here). We have used this wound width to successfully validate the heat-pulse method in apple, but found a larger wound correction of some 3.2 mm was required for kiwifruit vines to bring the heat-pulse measurement into line with actual flow rates (Green and Clothier, 1988). Kiwifruit have very large xylem vessels and a substantial interstitial area of woody matrix which affects the thermal homogeneity of the sapwood and, therefore, affects the transmission and measurement of heat-pulse in kiwifruit. Our results (Green and Clothier, 1988) and the results of Barrett et al. (1995) show the importance of validating the heatpulse method in order to determine the appropriate wound factor. Such a validation is useful, and sometimes necessary, in order to reach a good level of competence and confidence in using the heat-pulse method.

We also issue a practical warning: if due care is not taken to align the centers of the drill holes with the longitudinal direction of the sap flow, then the actual wound width could well be higher than expected. In practice, we believe the 2.4 mm wound correction to be the lower limit appropriate for probes of 1.8 mm diameter. We also stress the importance of **being careful** when placing sensors in the tree stem since the calculations of total sap flow are very sensitive to the wound factor.

A final point on the wound corrections: if the probes are left in place for an extended period, e.g. many months, then the initial wounding may be expected to increase. This is because of increased blockage due to tylose formation in the vessels close to the probes, which may occur as the tree reacts to further isolate the 'wound'. An increased wound reaction could reduce the sensitivity of the sap flow measurements. However, we have never experienced a significant decrease in the heat-pulse sensitivity over time, in either apple or kiwifruit, and so we have been able to use the same set of probes for periods of up to 3 months. In other species this may not be the case and then some reasoned assessment, or independent measure of transpiration, should be made to determine just how long the probes remain useful.

#### 1.4 Converting Heat-Pulse Velocity to Sapflow

Once the corrected heat-pulse velocity,  $V_c$ , has been determined, the next step is to relate it to the actual sap flow. Marshall's (1958) analysis showed that if the sap and woody matrix are considered to form a homogeneous medium, then the sap flux density, J [m s<sup>-1</sup>], can be calculated from

$$J = P(0.33 + M)V_c$$
 (3)

where P [kg m<sup>-3</sup>] is the wood density (oven dry weight of wood/green volume) and M is the moisture content ((wet weight - oven dry weight)/oven dry weight) of sapwood. The density and moisture content of the sapwood are both physical properties of the woody matrix, and they can be determined easily from trunk cores. The factor 0.33 in Eq (3) is the specific heat of dry wood, which is assumed to be constant. In our analysis, we use an alternative expression for J, which was developed by Edwards and Warrick (1984) by considering the sapwood to comprise 3 phases of gas, solid and liquid with appropriate physical and thermal properties. The working equation is given by

$$J = (0.505 F_M + F_L) V_c$$
 (4)

where  $F_{\rm M}$  and  $F_{\rm L}$  are the volume fractions of wood and water, respectively. The factor 0.505 is related to the thermal properties of the woody matrix, and is assumed to be constant within and between species.

### **<u>1.5.</u>** Measuring the Volume fractions, *F*<sub>M</sub> and *F*<sub>L</sub>

Volume fractions  $F_{\rm M}$  and  $F_{\rm L}$  implicit in Eq. (4) are determined from the Archimede's principle, in the following manner. Firstly, a core sample is taken and its fresh weight,  $M_{\rm F}$  [kg], is determined. This weight is equal to the mass of water and the mass of dry wood,

since the mass of air is negligible. The core sample is then immediately submerged in a beaker of water which has been placed on an accurate mass balance. The balance reading will indicate an immediate increase in mass, which equals the displacement of water,  $D_T$  [kg]. The total volume,  $V_T$  [m<sup>3</sup>], of the sample is then equal to  $\rho_L$  times  $D_T$ , where the density of water,  $\rho_L$ , is assumed to be 1000 kg m<sup>3</sup>. The core sample is then oven-dried to determine the mass of dry wood,  $M_D$  [kg]. The difference between the fresh weight and the dry weight, ( $M_F$ - $M_D$ ) is equal to the mass of water,  $M_L$  [kg], contained in the fresh core sample. Thus, the volume fraction of water is  $F_L = M_L/(\rho_L V_T)$ . Similarly, the volume fraction of wood  $F_M = M_D/(\rho_M V_T)$  where the density of dry wood,  $\rho_M$  equals 1530 kg m<sup>3</sup>.

#### **1.6.** Estimating Volumetric Sapflow

Equation (4) provides an estimate of the values of J at any point in the conducting sapwood. It is widely recognized that sap flux density is not uniform throughout the sapwood, but rather peaks at a depth of 10 - 20 mm in from the cambium. Consequently, sampling at several depths in the sapwood is necessary to characterize the sapflow velocity profile (Cohen et al., 1981; Edwards and Warrick, 1984; Green and Clothier, 1988). A volumetric measure of total sap flux can be obtained by the integration of these point estimates over the sapwood conducting area. The most common approach is to fit a least-squares polynomial to the depthwise estimates of sap flux density, and then to integrate the fitted function over the sapwood cross section. This is the approach that we favour. An alternative, simpler integration method, as presented by Hatton et al. (1990), is based on a weighted average approach. According to Hatton et al. this simpler approach is a more robust estimator of the volume flux when the velocity profiles exhibit large curvature.

In the ANALYSIS program described later we use the most common approach to calculate volume sap flow. Since our probes measure J at four radial depths, we fit a second-order regression of the form

$$J(r) = \alpha r^2 + \beta r + \gamma \tag{5}$$

in order to get the expression for the velocity profile as a function of stem radius, r [m]. This curve is then integrated over the sapwood cross-section to calculate the volume sap flux, Q, as

$$Q = \int_{H}^{R} 2\pi r J(r) dr$$
(6)

for a stem of cambium radius R [m] and heartwood radius H [m].The stem parameter H needs to be determined from an analysis of trunk cores taken at the end of the experiment while R can be derived from the stem circumference and an allowance for the depth of the bark.

## 2. Instrumentation

The HPV system described here is based on the 'compensation' Heat-Pulse method (Marshall, 1958; Swanson and Whitfield, 1981) and comprises a set of probes and associated electronics connected to a data logger (model CR10, CR21X or CR23X, Campbell Scientific Inc., Utah, USA). Each set of probes comprises a linear heater and two temperature sensors which are installed radially into the tree stem, as shown in Fig. 1. The heater probe is made from a length of 19 swg stainless steel tube, containing a central nichrome resistance wire (5  $\Omega$  m<sup>-1</sup>) which is insulated inside a fine Teflon tube. The temperature sensors each comprise four copper-constantan thermo-couple junctions (42 swg) and are made from a length of Teflon tubing (18 swg) which is filled with epoxy resin. The electronics consists of a heater controller and a set of linear instrumentation amplifiers which have a gain of about 5000. The simple heat-pulse controllers do not have any amplifiers.

A data logger (Campbell Scientific Inc., Logan, Utah) is used to activate the heater, for 0.5 to 1 s, in order to introduce a heat-pulse tracer into the moving sap stream. A pair of temperature sensors are used to monitor subsequent changes in stem temperature which occur as the heat-pulse is propagated through the sapwood, both by conduction through the wood and sap matrix and by convection with the moving sap streams. Typically,

output signals from the HPV unit should lie between  $\pm 40 \text{ mV}$  for the 1°C difference in temperature difference between the two sensors. The data logger is programmed to interpret the temperature signals and to record the subsequent 'cross-over' times which are used in Eq. (1) to calculate the raw heat-pulse velocity at a single point (depth) in the conducting sapwood. A laptop PC is later used to retrieve the  $t_z$  data from the logger and to calculate total sap flow in the tree stem, as described by Eqs. (4) - (6).

## 3. Connecting up the logger and getting it going.

This section refers to installation and operation of the the HPV units. The wiring and operation of the simple heat-pulse controller (no amplifiers) is described in Appendix B.

#### 3.1 Assembling the necessary hardware.

The following is a list of hardware needed to run the HPV unit.

3.1.1. You will need 2 sets of:

.. heat pulse probes (white ones with grey connectors)
.. heat pulse cables (white ones with silver connectors)
and 1 set of:
.. heat pulse unit with power lead
.. suite of heat pulse programs to capture and analyze the heat-pulse data

The above items are supplied with your installation.

#### 3.1.2. You will also need:

.. Campbell Datalogger (CR10X, CR21X or CR23X)

- .. external 12V (>70 AHr) battery
- .. Laptop with SC32 interface and Campbell Software (PC208W)

These items are not supplied with your installation.

#### **3.2.** Connecting the HPV unit to the data logger:

There are two leads which must to be connected to the HPV unit - a signal lead and a power lead. The pin-out of these leads is listed below.

Signal lead: This lead has 7 coloured wires which must be connected as follows:

orange	=	1H or 3H or 5H	(analog input)
orange/white	=	1L or 3L or 5L	"
blue	=	2H or 4H or 6H	"
blue/white	=	2L or 4L or 6L	"
green	=	AG	(analog ground)
green/white	=	C1 or C2 or C3	(control line)
white	=	AG or GND	(cable shield)

Power lead: This lead has 2 coloured wires which must be connected as follows:

black = GRND red = +12V

**IMPORTANT:** The black and red wires go to the POWER on the heat-pulse unit. A separate battery should be used for the logger. ALWAYS connect the red wire first, to avoid shorting out the logger. Also, be careful that you don't plug the wrong cable into the heat-pulse unit, since this may short-out the HPV unit or the logger (It hasn't happened yet, but that's little consol ation for when it does!!!). As a precaution, there is a diode inside the heat-pulse unit to protect it against reverse-polarity.

**VERY IMPORTANT:** If the same battery powers the logger and the heat-pulse unit then <u>do not</u> connect the green wire of the signal lead to AG. This would cause a ground loop and might affect the results...

## 4. Installing the heat-pulse probes.

This section gives advice on how to install the heat-pulse probes into a plant stem. Note: It is good practice to test the operation of the logger and the probes, and to test all the wiring connections before inserting the probes into the plant stem. Although the HPV unit is designed to be operated automatically, the software does allow for a manual test of the system, as described later in the next section.

#### 4.1. Checking if probes are OK

The pin-out for the connector on the temperature probes (the 9-pin D-plug) is:

n centre)
[

Each temperature sensors should be electrically isolated. A quick 'beep-test' of the temperature sensors using a multi-meter should confirm each thermocouple is connected, and isolated from the others. The temperature probes should have a resistance of about 19 ohms. The heater probe normally has a resistance of about 0.4-0.6 ohms. If the heater is faulty then this resistance will exceed this value.

#### 4.2. Procedure for installing probes.

- 4.2.1. Locate a fairly straight piece of stem, fairly free of bumps and knots. Measure the stem circumference, C, to the nearest mm.
- 4.2.2. Attach the drilling jig as shown below. Use thick stickytape for the stem, or use a special jig for roots and small branches.



4.2.3. Carefully drill the holes using a high-speed, electric drill.

- Don't drill too far at once (say more than 20mm) because this can ' ovebore' the hole. Make sure the hole is about 20 mm deeper than the longest probe.
- Remove the jig and ' plug' the holes with Vaseline.
- Take a ' cork bore' around the two outer holes so you can measure the bark depth, D (mm), *e.g.* with a set of calipers.

insert:

- Dip each probe in Vaseline, and then insert it CAREFULLY into the appropriate hole. The probe marked with the red dot goes closest to the heater. Insert the heater last.
- Tape the probes CAREFULLY to the tree stem, but don't bend them to far!!
- Check each probe to make sure its OK (see 4.1)

IF its OK THEN

• connect it to the logger.

ELSE

- get some new probes
- goto insert

ENDIF

## 4.3. Testing if everything is working.

Make sure the HPV system is properly connected (see 3.2 above) Make sure the logger is properly programmed (see 5 below) Fire a test pulse (see 5 below)

IF it seems to be OK THEN go for a beer

ELSE swear a lot blame someone else (but not me) goto deep\_shit ENDIF

Note1: if you cant find deep\_shit, then your not in it. Note2: There is no deep\_shit. I expect that every thing will work Note3: Murphy's Law suggests there will be some other problem to find.

## 5. Installing the data-logger software

The following program is to be run on a Campbell data logger. The logger software is located in one of the three sub-directories on the disk provided with the installation.

## 5.1. Files in A:\LOGGER

C10-HP*.STN	C21-HP*.STN
C10-HP*.DLD	C21-HP*.DLD
C10-HP*.CSI	C21-HP*.CSI

This sub-directory contains the above CAPTURE programs designed to measure the outputs generated by the HPV unit, and to calculate and store the  $t_Z$  values associated with each set of the probes. The program is rather basic (in keeping with our philosophy). It is intended to be run on a Campbell logger (CR10, CR21X or CR23X). A CR10 will measure up to three sets of probes and a CR21X will measure up to four sets of probes, a CR23X will measure up to 6 sets of probes. The whild-card '\*' in the file name implies the number of probes that will be measured.

Note: A single logger can up to 6 sets of probes. It is a simple matter to extend the total number of probes by using a Campbell AM25T solid state multiplexer, to switch the output from many more probes. This requires a slightly modified version of the CAPTURE program to include use of the multiplexer and to allocate the extra channels on the logger. If the USER wishes to consider either of these modifications then examples of the necessary programs can be supplied, via email, at a later date. Details are in Appendix A.

In what follows, we assume the USER is familiar with the various functions of the CR10 data logger, and the Campbell programs included with the PC208 software (GraphTerm and EDLOG).

The following files have been supplied in the sub-directory A:\LOGGER of the installation disk:

CR10-HP3.STN is the Station file required to communicate with the logger. CR10-HP3.DLD is a file to be ' downloaded' to the logger, via the GT program. CR10-HP3.CSI is a file created by the program editor, EDLOG.

The program CR10-HP3.DLD should be downloaded to the logger using the GT program (see Campbell PC208 manual for instructions on how to do this).

## 5.3. Down-loading programs to the logger

There are two ways to enter the CAPTURE program into the data logger - via the key pad or by using the PC208 software as supplied by Campbell Sci. The latter is the preferred option since GT can also be used to download program, and retrieve data, in the usual manner.

NOTE. to get the logger-prompt ' >' via GT, enter 2718H at the ' \*' prompt. You can now talk to the logger via the PC, or exit GT and talk to the logger via the keypad. Special ' modes' for the logger are \*1, \*5, \*6, and \*7, as explained below. Remember, CTRL\_ gets you back to the options menu. !!!!!

## 5.4. Review of the logger modes

For a full description of the logger modes, the USER should consult a Campbell datalogger manual. The following is some basic information that may help you to interpret the logger functions.

\*1 mode is used to enter and/or alter a program (Table-1) that resides in the memory of the logger. Enter ' \*1 X A' to view instruction no. x in Table 1.

**\*5 mode** is used to set the clock. **!!!** Most important to do this before the heat-pulse program is run. Expect the following responses:

Enter' \*5 A YY A DOY A HRMIN A' to set the year, day-year and current time in hours and minutes.

Note: PC208 can also be used to download the PC time to the logger (the preferred option).

\*6 mode is used to view and set the ' flags' as well as the input value

**\*7 mode** is used to examine output memory. Enter \*7 to see memory pointer to the next location in output memory (say 740). Enter \*7 X to see data stored at location X (say 740).

## 5.5. Retrieving data from the logger

Use the program PC208 to retrieve all the 'uncollected' data from the data logger.

## 5.6. Operation of the logger program - C10-HP3.DLD

Here we describe a number of program changes and system tests that you may want to do. We also describe some ' normal' program behaviour that may be expected during the course of a measurement period. Note: After you have finished playing with the logger, ALWAYS press \*0 to recompile any changes, or to continue by leaving the logger in the ' LOG1' mode.

5.6.1. To change the interval between heat pulses (alter Inst-1)

enter \*1 1 A A A x A \*0 where x = interval in minutes The default time is 30 minutes

5.6.2. To fire a test heat-pulse

enter \*6 A D 1 (the lights should go on, and the program will run) enter \*6 A D 6 for an early exit of program enter \*0 to continue

5.6.3. To check if the system is working properly (generally a good idea!)

fire a test heat pulse (see 5.6.2) check the initial voltages (+/- 20 mV is OK, -9999 is stuffed) i.e. enter \*6 x A where x = 41..56 check the present voltages (+/- 100 mV is OK, -9999 is stuffed) i.e. enter \*6 x A where x = 21..36 enter \*0 to continue

Note. Readings are in mV so anything in the range +/- 200 is OK.

5.6.4. To examine  $t_z$  data (stored in locations 1..16)

enter \*6 x A where x is the location. loc. 1 = tz1-1 (outer) .... loc. 4 = tz1-4 (inner) loc. 5 = tz2-1 (outer) .... loc. 8 = tz2-4 (inner) loc. 9 = tz3-1 (outer) .... loc. 12 = tz3-4 (inner) loc. 13 = tz4-1 (outer) .... loc. 16 = tz4-4 (inner) enter \*0 to continue 5.6.5. To find out the total running-time since the heat-pulse was fired (loc. 99)

enter \*6 99 A enter \*0 to continue

5.6.6. To change the duration of the heat pulse (alter Inst-44)

enter \*1 44 A A A X A \*0 where x is duration in s default value is 2.0 s (this is also the maximum time)

5.6.7. To change the delay between firing a heat pulse and testing for a ' crossover' . This may be necessary for really fast flows (alter Inst-49)

enter \*1 49 A A A x A \*0 where x is delay in multiples of 0.1s default value is 15 s, i.e. x=150

5.6.8. To change the maximum time for a  $t_z$  calculation (alter Inst-14) enter \*1 14 A A A x A where x is max time in multiples of 0.1s default value if 500 s, i.e. x=500, but 300s might be OK

## 5.7. Listing of the logger program - C10-HP3.CSI

This section gives a listing of the CAPTURE program designed to measure the outputs generated by the HPV unit, and to calculate and store the  $t_z$ 's associated with each set of the probes. The program is rather basic (in keeping with our philosophy). It is located in the subdirectory A:\LOGGER on the installation disk provided. This programme was compiled using the latest version of EDLOG. As a result, the program may not install and run properly if the old version of EDLOG and GT is used. However, if any problems do occur then it is a simple matter to enter the following program by hand, via the keypad, and subsequently retrieve it back using the GT (or TERM) program.

# Note: For the program to run, the USER needs to enter the \*A mode and reset the number of final output locations to 100.

;{CR10}		
*Table 1	Program	
01: 0.25	Execution Interval (seconds)	
1: If time	e is (P92)	Flag 1 is used to activate automatic sampling
1:0	Minutes (Seconds) into a	once every 30 mins.
2: <b>30</b>	Interval (same units as above)	Change as required
3: 11	Set Flag 1 High	
2: If Flag	g/Port (P91)	<b>Flag 5</b> is set when $t_z$ is calculated
1:15	Do if Flag 5 is High	
2:30	Then Do	
3: Timer	· (P26)	store current time in loc (99)

1:99 Loc [ \_\_\_\_\_ ] 4: Volts (SE) (P1) Measure current temp. signal and store in loc (21..32) Reps Change as required 1: **12** 2:14 ñ 250 mV Fast Range 3:1 SE Channel 4:21 Monitor loc (21..32) to observe temperature trace Loc [ \_\_\_\_\_ ] 5:1 Mult 6: 0 Offset 5: Beginning of Loop (P87) Check for cross-over times Delay 1:0 2:12 Loop Count Change as required 6: IF (X<=>F) (P89) 1:1 -- X Loc [\_\_\_\_] tz's are stored in loc (1..12)2:1= 3:0 F 4:30 Then Do 7: IF (X<=>Y) (P88) test for a temperature 'cross over' 1: 41 -- X Loc [\_\_\_\_] initial temperature signal in loc (41..52) 2:3 >= 3: 21 -- Y Loc [\_\_\_\_\_] current temperature signal in loc (21..32)4:30 Then Do If crossed over then 8: Z=X (P31) 1: 99 X Loc [ \_\_\_\_\_ ] 2: 1 -- Z Loc [ \_\_\_\_\_ ] store tz in loc (1..12)9: Z=Z+1 (P32) inc a 'tz' counter 1:90 Z Loc [\_\_\_\_\_] 10: End (P95) 11: End (P95) 12: End (P95) 13: IF (X<=>F) (P89) If all 12 channels have crossed over then X Loc [ \_\_\_\_\_ ] 1:90 set Flag 6 2:3 >= 3: **12** F Change as required 4:16 Set Flag 6 High 14: IF (X<=>F) (P89) If more than 500 s have elapsed then 1:99 X Loc [\_\_\_\_\_] set flag 6 2:3 >= 3: 500 F Change as required 4:16 Set Flag 6 High 15: End (P95) 16: If Flag/Port (P91) If Flag 6 is set then Do if Flag 6 is High 1:16 output all the data

2:30 Then Do 17: Do (P86) Set Output Flag High 1:10 18: Sample (P70) Ouput the date and time 1:2 Reps 2:91 Loc [ \_\_\_\_\_ ] 19: Sample (P70) Output the 12 tz values 1:12 Reps Change as required 2:1 Loc [ \_\_\_\_\_ ] 20: Do (P86) Set Flag 6 Low 1:26 21: Do (P86) 1:25 Set Flag 5 Low 22: End (P95) 23: If Flag/Port (P91) If Flag 1 is set then 1:11 Do if Flag 1 is High Initialise and reset arrays 2:30 Then Do 24: Time (P18) Store Day of Year in loc (91) 1:2 Hours into current year (maximum 8748) 2: 8784 Mod/By 3: 91 Loc [ \_\_\_\_\_ ] 25: Z=X\*F (P37) 1: 91 X Loc [\_\_\_\_\_] 2:.04167 F 3: 91 Z Loc [ \_\_\_\_\_ ] 26: Z=INT(X) (P45) X Loc [ \_\_\_\_\_ ] Z Loc [ \_\_\_\_\_ ] 1:91 2:91 27: Z=Z+1 (P32) 1:91 Z Loc [\_\_\_\_\_] 28: Time (P18) Store time (hrmin ) in loc (92) 1:2 Hours into current year (maximum 8748) 2:24 Mod/By 3: 92 Loc [ \_\_\_\_\_ ] 29: Z=X\*F (P37) X Loc [\_\_\_\_\_] 1:92 2:100 F 3: 92 Z Loc [\_\_\_\_\_] 30: Time (P18) 1:1 Minutes into current day (maximum 1440)

2:60 Mod/By Loc [\_\_\_\_\_] 3:93 31: Z=X+Y (P33) X Loc [ \_\_\_\_\_ ] 1:92 Y Loc [ \_\_\_\_\_ ] 2:93 3: 92 Z Loc [ \_\_\_\_\_ ] 32: Beginning of Loop (P87) Reset all storage arrays 1:0Delay Loop Count 2:90 33: Z=F (P30) 1:0 F 2:0 Exponent of 10 3: 1 -- Z Loc [\_\_\_\_] 34: End (P95) 35: Volts (SE) (P1) Measure initial temp signal and store in loc (41..52) Change as required 1: **12** Reps 2:4 ñ 250 mV Slow Range SE Channel 3:1 Loc [ \_\_\_\_\_ ] 4:41 Monitor loc (41..52) to observe initial temp signal 5:1 Mult Offset 6:0 36: Timer (P26) Reset timer Loc [ \_\_\_\_\_ ] 1:037: Do (P86) 1:21 Set Flag 1 Low 38: Do (P86) 1:12 Set Flag 2 High 39: End (P95) 40: If Flag/Port (P91) Flag 2 is used to initiate the heat-pulse 1:12 Do if Flag 2 is High 2:30 Then Do 41: Set Port(s) (P20) 1:0 C8..C5 = 0/0/0/02: 111 C4..C1 = 0/high/high/high 42: Beginning of Loop (P87) 1:1 Delay 2:0Loop Count 43: Timer (P26) Loc [ \_\_\_\_\_ ] 1:99 44: IF (X<=>F) (P89) Fire a 2 s heat pulse X Loc [ \_\_\_\_\_ ] 1:99

2:3 >= 3: 2 F Change as required 4:31 Exit Loop if True 45: End (P95) 46: Set Port(s) (P20) 1:0 C8..C5 = 0/0/0/02:0C4..C1 = 0/0/0/047: Beginning of Loop (P87) 1:1 Delay 2:0Loop Count 48: Timer (P26) Loc [ \_\_\_\_\_ ] 1:99 49: IF (X<=>F) (P89) Wait 15 s before sampling for cross overs X Loc [ \_\_\_\_\_ ] 1:99 2:3 >= 3: 15 Change as required F 4:15 Set Flag 5 High 50: If Flag/Port (P91) Do if Flag 5 is High 1:15 2:31 Exit Loop if True 51: End (P95) 52: Do (P86) 1:22Set Flag 2 Low 53: End (P95) 54: Batt Voltage (P10) Store battery voltage in loc (98) 1:98 Loc [ \_\_\_\_\_ ]

#### End Program

## 5.8. Operation of the logger program - C21-HP4.DLD

Here we describe the HPV program for a CR21X logger and the normal tests that you may want to do. We also describe some ' normal' program behaviour that may be exped during the course of a measurement period. Note: After you have finished playing with the logger, ALWAYS press \*0 to recompile any changes, or to continue by leaving the logger in the ' LOG1' mode.

5.8.1. To change the interval between heat pulses (alter Inst-1)

enter \*1 1 A A A x A \*0 where x = interval in minutes

The default time is 30 minutes

5.8.2. To fire a test heat-pulse

enter \*6 A D 1 (the lights should go on, and the program will run) enter \*6 A D 6 for an early exit of program enter \*0 to continue

5.8.3. To check if the system is working properly (generally a good idea!)

fire a test heat pulse (see 5.8.2) check the initial voltages (+/- 20 mV is OK, -9999 is stuffed) i.e. enter \*6 x A where x = 41..56check the present voltages (+/- 100 mV is OK, -9999 is stuffed) i.e. enter \*6 x A where x = 21..36enter \*0 to continue

Note. Readings are in mV so anything in the range +/- 200 is OK.

5.8.4. To examine  $t_z$  data (stored in locations 1..16)

enter \*6 x A where x is the location. loc. 1 = tz1-1 (outer) .... loc. 4 = tz1-4 (inner) loc. 5 = tz2-1 (outer) .... loc. 8 = tz2-4 (inner) loc. 9 = tz3-1 (outer) .... loc. 12 = tz3-4 (inner) loc. 13 = tz4-1 (outer) .... loc. 16 = tz4-4 (inner) enter \*0 to continue

5.8.5. To find out the total running-time since the heat-pulse was fired (loc. 99)

enter \*6 99 A enter \*0 to continue

5.8.6. To change the duration of the heat pulse (alter Inst-48)

enter \*1 48 A A A X A \*0 where x is duration in s default value is 2.0 s (this is also the maximum time)

5.8.7. To change the delay between firing a heat pulse and testing for a ' crossover' . This may be necessary for really fast flows (alter Inst-56)

enter \*1 56 A A A x A \*0 where x is delay in multiples of 0.1s default value is 15 s, i.e. x=150

5.8.8. To change the maximum time for a  $t_z$  calculation (alter Inst-15)

enter \*1 15 A A A x A where x is max time in multiples of 0.1s default value if 500 s, i.e. x=500, but 300s might be OK

### 5.9. Listing of the logger program - C21-HP4.CSI

This section gives a listing of the CAPTURE program designed to measure the outputs generated by the HPV unit, and to calculate and store the  $t_z$ 's associated with each set of the probes. Note: For the program to run on a CR21X, the USER needs to enter the \*A mode and reset the number of final output locations to 100. The programme is similar to C10-HP3.CSI, except for minor changes caused by instructions P20 and P30 which are described in the Campbell data logger manual. Locations where the USER can make changes are written in bold type.

;{21X} 1: 41 -- X Loc [\_\_\_\_] \*Table 1 Program 2:3 >= 01: 0.2000 Execution Interval (seconds) 3: 21 -- Y Loc [\_\_\_\_\_] 4:30 Then Do 1: If time is (P92) 1:0 Minutes into a 8: Z=X (P31) 1: 99 X Loc [ \_\_\_\_\_ ] 2:30 **Minute Interval** Set Flag 1 High 2: 1 -- Z Loc [ \_\_\_\_\_ ] 3:11 2: If Flag/Port (P91) 9: Z=X\*F (P37) 1: 1 -- X Loc [ \_\_\_\_\_ ] 1:15 Do if Flag 5 is High 2:30Then Do 2:0.1 F 3:1 -- Z Loc [\_\_\_\_] 3: Timer (P26) Loc [ ] 1:99 10: Z=Z+1 (P32) 1:90 Z Loc [ \_\_\_\_\_ ] 4: Volts (SE) (P1) 1:16 Reps 11: End (P95) 2:4 ñ 500 mV Slow Range 3:1 SE Channel 12: End (P95) 4:21 Loc [ \_\_\_\_\_ ] 5:1 Mult 13: End (P95) 6:0 Offset 14: IF (X<=>F) (P89) 5: Beginning of Loop (P87) 1:90 X Loc [ \_\_\_\_\_ ] 1:0 Delay 2:3 >= 2:16 **Loop Count** 3:16 F 4:16 Set Flag 6 High 6: IF (X<=>F) (P89) 1: 1 -- X Loc [ \_\_\_\_\_ ] 15: IF (X<=>F) (P89) X Loc [ \_\_\_\_\_ ] 2:1 = 1:99 F 3:0 2:3 >= 4:30 Then Do 3: 5000 F Set Flag 6 High 4:16 7: IF (X<=>Y) (P88)

16: End (P95) 17: If Flag/Port (P91) Do if Flag 6 is High 1:16 2:30 Then Do 18: Do (P86) 1:10 Set Output Flag High 19: Sample (P70) 1:2Reps 2:91 Loc [ \_\_\_\_\_ ] 20: Sample (P70) 1:16 Reps Loc [\_\_\_\_\_] 2:1 21: Do (P86) 1:26 Set Flag 6 Low 22: Do (P86) 1:25 Set Flag 5 Low 23: End (P95) 24: If Flag/Port (P91) 1:11 Do if Flag 1 is High 2:30 Then Do 25: Time (P18) 1:2Hours into current year (max 8748) 2: 8784 Mod/By 3: 91 Loc [ \_\_\_\_\_ ] 26: Z=X\*F (P37) 1: 91 X Loc [ \_\_\_\_\_ ] 2:.04167 F Z Loc [\_\_\_\_\_] 3:91 27: Z=INT(X) (P45) X Loc [ \_\_\_\_\_ ] 1:91 2:91 Z Loc [ \_\_\_\_\_ ] 28: Z=Z+1 (P32) Z Loc [ \_\_\_\_\_ ] 1:91 29: Time (P18) Hours into current year (maximum 1:28748) 2:24 Mod/By Loc [ \_\_\_\_\_ ] 3: 92 30: Z=X\*F (P37) X Loc [ \_\_\_\_\_ ] 1:92 2:100 F

Z Loc [\_\_\_\_] 3: 92 31: Time (P18) Minutes into current day (max 1440) 1:1 2:60 Mod/By 3:93 Loc [ \_\_\_\_\_ ] 32: Z=X+Y (P33) X Loc [ \_\_\_\_\_ ] 1:92 Y Loc [\_\_\_\_\_] Z Loc [\_\_\_\_\_] 2:93 3:92 33: Beginning of Loop (P87) 1:0 Delay 2:90 Loop Count 34: Z=F (P30) 1:0 F 2:1 -- Z Loc [\_\_\_\_] 35: End (P95) 36: Volts (SE) (P1) 1:16 Reps 2:4 ñ 500 mV Slow Range SE Channel 3:1 Loc [ \_\_\_\_\_ ] 4:41 5:1 Mult Offset 6:0 37: Timer (P26) 1:0 Loc [ \_\_\_\_\_ ] 38: Do (P86) Set Flag 1 Low 1:21 39: Do (P86) 1:12 Set Flag 2 High 40: End (P95) 41: If Flag/Port (P91) 1:12 Do if Flag 2 is High 2:30 Then Do 42: Set Port (P20) 1:1 Set High Port Number 2:143: Set Port (P20) Set High 1:1 2:2 Port Number 44: Set Port (P20)

1:1

Set High

2:3 Port Number 45: Set Port (P20) Set High 1:1 2:4 Port Number 46: Beginning of Loop (P87) 1:1 Delay 2:0Loop Count 47: Timer (P26) 1:99 Loc [ \_\_\_\_\_ ] 48: IF (X<=>F) (P89) X Loc [ \_\_\_\_\_ ] 1:99 2:3 >= 3:20 F 4:31 Exit Loop if True 49: End (P95) 50: Set Port (P20) 1:0 Set Low 2:1Port Number 51: Set Port (P20) 1:0 Set Low 2:2 Port Number 52: Set Port (P20) 1:0 Set Low 2:3 Port Number 53: Set Port (P20) Set Low 1:0 2:4 Port Number

54: Beginning of Loop (P87) Delay 1:1 2:0 Loop Count 55: Timer (P26) 1:99 Loc [ \_\_\_\_\_ ] 56: IF (X<=>F) (P89) X Loc [ \_\_\_\_\_ ] 1:99 2:3 >= 3:150 F Set Flag 5 High 4:15 57: If Flag/Port (P91) Do if Flag 5 is High 1:15 2:31 Exit Loop if True 58: End (P95) 59: Do (P86) 1:22 Set Flag 2 Low 60: End (P95) 61: Batt Voltage (P10) 1:98 Loc [ \_\_\_\_\_ ] \*Table 2 Program 01: 0.0000 Execution Interval (seconds) \*Table 3 Subroutines End Program

# 6. Running the ANALYSIS software ... (still under review)

This section describes the software used to analyze the tz data collected by the data loggers. The analysis software is located in one of the four sub-directories on the disk provided with the installation.

## 6.1. Files in A:\FORT

HPV-2000.FOR HPV-2000.EXE HPSAMPLE.DAT HPHEADER.DAT

This subdirectory contains the FORTRAN programs required to analyze the heat-pulse data (HPV-2000.FOR and HPV-2000). This program has been compiled using Digital-Visual FORTRAN Version 5.1, and should run on any PC under Windows 3.1 or higher. The program HPV-2000.EXE can be copied to any sub-directory on a laptop or a PC. But in order to run HPV-2000, the program and the data (e.g. hpsample.dat) should reside in the same directory.

## 6.2. Setting up the input file

The file HPHEADER.DAT is an example of the first few lines which must be at the top of each data file. Because HPV-2000 uses a FORMATTED-read of the input data, it is important to include a header-file at the top of the  $t_z$  data, in exactly the same format as shown below. The header-file sets up the independent parameters involved in the sapflow calculations, e.g. sapwood radius, heartwood radius, the volume fractions of wood and water, etc. If you are familiar with FORTRAN then you can examine the source code (HPV-2000.FOR) to find the formatted read statement.

The process to set up the input data is as follows:

<u>Step - 1.</u>

Each data file should have the following 10+2n lines at the top of the data files (see e.g. HPHEADER.DAT as supplied on disk), where *n* is the number of probes being read. The example below is for n=3 sets of probes and nsensors=4 is the no. of sensors in each probe.

 nprobes:
 3

 nsensors:
 4
 4

 wound\_width:
 2.40
 2.40
 2.40

 Swanson fac:
 1
 v

 v-frac wood:
 0.36
 v
 v

 v-frac wat :
 0.54
 sapwood\_rad:
 6.21
 6.00
 6.00

 hrtwood\_rad:
 0.00
 0.00
 0.00
 0.00
 0.00

prob depth1:	0.50	1.20	2.20	3.50
prob_space1:	1.00	1.00	1.00	1.00
prob depth2:	0.50	1.20	2.20	3.50
prob_space2:	1.00	1.00	1.00	1.00
prob_depth3:	0.50	1.20	2.20	3.50
prob space3:	1.00	1.00	1.00	1.00
Tmin,Tmax :	185.	192.		
Emax values:	5.00	5.00	5.00	

The next example is the header-file required to analyze n=2 sets of probes:

nprobes: 2 nsensors: 4 4 wound\_width: 2.40 2.40 Swanson fac: 1 v-frac wood: 0.36 v-frac wat : 0.54 sapwood rad: 6.21 6.00 hrtwood rad: 0.00 0.00 prob depth1: 0.50 1.20 2.20 3.50 prob\_space1: 1.00 1.00 1.00 1.00 prob\_depth2: 0.50 1.20 2.20 3.50 prob\_space2: 1.00 1.00 1.00 1.00 Tmin,Tmax : 185. 192. Emax values: 5.00 5.00

In the two examples given above, the program is expecting to analyze data beginning on day of year 185 (*Tmin*) through until day of year 192 (*Tmax*). The program will also plot the volume flow rates for each set of probes, assuming the maximum flow, *Emax*, equals  $5.0 \text{ L} \text{ h}^{-1}$ . Swanson's correction factors (Table 1) are used if the parameter equals 1 (an integer). Otherwise, inputting a zero-value means the correction factors of Green and Clothier (1988) will be used. For wide probe spacings we recommend the Green and Clothier factors be used. Otherwise Swanson's factors are used for narrow spacings.

The USER can modify the input data (e.g. to change probe spacings, probe depths, sapwood radii, etc). But, be careful to keep them in the same ' format(a16,4f8.2)', otherwise the program will probably generate an error.

Step - 2.

Next, add the  $t_z$  data collected from the logger. This data should look something like:

 $103,100,1200,120.5,135.6,180.2,268.2,195.6,140.2,78.2,30.4\\103,100,1215,120.5,135.6,180.2,268.2,195.6,140.2,78.2,30.4\\103,100,1230,120.5,135.6,180.2,268.2,195.6,140.2,78.2,30.4\\103,100,1245,120.5,135.6,180.2,268.2,195.6,140.2,78.2,30.4$ 

Note. The output from the logger is in the following format:

opid,day,hrmin,tz1\_1,tz1\_2,tz1\_3,tz1\_4,tz2\_1,tz2\_2,tz2\_3,tz2\_4

where		
opid	=	output identifier (103 $\Rightarrow$ output from table 1, line 3)
day	=	current day of year
hrmin	=	time when heat-pulse was fired
tz1_*	=	$t_z$ times for probe 1 (*=1 is the outside depth)
tz2_*	=	$t_z$ times for probe 2 (*=1 is the outside depth)

<u>Step - 3</u>

Just keep appending new data to the bottom of the old input file

### 6.3. Examining the output file

The analysis programme outputs three calculations of total sap flow, depending on how the volume sap flux, Q, is determined. In theory, this is given by the integral

$$Q = \int_{H}^{R} 2\pi r \ J(r) \ dr \tag{7}$$

for a stem of cambium radius R [m] and heartwood radius H [m]. In practice, this integral can be obtained by three different ways, where the operator <> will be used to represent the least-squares fit to the profile data.

Method 1: Fit the velocity profile and store the data in FILENAME.VEL.

$$Q = 2\pi \int_{H}^{R} r \left\langle J(r) \right\rangle dr$$
(7a)

Method 2: Fit the flux profile and store the data in FILENAME.FLX.

$$Q = 2\pi \int_{H}^{R} \left\langle r J(r) \right\rangle dr$$
(7b)

**Method 3**: Calculate a weighted sum of velocity,  $V_i$ , times an associated sapwood area,  $A_i$  and store the data in FILENAME.SUM (see Hatton, 1990 and analysis programme for details of  $A_i$ 's).

$$Q = \sum_{i} A_i V_i \tag{7c}$$

For well-behaved velocity profiles (i.e. small curvature at large radii) all three methods yield similar results, but for profiles where the curvature near the cambium method 3 is recommended (Hatton et al, 1990).

#### 6.4. Listing of the ANALYSIS program

The following is a listing of the FORTRAN program HPV-2000.FOR used to analyze the tz-data collected by the HPV data logger. The analysis procedure follows that outlined in the Background Section of this document. This is a fairly big program – only because it includes routines for graphical output to the screen.

```
c ... Program HPV2000.FOR to convert tz data to correct sap
c ... velocities using numerical simulation results for a
c ... given wound width and probe spacings of (-0.5,0,1.0)
 C
       ----- LAST modified AUG, 2000, S.R. Green -----
с...
USE DFLIB
       IMPLICIT NONE
c include files for MS Fortran graphics
        CHARACTER*50 CTITLE, ans
        REAL*8 NXPIX, NYPIX
        REAL*8 X1(101), Y1(101), X2(101), Y2(101)
        REAL*8 X1MIN, X1MAX, Y1MIN, Y1MAX
        INTEGER IX4, IY4, CWIN/0/
        LOGICAL STATUS, END_CALC
        TYPE (RCCOORD)
                             CURPOS
        TYPE (WINDOWCONFIG) WINC
        TYPE (QWINFO)
                                OWIN
      REAL TZ(4,4), HPV(4), PD(4,4), PS(4,4)
REAL TMIN, TMAX, EMIN, F0, F1, F2, BEGYR
        REAL R1P, R1M, R2M, R3M, R4M, A3, A4
        INTEGER IDAY, ITOD, IJ
        REAL WC1(5,7), WC2(5,7)
      REAL R(4), SV(4), SF(4)
      REAL SVIJ(16), T(100), Y(100)
      REAL SAPFLOWV(4,100), SAPFLOWF(4,100), SAPFLOWS(4,100)
       REAL SWR(4), HWR(4), WW(4), EMAX(4)
REAL VFWOOD, VFWAT, TOD
      REAL A0, A1, A2, FLUXVEL, FLUXFLX, FLUXV(4), FLUXF(4)
REAL ID, MI, PI, TWOPI
        REAL CHANID, DAY, HRMIN, HR, MIN
      INTEGER NHPV, N, I, ICORR, IW(4), J, NCOL(4), NTC(4), NC
      CHARACTER*40 FILNAM
        CHARACTER*4 STR
      LOGICAL SWANCOR
      INTEGER*2 DUMMY2, FGD
      INTEGER*4 DUMMY4, BGD
        COMMON WINC
        COMMON QWIN
C-----
c ... Set the wound corrections of Swanson and Whitfield (1983)
          -----
        DATA WC1/ 0, 0, 1,
                                    Ο,
                                           0.0.

        16, 0.393,
        1.356,
        0.036,
        0.0,

        20, 0.807,
        1.203,
        0.058,
        0.0,

        24,
        1.184,
        1.072,
        0.087,
        0.0,

        28,
        1.524,
        0.964,
        0.124,
        0.0,

     *
     *
```

32, 1.826, 0.879, 0.169, 0.0, 36, 2.090, 0.818, 0.221, 0.0 / C----c ... Set the wound corrections of Green and Clothier (1988) C----\_\_\_\_\_ DATA WC2/ 0, 0, 1, 0, 0.0, 16, -0.171, 1.299, 0.0194, -0.000093, 20, -0.159, 1.318, 0.0270, -0.000140, 24, -0.135, 1.326, 0.0367, -0.000194, 28, -0.143, 1.306, 0.0488, -0.000267, 20, 0.0027, 1.255 

 10,
 -0.1159,

 24,
 -0.135,

 28,
 -0.143,

 32,
 -0.067,

 36,
 -0.013,

 \* 1.355, 0.0571, -0.000203, 1.379, 0.0670, -0.000105/ PI=3.14159 TWOPI=2.\*PI C-----c ... Set the graphics mode CTITLE(1:40) = ' HEAT-PULSE analysis program C----CALL GRAPHICSMODE (CTITLE) 1 CALL CLEARSCREEN (\$GCLEARSCREEN) CALL SETTEXTPOSITION (5, 1, CURPOS) NXPIX = WINC.NUMXPIXELS !-20 NYPIX = WINC.NUMYPIXELS !- 100 NCOL(1) = 4NCOL(2)=10 NCOL(3) = 1NCOL(4) = 15BEGYR = -9999C ... Open input/output files C----- $\label{eq:WRITE(*,'(a\)') 'Enter the Input filename (.dat): 'READ(*,'(A)') FILNAM$ CALL NCSTRING (FILNAM, NC) OPEN(UNIT=30, FILE=FILNAM(1:NC)//'.DAT', STATUS='UNKNOWN') OPEN(UNIT=31, FILE=FILNAM(1:NC)//'.VEL', STATUS='UNKNOWN') OPEN(UNIT=32, FILE=FILNAM(1:NC)//'.FLX', STATUS='UNKNOWN') OPEN(UNIT=33, FILE=FILNAM(1:NC)//'.SUM', STATUS='UNKNOWN') C----c ... Read input data \_\_\_\_\_ C---WRITE(\*,\*)  $\texttt{WRITE}\left(\star,\star\right)$  'Enter the number of heat pulse probes (1..4)' READ(30,1099) ANS, NHPV 1099 FORMAT (A16, 418) WRITE(\*,1099) ANS, NHPV WRITE(\*,\*)
WRITE(\*,\*) 'Enter the number of sensors in each probe'
WRITE(\*,\*) 'Enter the number of sensors in each probe' WRITE(\*,\*) 'Enter the wound width from 1.6 to 3.6 (mm)' READ(30,1098) ANS, (WW(I), I=1,NHPV) 1098 FORMAT (A16, 4F8.2) WRITE(\*,1098) ANS, (WW(I), I=1,NHPV) SWANCOR = .FALSE. READ(30,1099) ANS, ICORR IF(ICORR.GT.(0.0)) THEN WRITE(\*,\*) 'Use Swansons corrections: YES' SWANCOR=.TRUE. ELSE WRITE(\*,\*) 'Use Swansons corrections: NO' SWANCOR=.FALSE. ENDIF WRITE(\*,\*) DO 12 J=1,NHPV IF(WW(J).EQ.(0.0)) IW(J) = 1IF (WW (J).GE. (1.6)) IW (J) = INT ((WW (J) - 1.6) / 0.4+2.5) IF (IW (J).GT.7) IW (J) = 7 CONTINUE 12 C-----

```
c ... vfwood = volume fraction of wood = 0.34
c ... vfwat = volume fraction of water = 0.56
C----
       WRITE(*,*) 'Enter the volume fraction of wood '
       READ(30,1098) ANS,VFWOOD
       WRITE(*,*) 'Enter the volume fraction of water '
       READ(30,1098) ANS, VFWAT
C-----
c ... mean sap wood radius in cm
C---
       WRITE(*,*) 'Enter the sap-wood radius of each stem/root [cm] '
       READ(30,1098) ANS, (SWR(J), J=1,NHPV)
       WRITE(*,1098) ANS, (SWR(J), J=1,NHPV)
WRITE(*,*) 'Enter the heartwood radius of each stem/root [cm] '
       READ(30,1098) ANS, (HWR(J), J=1,NHPV)
WRITE(*,1098) ANS, (HWR(J), J=1,NHPV)
       WRITE(*,*)
   _____
c ... read in the probe depths
C----
                  _____
           _____
       \texttt{WRITE}\,(\,^{\star},\,^{\star}) 'Enter the thermistor depths of each probe [cm] '
       DO 30 J=1,NHPV
         READ(30,1098) ANS, (PD(I,J),I=1,NTC(J))
         WRITE(*,1098) ANS, (PD(I,J),I=1,NTC(J))
         READ(30,1098) ANS, (PS(I,J),I=1,NTC(J))
WRITE(*,1098) ANS, (PS(I,J),I=1,NTC(J))
         DO 30 I=1,NTC(J)
30
       PD(I,J) = ABS(SWR(J) - PD(I,J))
       WRITE(*,*)
C-----
                  _____
c ... read plot range
C-----
       WRITE(*,*) 'Enter DOY range: Tmin, Tmax'
       READ(30,1098) ANS, TMIN,TMAX
WRITE(*,1098) ANS, TMIN,TMAX
WRITE(*,*) 'Enter SAPFLOW range: Emin, Emax'
       READ(30,1098) ANS, (EMAX(I), I=1,NHPV)
WRITE(*,1098) ANS, (EMAX(I), I=1,NHPV)
       EMIN = 0.0
      CALL SETTEXTPOSITION(33,35,CURPOS)
       WRITE(*,*) '***** Click <MOUSE> to END *****'
       CALL MOUSECLICK (IX4, IY4)
       CALL CLEARSCREEN ($GCLEARSCREEN)
       STATUS = SETCOLOR(8)
       STATUS = RECTANGLE($GFILLINTERIOR, 0, 0, NXPIX, NYPIX)
       STATUS = SETCOLOR(2)
C-----
c ... main Loop
c-----
                     _____
     TDAY=0
100 READ(30, *, END=1000) CHANID, DAY, HRMIN,
              ((TZ(I,J),I=1,NTC(J)),J=1,NHPV)
       IF (BEGYR.LT.0) THEN
         TMIN = DAY
         BEGYR = 9999
       ENDIF
       IF (HRMIN.LT.5) THEN
         IDAY=IDAY+1
          DO 120 J=1, NHPV
            DO 110 I=1,ITOD
            X1(I) = T(I)
               Y1(I) = SAPFLOWV(J, I)
110
          CONTINUE
          X1MIN = TMIN !T(1)
          X1MAX = TMIN+5. !T(ITOD)
          Y1MIN = EMIN
          Y1MAX = EMAX(1)
    CALL NEWONEPLOT(X1,Y1,ITOD,'Day of Year', ''
&,'Water_Use_[L/h]','', X1MIN,X1MAX,Y1MIN,Y1MAX,.TRUE.,.FALSE.,8+J)
120
         CONTINUE
```

```
ITOD = 1
        IF (IDAY.GT.5) THEN
          IDAY = 1
          TMIN = TMIN+5
TMAX = TMAX+5
          CALL SETTEXTPOSITION(33, 35, CURPOS)
          WRITE (*, *) '***** Click <MOUSE> to CONTINUE *****'
          CALL MOUSECLICK (IX4, IY4)
          CALL CLEARSCREEN ($GCLEARSCREEN)
          STATUS = SETCOLOR(8)
          STATUS = RECTANGLE($GFILLINTERIOR, 0, 0, NXPIX, NYPIX)
          STATUS = SETCOLOR(2)
        ENDIF
      ELSE
        ITOD = ITOD+1
      ENDIF
C-----
c ... convert hrmin to time of day
C--
                              _____
      HR = INT(HRMIN/100)
      MIN = HRMIN - 100*HR
      TOD = DAY + (HR+MIN/60)/24
      T(ITOD) = TOD
C-----
c ... For each set of probes find the corrected SV profile,
C ... then compute flux using three different methods
C----
      DO 300 J=1,NHPV
         DO 200 I=1,NTC(J)
           IF( TZ(I, J).gt.(0.0) ) THEN
            HPV(I) = PS(I,J) / (2.*TZ(I,J))*3600.
           ELSE
            HPV(I) = 0.0
           ENDIF
C-----
                           c ... compute the corrected SV
C-----
          IJ = (J-1) * NTC (J) + I
          IF (SWANCOR) THEN
            SV(I) = (WC1(5,IW(j))*HPV(I)*HPV(I)*HPV(I)
                  + WC1(4, IW(j)) * HPV(I) * HPV(I)
    *
                  + WC1(3,IW(j))*HPV(I)
                  + WC1(2, IW(j)))*(0.505*VFWOOD + VFWAT)
          ELSE
            SV(I) = (WC2(5, IW(j)) * HPV(I) * HPV(I) * HPV(I))
                  + WC2(4, IW(j)) *HPV(I) *HPV(I)
+ WC2(3, IW(j)) *HPV(I)
    *
                  + WC2(2,IW(j)))*(0.505*VFWOOD + VFWAT)
           ENDIF
          R(I) = PD(I, J)
           SVIJ(IJ) = SV(I)
           SF(I) = SV(I) * R(I)
200
       CONTINUE
      N = NTC(J)
      CALL REGRESS(N, R, SV, A0, A1, A2)
     CALL REGRESS(N, R, SF, F0, F1, F2)
C_____
c ... compute total flow, making sure that it remains positive !!!
C----
       FLUXV(J) = 0.0
       FLUXF(J) = 0.0
       ID = HWR(J) - 0.01
       DO WHILE (ID.LT.SWR(J))
         ID = ID + 0.01
         MI = ID + 0.005
         FLUXVEL = TWOPI*MI*(A0 + A1*MI + A2*MI*MI)*0.01
         IF (FLUXVEL.GT.(0.0)) FLUXV(J) = FLUXV(J) + FLUXVEL
         FLUXFLX = TWOPI*(F0 + F1*MI + F2*MI*MI)*0.01
         IF (FLUXFLX.GT.(0.0)) FLUXF(J) = FLUXF(J) + FLUXFLX
       END DO
       FLUXV(J) = FLUXV(J)/1000
       FLUXF(J) = FLUXF(J) / 1000
```

```
SAPFLOWV(J,ITOD) = FLUXV(J)
        SAPFLOWF(J, ITOD) = FLUXF(J)
С
       GOTO 299
C-----
C ... compute sum of sap velocity times relative sapwood area
C----
                       _____
       R1P = SWR(J)
       R1M = (R(1) + R(2)) / 2.
       R2M = (R(2) + R(3)) / 2.
       R3M = (R(3) + R(4)) / 2.
       R4M = HWR(J)
       A1=(R1P*R1P-R1M*R1M)*PI
       A2 = (R1M*R1M-R2M*R2M)*PI
       A3=(R2M*R2M-R3M*R3M)*PI
        A4=(R3M*R3M-R4M*R4M)*PI
       SAPFLOWS(J,ITOD) = A1*SV(1)+A2*SV(2)+A3*SV(3)
SAPFLOWS(J,ITOD) = (SAPFLOWS(J,ITOD)+A4*SV(4))/1000.
299
       CONTINUE
C-----
c ... print out the results
C----
                 _____
300
     CONTINUE
301
       CONTINUE
     WRITE(31,995) T(ITOD), (SAPFLOWV(J,ITOD), J=1,NHPV)
* ,(SAPFLOWV(1,ITOD)+SAPFLOWV(2,ITOD))/2.
С
      WRITE(32,995) T(ITOD), (SAPFLOWF(J,ITOD), J=1,NHPV)
С
          , (SAPFLOWF(1,ITOD)+SAPFLOWF(2,ITOD))/2.
      (SAPFLOWS (1, ITOD), (SAPFLOWS (J, ITOD),
* ,(SAPFLOWS (1, ITOD) + SAPFLOWS (2, ITOD))/2.
GOTO 100
      WRITE(33,995) T(ITOD), (SAPFLOWS(J,ITOD), J=1,NHPV)
C
1000
      CONTINUE
       FORMAT (2A40)
999
      FORMAT(5x, 'Time [d] = ', F8.3, ' Sap flow [L/h] = ', 8F8.3
996
        ,6X,1H.)
     FORMAT(1X, F8.3, 8F8.3)
995
C-----
      CALL SETTEXTPOSITION(33,35,CURPOS)
       WRITE(*,*) '***** Click <MOUSE> to END *****'
       CALL MOUSECLICK(IX4,IY4)
      CALL CLEARSCREEN ($GCLEARSCREEN)
C-----
      STOP
       END
_____
      SUBROUTINE REGRESS(N, X, Y, A0, A1, A2)
 ... fit a parabola through the SFD data using N data points
С
С
     of the form \dots y = A0 + A1.x + A2.x<sup>2</sup>
IMPLICIT NONE
       REAL X(4), Y(4), A0, A1, A2
       REAL SX, SY, SX2, SXY, SX2Y, SX3, SX4
       REAL SSX2, D
       INTEGER N, I
       IF (N.GT.2) THEN
       SX = 0
       SY = 0
       SX2 = 0
       SXY = 0
       SX3 = 0
       SX2Y = 0
       SX4 = 0
       DO 100 I=1,N
       SX = SX + X(I)
       SY = SY + Y(I)
       SXY = SXY + X(I) * Y(I)
       SX2 = SX2 + X(I) * X(I)
       SX2Y= SX2Y+ X(I)*X(I)*Y(I)
       SX3 = SX3 + X(I) * * 3
       SX4 = SX4 + X(I) * * 4
100
       CONTINUE
       SSX2 = SX2
       SX4 = SX4 - SX2*SX2/N
```

```
SX3 = SX3 - SX*SX2/N
     SXY = SXY - SX*SY/N
     SX2Y= SX2Y- SX2*SY/N
     SX2 = SX2 - SX*SX/N
     D = SX2*SX4 - SX3**2
A1 = (SX4*SXY - SX3*SX2Y)/D
     A2 = (SX2*SX2Y - SX3*SXY)/D
     A0 = SY/N - A1*SX/N - A2*SSX2/N
      ELSE
       A0 = (Y(1) + Y(2)) / 2.
       A1=0.0
       A2=0.0
      ENDIF
     RETURN
     END
! _____
     SUBROUTINE GRAPHICSMODE(CTITLE)
1_____
     USE DFLIB
     IMPLICIT NONE
     TYPE (WINDOWCONFIG) WINC
     TYPE (QWINFO)
                       OW
     INTEGER RETI2, CWIN/0/
     LOGICAL STATUS, RESULT
     CHARACTER*50 CTITLE
     COMMON WINC
     COMMON QW
  _____
! ... set up the size of the frame window
1_____
         _____
     WINC.NUMXPIXELS = -1
     WINC.NUMYPIXELS = -1
     WINC.NUMTEXTCOLS = -1
     WINC.NUMTEXTROWS = -1
     WINC.NUMCOLORS = -1
WINC.TITLE = CTITLE
     STATUS = SETWINDOWCONFIG(WINC)
     IF(.NOT.STATUS) STATUS = SETWINDOWCONFIG(WINC)
     STATUS = FOCUSQQ(CWIN)
1 ---
  _____
! ... set the frame window to maximum
1 -----
                   _____
     QW.TYPE = QWIN$MAX
     RETI2 = SETWSIZEQQ(QWIN$FRAMEWINDOW, QW)
     RETI2 = SETWSIZEQQ(CWIN, QW)
     RETURN
     END SUBROUTINE GRAPHICSMODE
SUBROUTINE NCSTRING (STRING, NCHAR)
CHARACTER*40 STRING
      INTEGER NCHAR, I
      T = 2
      DO WHILE (STRING (I:I) .NE.'')
       I = I + 1
      END DO
      NCHAR = I-1
      END
!-----
               SUBROUTINE INLINE (NUNIT, NLINE, OP)
c ... read nlines from file nunit write to screen in OP is true
!=====
      IMPLICIT NONE
      INTEGER I, NLINE, NUNIT
CHARACTER*80 LINE
      LOGICAL OP
```

```
DO 10 I=1,NLINE
          READ (NUNIT, 99) LINE
          IF(OP) WRITE( *,99) LINE
         CONTINUE
10
99
        FORMAT (A75)
        RETURN
        END SUBROUTINE INLINE
SUBROUTINE NEWONEPLOT(X1,Y1,NUM1,XTITLE, XUNIT, YTITLE, YUNIT
     & ,GX1MIN, GX1MAX, GY1MIN, GY1MAX, Y1LABEL, Y2LABEL ,LCOL)
USE DFLIB
       IMPLICIT NONE
       TYPE (WINDOWCONFIG) WINC
       TYPE (QWINFO)
       TYPE (QWINFO) QW
INTEGER NUM1, NTICKX1, NTICKY1
INTEGER I, J,NXPIX, NYPIX, NC1, NC2
       INTEGER IX, IY, ix4, iy4, LCOL
        INTEGER STATUS
       REAL*8 X1(NUM1), Y1(NUM1)
       REAL*8 XX(NUM1), YY(NUM1)
       REAL*8 X1MIN, X1MAX, X1RANGE, Y1MIN, Y1MAX, Y1RANGE
       REAL*8 GX1MIN, GX1MAX, GY1MIN, GY1MAX
       REAL*8 X1SCALE, DTICKX1, DUMMYSCALE
REAL*8 Y1SCALE, DTICKY1
       REAL*8 XP,YP, NEWX1MAX
       CHARACTER*40 XTITLE, XUNIT, NEWXUNIT, XTITLEUNIT
       CHARACTER*40 YTITLE, YUNIT, NEWYUNIT, YTITLEUNIT, GTITLE
LOGICAL INVERT, LOGPLOT, SCALE, TALL, Y1LABEL, Y2LABEL
       COMMON WINC
       COMMON QW
       NXPIX = WINC.NUMXPIXELS !-20
NYPIX = WINC.NUMYPIXELS !-100
       X1MIN = GX1MIN
       X1MAX = GX1MAX
       Y1MIN = GY1MIN
       Y1MAX = GY1MAX
       DO 10 I=1,NUM1
         XX(I) = (X1(I) - X1MIN) / (X1MAX - X1MIN)
         YY(I) = (Y1(I) - Y1MIN) / (Y1MAX-Y1MIN)
10
       CONTINUE
       CALL AXISSET (X1MIN, X1MAX, X1SCALE, NTICKX1, DTICKX1)
                                                                      ! SOMETHING WRONG HERE
??
       CALL AXISSET (Y1MIN, Y1MAX, Y1SCALE, NTICKY1, DTICKY1)
       X1RANGE = (X1MAX-X1MIN) *X1SCALE
!
       Y1RANGE = (Y1MAX-Y1MIN) *Y1SCALE
!
       CALL NCSTRING(XTITLE, NC1)
       CALL NCSTRING( XUNIT, NC2)
       XTITLEUNIT = XTITLE(1:NC1)//XUNIT(1:NC2)
       if(x1scale.gt.1.0) xtitleunit = xtitle(1:11)//']'
       CALL NCSTRING (YTITLE, NC1)
       CALL NCSTRING( YUNIT, NC2)
       YTITLEUNIT = YTITLE(1:NC1)//YUNIT(1:NC2)
       CALL SETVIEWPORT(0,0,NXPIX/1.0, NYPIX)
        ! FOR GRAPH1
       STATUS = SETWINDOW(.TRUE., -0.25D0, -0.50D0, 1.25D0, 1.15D0)
       CALL TITLEAXIS(0.5D0,-0.15D0,XTITLEUNIT,1.4D0,1.4D0,NXPIX/1
     &
         ,NYPIX,TALL,1)
        ! XAXIS TITLE
       CALL PLOTXTICK (X1MIN, X1MAX, X1SCALE, NTICKX1, 15, TALL
     & ,1.4D0,1.4D0,NXPIX/1, NYPIX,.FALSE.)
        IF(Y1LABEL) THEN
         CALL TITLEAXIS (-0.20D0, 0.5D0, YTITLEUNIT, 1.4D0, 1.4D0, NXPIX/1
         ,NYPIX,TALL,2)
        ! YAXIS TITLE
         CALL PLOTYTICK(0.0D0,Y1MIN, Y1MAX, Y1SCALE, NTICKY1,15, TALL
     & ,1.4D0,1.4D0,NXPIX/1, NYPIX)
```

```
38
```

```
ENDIF
       IF (Y2LABEL) THEN
        CALL TITLEAXIS(1.15D0,0.5D0,YTITLEUNIT,1.4D0,1.4D0,NXPIX/1
         ,NYPIX,TALL,2)
    £
       ! YAXIS TITLE
        CALL PLOTYTICK(1.0D0,Y1MIN, Y1MAX, Y1SCALE, NTICKY1,15, TALL
       ,1.4D0,1.4D0,NXPIX/1, NYPIX)
    £
      ENDIF
       STATUS = SETCOLOR(7)
      STATUS = RECTANGLE_W($GBORDER, 0.0D0, 0.0D0, 1.0D0, 1.0D0)
      CALL PLOTLINE (XX, YY, NUM1, LCOL)
      RETURN
      END SUBROUTINE NEWONEPLOT
!============
              _____
      SUBROUTINE TITLEAXIS (WXP, WYP, AXTITLE, XW, YH
    & ,NXPIX, NYPIX, TALL ,NAXIS)
!=====
               _____
      USE DFLIB
      IMPLICIT NONE
      REAL*8 WXP, WYP, DWXP, DWYP, XW, YH
CHARACTER*30 AXTITLE
      INTEGER I, CHEI, CWID, NCBEG, NCEND, TLEN, NAXIS INTEGER STATUS, NXPIX, NYPIX
      LOGICAL TALL
       TYPE (WXYCOORD)
                         WXY
                        FONT
      TYPE (FONTINFO)
! ... set the font
      STATUS = INITIALIZEFONTS()
       I = SETFONT ("T'COURIER NEW'H30W15")
      CWID = FONT.PIXWIDTH
       CHEI = FONT.PIXHEIGHT
       STATUS = SETCOLOR(INT2(0))
! ... trim the string for leading blanks
       NCBEG = 1
      DO WHILE (AXTITLE (NCBEG:NCBEG) .EQ.'')
        NCBEG = NCBEG+1
      END DO
      NCEND = NCBEG + LEN_TRIM(AXTITLE(NCBEG:))-1
       TLEN = GETGTEXTEXTENT (AXTITLE (NCBEG:NCEND) )
! ... add an offset for the text
       IF (NAXIS.EQ.1) THEN
        DWYP = 0.0
        DWXP = -((REAL(TLEN)/2.)/REAL(NXPIX)*XW)
      ELSE IF (NAXIS.EQ.2) THEN
        DWYP = -((REAL(TLEN)/2.)/REAL(NYPIX)*YH)
        DWXP = 0.0
      ELSE
        DWYP = 0.0
        DWXP = -(REAL(TLEN/2.)/REAL(NXPIX)*XW)
      ENDIF
      CALL MOVETO_W(WXP+DWXP,WYP+DWYP,WXY)
      IF (NAXIS.EQ.2) THEN
        CALL SETGTEXTROTATION(900)
      ELSE
        CALL SETGTEXTROTATION(0)
      ENDIF
      CALL OUTGTEXT ( AXTITLE (NCBEG:NCEND))
      RETURN
      END SUBROUTINE TITLEAXIS
SUBROUTINE PLOTLINE (XX, YY, NUM, LCOL)
USE DELTR
      IMPLICIT NONE
      INTEGER I, NUM, LCOL, BGCOL
```

```
REAL*8 XX(NUM), YY(NUM)
      LOGICAL STATUS
      TYPE (WXYCOORD)
                         WXY
      STATUS = SETCOLOR(LCOL)
      CALL MOVETO_W(XX(1), YY(1), WXY)
      DO 10 I=2, NUM
        STATUS = LINETO_W(XX(I), YY(I))
10
      CONTINUE
      RETURN
      END SUBROUTINE PLOTLINE
SUBROUTINE PLOTXTICK (LOWX, HIGHX, XSCALE, NTICK, NCOL,
   & TALL, XW, YH, NXPIX, NYPIX, LOGPLOT)
USE DFLIB
      IMPLICIT NONE
      TYPE (WXYCOORD)
                                WXY
      REAL*8 LOWX, HIGHX, XSCALE, XRANGE, XTICK, DXTICK
      REAL*8 LOWY, HIGHY, YSCALE, YRANGE, YTICK, DYTICK
      REAL*8 XW,YH, XLABEL
      REAL*8 TICKLEN /0.025/
      INTEGER I, NTICK, NCOL, NXPIX, NYPIX
LOGICAL RESULT, STATUS, TALL, LOGPLOT
! plot the xticks
      STATUS = SETCOLOR (NCOL)
      IF(TALL) TICKLEN = 0.015
      DXTICK = 1.0D0/REAL(NTICK)
      DO 10 I=0,NTICK
        XTICK = REAL(I) *DXTICK
        YTICK = 0.0D0
        XLABEL = LOWX + XTICK* (HIGHX-LOWX)
        CALL MOVETO_W(XTICK, YTICK, WXY)
        RESULT = LINETO_W(XTICK, YTICK - TICKLEN)
        CALL NUMAXIS(XTICK, YTICK-2.0*TICKLEN, XLABEL, XW, YH, NXPIX, NYPIX
        ,1, LOGPLOT)
    8
      !!!!! LOG PLOT ON XAXIS
        XTICK = REAL(I)*DXTICK
YTICK = 1.0D0
        CALL MOVETO_W(XTICK, YTICK, WXY)
        RESULT = LINETO_W(XTICK, YTICK + TICKLEN)
10
      CONTINUE
      RETURN
      END SUBROUTINE PLOTXTICK
SUBROUTINE PLOTYTICK (XLOC, LOWY, HIGHY, YSCALE, NTICK, NCOL,
                        TALL, XW,YH,NXPIX, NYPIX )!,Y1TICK,Y2TICK)
   £
USE DFLIB
      IMPLICIT NONE
      TYPE (WXYCOORD)
                                 WXY
      REAL*8 LOWX, HIGHX, XSCALE, XRANGE, XTICK, DXTICK
      REAL*8 LOWY, HIGHY, YSCALE, YRANGE, YTICK, DYTICK
      REAL*8 TICKLEN /0.01/
      REAL*8 XW, YH, YLABEL, XLOC
      INTEGER I, NTICK, NCOL, NXPIX, NYPIX
      LOGICAL RESULT, STATUS, TALL !, Y1TICK, Y2TICK
! plot the xticks
      STATUS = SETCOLOR (NCOL)
      IF(TALL) TICKLEN = 0.020
DYTICK = 1.0D0/REAL(NTICK)
      DO 10 I=0,NTICK
        YTICK = REAL(I) *DYTICK
        XTICK = XLOC
        YLABEL = LOWY + YTICK* (HIGHY-LOWY)
        CALL MOVETO_W(XTICK, YTICK, WXY)
        RESULT = LINETO_W (XTICK-TICKLEN, YTICK )
        IF(XLOC.LT.0.5D0) THEN
         CALL NUMAXIS(XTICK-0.05,YTICK,YLABEL, XW,YH,NXPIX
    &
       , NYPIX,2, .FALSE.)
                              !!!! NO LOG PLOT ON YAXIS
```

```
ELSE
           CALL NUMAXIS (XTICK+0.1, YTICK, YLABEL, XW, YH, NXPIX
          NYPIX, 2, .FALSE.) !!!! NO LOG PLOT ON YAXIS
     £
         ENDIF
10
       CONTINUE
       RETURN
       END SUBROUTINE PLOTYTICK
!_____
       SUBROUTINE NUMAXIS (WXP, WYP, VALUE, XW, YH, NXPIX, NYPIX, NAXIS, LOGPLOT)
! THE MAJOR TICKS
!==================
                        USE DFLIB
       IMPLICIT NONE
       REAL*8 WXP, DWXP, WYP, DWYP, VALUE, XW,YH INTEGER NXPIX, NYPIX, CHEI, CWID
       INTEGER I, STATUS, NPOINTS/1/, NAXIS, TLEN
       INTEGER NCBEG, NCEND, NC1, NC2, NC3
CHARACTER*16 TEMPSTR, FMS, LOGSTR
       LOGICAL LOGPLOT
       TYPE (XYCOORD) XY
       TYPE (WXYCOORD) WXY
       TYPE (WINDOWCONFIG) WINC
       TYPE (FONTINFO) FONT
       COMMON WINC
! ... get the font information
       STATUS = INITIALIZEFONTS()
       I = SETFONT("T'COURIER NEW'H20W10")
       I = GETFONTINFO (FONT)
       CWID = FONT.PIXWIDTH
CHEI = FONT.PIXHEIGHT
! ... get the tick value
WRITE(FMS,'(A5,I2,A1)') '(F10.',NPOINTS,')'
       WRITE (TEMPSTR, FMS) VALUE
! ... trim the string for leading blanks
       NCBEG = 1
       DO WHILE (TEMPSTR (NCBEG:NCBEG) .EQ.'')
         NCBEG = NCBEG+1
       END DO
       NCEND = NCBEG + LEN_TRIM(TEMPSTR(NCBEG:))-1
! ... add in the exponent for a log scale
       IF (LOGPLOT) THEN
         LOGSTR = '1E'//TEMPSTR(NCBEG:NCEND)
         CALL NCSTRING (LOGSTR, NC1)
         TEMPSTR(1:NC1) = LOGSTR(1:NC1)
         NCBEG = 1
         NCEND = NC1
       ENDIF
       TLEN = GETGTEXTEXTENT (TEMPSTR (NCBEG:NCEND))
! ... add an offset for the text (to centre it on the ticks)
       IF(NAXIS.EQ.1) THEN
         DWYP = 0.0
         DWXP = -((REAL(TLEN)/2.)/REAL(NXPIX)*XW)
       ELSE
         DWYP = ((REAL(CHEI)/2.)/REAL(NYPIX)*YH)
         DWXP = -((REAL(TLEN))/REAL(NXPIX)*XW)
       ENDIF
       CALL MOVETO_W(WXP+DWXP,WYP+DWYP,WXY)
       CALL SETGTEXTROTATION(0)
       CALL OUTGTEXT ( TEMPSTR (NCBEG:NCEND) )
       RETURN
       END SUBROUTINE NUMAXIS
```

SUBROUTINE AXISSET(LOW, HIGH, RSCALE, NTICKS, DTICKS)

```
IMPLICIT NONE
       REAL*8 HIGH, LOW, RANGE, DLHI, DLLO, DTICKS
REAL*8 RPOW, RSCALE, RMAG, TEMP, TINY/1E-20/
         INTEGER NTICKS, HELPSCALE
! ... find the range and magnitude and rescale if necessary
        RPOW = 0.0D0
         RANGE = HIGH - LOW
         IF(LOW .EQ.0.0D0) LOW = TINY
         IF(HIGH.EQ.0.0D0) HIGH = 2.0d0*LOW
        IF (RANGE.EQ. 0.0D0) THEN ! THE LINE IS VERTICAL
         HIGH = HIGH + 0.5
         LOW = LOW - 0.5
        ENDIF
        DLHI = DLOG10 (ABS (HIGH))
        DLLO = DLOG10 (ABS (LOW))
        DO WHILE (DLHI.LT.0.0D0 .AND. DLLO.LT.0.0D0)
         DLHI = DLHI + 3.0D0
         DLLO = DLLO + 3.0D0
         RPOW = RPOW + 3.0D0
        END DO
        HIGH = HIGH*10**RPOW
        LOW = LOW*10**RPOW
        RSCALE = 10 * * - RPOW
       RANGE = HIGH-LOW
        RMAG = 10**INT(DLOG10(RANGE)) ! 10S, 100S, 1000S FOR EG.
  ... determine the lhs axis value
!
        TEMP = LOW/RMAG
                                       ! CALCULATE LOW (FOR AXIS)
             = INT(TEMP)
        LOW
        IF (ABS(TEMP-LOW).GE.1.0E-12 .AND. TEMP.LT.0) THEN
         LOW = LOW - 1
        ENDIF
       LOW = LOW*RMAG
! ... determine the rhs axis value
        TEMP = HIGH/RMAG
                                       ! CALCULATE HIGH (FOR AXIS)
        HIGH = INT(TEMP)
        IF (ABS (TEMP-HIGH).GE.1E-12 .AND. TEMP.GT.0) THEN
         HIGH = HIGH + 1
        ENDIF
        HIGH = HIGH*RMAG
! ... determine the number of axis ticks
        HELPSCALE = (HIGH-LOW) / RMAG
        IF (HELPSCALE.GT.5) THEN
         NTICKS = 5 !HELPSCALE
        ELSE
         SELECT CASE (HELPSCALE)
           CASE(5)
             NTICKS = 5
           CASE(4)
             NTICKS = 4
            CASE(3)
             NTICKS = 3
            CASE(2)
             NTICKS = 4
            CASE(1)
             NTICKS = 5
         END SELECT
        ENDIF
       DTICKS = (HIGH-LOW) /NTICKS
RANGE = HIGH-LOW
         IF (RANGE.GE.1000) THEN
           HIGH = HIGH*1.0D-3
LOW = LOW*1.0D-3
           RSCALE = RSCALE*1.0D3
         ENDIF
       END SUBROUTINE AXISSET
!-----
      SUBROUTINE RANGESET(X, NX, XMIN, XMAX)
____
                                       _____
```

C------

IMPLICIT NONE

```
INTEGER I, NX
      REAL*8 X(NX), XMIN, XMAX
XMIN = 1.0D10
      XMAX = -1.0D10
      DO 10 I=1,NX
       IF(X(I).LE.XMIN) XMIN = X(I)
       IF(X(I).GE.XMAX) XMAX = X(I)
10
      CONTINUE
      RETURN
      END SUBROUTINE RANGESET
SUBROUTINE MOUSECLICK(X,Y)
USE DFLIB
      IMPLICIT NONE
      INTEGER*4 MOUSEEVENT, KEYSTATE, X, Y, RESULT
       MOUSEEVENT = MOUSE$RBUTTONDOWN .OR. MOUSE$LBUTTONDOWN
       RESULT = WAITONMOUSEEVENT (MOUSEEVENT, KEYSTATE, X, Y)
       WRITE(5,*) 'MOUSE AT ', X, Y
!
      RETURN
      END SUBROUTINE MOUSECLICK
!======
     SUBROUTINE MOUSETOEXIT (UNIT, MOUSEEVENT, KEYSTATE
   & ,MOUSEXPOS,MOUSEYPOS)
!======
       _____
               _____
                          USE DFLIB
       INTEGER UNIT, MOUSEEVENT, KEYSTATE, MOUSEXPOS, MOUSEYPOS
       LOGICAL MOUSEEXIT
       COMMON /MOUSE/ MOUSEEXIT
       MOUSEEXIT = .TRUE. ! ONLY EXECUTED IF MOUSE LBUTTON IS PRESSED
       RETURN
      END SUBROUTINE MOUSETOEXIT
```

## 7. References

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#### Appendix A – use of an AM25T multiplexer:

Listing of logger programme to connect 3 heat-pulse units to a single CR10 data logger. Note: One AM25T could be used to measure up to 6 heat-pulse units, but this requires a small modification to the programme described below. Please email the author for details.

CR10: AM25T +12 +12 G G C3 CLK C2 RES EX no connection AG AG 1H HI 1L LO (1H, 1L, 2H, 2L) Output from box-1, probe 1 (3H, 3L, 4H, 4L) Output from box-1, probe 2 (5H, 5L, 6H, 6L) Output from box-2, probe 1 (7H, 7L, 8H, 8L) Output from box-2, probe 2 and so on ... \*Table 1 Program 01: 0.25 Execution Interval (seconds) 1: If time is (P92) ; Flag 1 is automatic sampling 1: 0000 Minutes (Seconds --) into a ; once every 30 minutes 2: 30 Interval (same units as above) ;Change as required 3: 11 Set Flag 1 High 2: If Flag/Port (P91) ; Flag 5 is set when  $t_z$  is calculated 1: 15 Do if Flag 5 is High 2: 30 Then Do 3: Timer (P26) 1: 99 Loc [ \_\_\_\_\_ ] 4: Do (P86) ; Activate AM25T Set Port 2 High 1: 42 ; Connect Port 2 (C2) to Reset on AM25T 5: Beginning of Loop (P87) ; Measure inputs on 2\*N boxes 1: 0000 Delav 2: 12 Loop Count ; (2\* N boxes) Change as required 6: Step Loop Index (P90) 1: 2 Step ; Connect Port 3 (C3) to Clock on AM25T 7: Do (P86) 1: 43 Set Port 3 High 8: Do (P86) 1: 53 Set Port 3 Low 9: Do (P86) 1: 43 Set Port 3 High 10: Do (P86)

1: 53 Set Port 3 Low 11: Volt (SE) (P1) 1: 2 Reps 2: 15 2500 mV Fast Range 3: 1 SE Channel 4: 31 -- Loc [ \_\_\_\_\_ ] 5: 1.0 Mult 6: 0.0 Offset 12: Z=X-Y (P35) Calculate temperature difference 1: 31 -- X Loc [ \_\_\_\_\_ ] -- Y Loc [ \_\_\_\_\_ ] 2: 61 3: 31 -- Z Loc [ \_\_\_\_\_ ] and store in loc (31..54) 13: End (P95) 14: Do (P86) De-activate AM25T 1: 52 Set Port 2 Low 15: Beginning of Loop (P87) ; Check each input for a cross-over 1: 0 Delay Loop Count 2: 24 8\*N boxes 16: If (X<=>F) (P89) 1: 1 -- X Loc [ \_\_\_\_ ] 2: 1 = F 3: 0.0 4: 30 Then Do 17: If (X<=>F) (P89) If a cross-over has occurred 1: 31 -- X Loc [\_\_\_\_\_] < 2: 4 3: 0.0 F 4: 30 Then Do 18: Z=X (P31) Store tz in loc (1..24) 

 1: 99
 X Loc [ \_\_\_\_\_ ]

 2: 1
 -- Z Loc [ \_\_\_\_\_ ]

 19: Z=Z+1 (P32) Increment the 'tz' counter 1: 90 Z Loc [ \_\_\_\_\_ ] 20: End (P95) 21: End (P95) 22: End (P95) 23: If (X<=>F) (P89) ; If all 24 channels have crossed over 1: 90 X Loc [\_\_\_\_\_ ]; then set flag 6 (to exit loop) 2: 3 >= F 3: 24 4: 16 Set Flag 6 High 24: If (X<=>F) (P89) ; if time > 300 s 1: 99 X Loc [ \_\_\_\_\_ ] ; then set flag 6 (to exit loop) >= 2: 3 3: 300 F Set Flag 6 High 4: 16

25: End (P95) 26: If Flag/Port (P91) ; Flag 6 is used to generate output 1: 16 Do if Flag 6 is High Then Do 2: 30 27: Do (P86) 1: 10 Set Output Flag High 28: Sample (P70) Output the date and time 1: 2 Reps Loc [ \_\_\_\_\_ ] 2: 91 29: Sample (P70) Output the 24 tz values 1: 24 change as required Reps Loc [ \_\_\_\_\_ ] 2: 1 30: Do (P86) 1: 26 Set Flag 6 Low 31: Do (P86) 1: 25 Set Flag 5 Low 32: End (P95) 33: If Flag/Port (P91) ; Flag 1 begins the heat-pulse routine 1: 11 Do if Flag 1 is High 2: 30 Then Do 34: Time (P18) 1: 2 Hours into current year (maximum 8784) 2: 8784 Mod/By 3: 91 Loc [\_\_\_\_\_] 35: Z=X\*F (P37) 1: 91 X Loc [\_\_\_\_\_] 2: .04167 F 3: 91 Z Loc [ \_\_\_\_\_ ] 36: Z=INT(X) (P45) X Loc [ \_\_\_\_\_ ] Z Loc [ \_\_\_\_\_ ] 1: 91 2: 91 

 37: Z=Z+1 (P32)
 ; Store the current day number (loc 91)

 1: 91
 Z Loc [\_\_\_\_\_]

 38: Time (P18) 1: 2 Hours into current year (maximum 8784) Mod/By 2: 24 3: 92 Loc [ \_\_\_\_\_ ] 39: Z=X\*F (P37) 1: 92 X Loc [\_\_\_\_\_] 2: 100 F 3: 92 Z Loc [ \_\_\_\_\_ ] 40: Time (P18) 1: 1 Minutes into current day (maximum 1440) 2: 60 Mod/By 3: 93 Loc [\_\_\_\_\_]

 

 41: Z=X+Y (P33)
 ; Store the time (hrmin) (loc 92)

 1: 92
 X Loc [\_\_\_\_\_\_]

 41: Z=X+Y (P33) 2: 93 Y Loc [ \_\_\_\_\_ ] 3: 92 Z Loc [ \_\_\_\_\_ ] 42: Beginning of Loop (P87) 1: 0 Delay 2: 90 Loop Count +>: Z=F (P30) ; Reset all storage arrays
1: 0 F
2: 0 Exponent of 10
3. 1 43: Z=F (P30) 3: 1 -- Z Loc [ \_\_\_\_\_ ] 44: End (P95) 45: Do (P86) ; measure initial voltage using AM25T 1: 42 Set Port 2 High ; Port 2 is connected reset of AM25T 46: Beginning of Loop (P87) Delay 1: 0 Loop Count ; for 4\* N boxes 2: 12 47: Step Loop Index (P90) 1: 2 Step 48: Do (P86) ; Port 3 (C3) connects to clock of AM25T 1: 43 Set Port 3 High 49: Do (P86) 1: 53 Set Port 3 Low 50: Do (P86) 1: 43 Set Port 3 High 51: Do (P86) 1: 53 Set Port 3 Low 52: Volt (SE) (P1) ; Store initial voltage in Loc (61..84) 
 1: 2
 Reps

 2: 15
 2500 mV Fast Range

 3: 1
 SE Channel
 4: 61 -- Loc [ \_\_\_\_\_ ] 5: 1.0 Mult 6: 0.0 Offset 53: End (P95) 54: Do (P86) 1: 52 Set Port 2 Low 55: Timer (P26) 1: 0 Reset Timer 56: Do (P86) 1: 21 Set Flag 1 Low 57: Do (P86) 1: 12 Set Flag 2 High 58: End (P95)

59: If Flag/Port (P91) 1: 12 Do if Flag 2 is High 2: 30 Then Do 60: Set Port(s) (P20) ; **Port 1** (C1) is the heater control line 1: 0 C8..C5 = low/low/low/low 2:1 C4..C1 = low/low/low/high61: Beginning of Loop (P87) 1: 1 Delay Loop Count 2:0 62: Timer (P26) 1: 99 Loc [ \_\_\_\_\_ ] 63: If (X<=>F) (P89) ; Fire the heater for 1 s 1: 99 X Loc [\_\_\_\_\_]  $\geq =$ 2: 3 3: 1 F Change as required 4: 31 Exit Loop if True 64: End (P95) 65: Set Port(s) (P20) 1: 0 C8..C5 = low/low/low/low 2: 0 C4..C1 = low/low/low/low 66: Beginning of Loop (P87) 1: 1 Delay 2: 0 Loop Count 67: Timer (P26) 1: 99 Loc [ \_\_\_\_\_ ] 68: If (X<=>F) (P89) ; Wait 15 s for heat-pulse to arrive 1: 99 X Loc [\_\_\_\_\_ ] 2: 3 >= **F** Set Flag 5 High ; Change as required 3: 15 4: 15 69: If Flag/Port (P91) Do if Flag 5 is High Exit Loop if True 1: 15 2: 31 70: End (P95) 71: Do (P86) 1: 22 Set Flag 2 Low 72: End (P95) 73: Batt Voltage (P10) ; Store battery voltage in Loc 98 1: 98 Loc [ \_\_\_\_\_ ]

#### Appendix B - use of simple heat-pulse controller (no amplifiers)

The heat-pulse controller and probes can be operated with most Campbell data loggers. The wiring is to be connected as described below:

<u>CR10/21X/23</u>	Controller	
+12	Grey (external 12V battery)	
G	Grey/Black	
C1	Blue of controller #	¥1
AG	Blue/white "	
C2	Blue of controller #	<b>#</b> 2
AG	Blue/white "	
	Probe 1	
(1H, 1L)	Orange, Orange/white	
(2H, 2L)	Blue, Blue/white	
AG	Green <sup>1</sup>	
AG	Shield	
	Probe 2	
(3H, 3L)	Orange, Orange/white	
(4H, 4L)	Blue, Blue/white	
AG	Green <sup>1</sup>	
AG	Shield	

<sup>1</sup> **VERY IMPORTANT:** If the same battery powers the logger and the heat-pulse unit then <u>do not</u> connect the green wire of the signal lead to AG. This would cause a ground loop and might affect the results...

Listing of a CR10 logger programme to connect

```
;{CR10}
*Table 1 Program
 01: 0.2500 Execution Interval (seconds)
1: If time is (P92)
                                    ! set for 15 min intervals
1: 0Minutes (Seconds --) into a2: 15Interval (same units as above) ! change as required
3: 11
            Set Flag 1 High
2: If Flag/Port (P91)
1: 15 Do if Flag 5 is High
2: 30
            Then Do
3: Timer (P26)
                                     ! stores the time since heat-pulse
       Loc [ _____ ]
1: 99
4: Thermocouple Temp (SE) (P13) ! loc 21..28 = temperature signals
1: 8Reps2: 12.5 mV Slow Range3: 1SE Channel
```

Type T (Copper-Constantan) 4: 1 Ref Temp (Deg. C) Loc [ \_\_\_\_\_ ] 5: 100 6: 21 Loc [ \_\_\_\_\_ ] 7: 1 Mult 8: 0 Offset 5: Beginning of Loop (P87) Delay 1: 0 2: 8 Loop Count (X<=>F) (P89) ! loc 1..8 = Tz cross-over times -- X Loc [ \_\_\_\_\_ ] 6: If (X<=>F) (P89) 1: 1 = 2: 1 3: 0 F 4: 30 Then Do 7: If (X<=>Y) (P88) 1: 41 -- X Loc [ \_\_\_\_\_ ] ! loc 41..48 = original temperature 2: 3 >= 3: 21 -- Y Loc [ \_\_\_\_\_ ] ! loc 21..28 = temperatures now 4: 30 Then Do 8: Z=X (P31) 1: 99 X Loc [ \_\_\_\_\_ ] 2: 1 -- Z Loc [ \_\_\_\_\_ ] ! loc 1..8 = final Tz time 9: Z=Z+1 (P32) 1: 90 Z Loc [ \_\_\_\_\_ ] 10: End (P95) 11: End (P95) 12: End (P95) 13: If (X<=>F) (P89) X Loc [ \_\_\_\_\_ ] ! loc 90 = number of Tz recorded 1: 90 2: 3 >= 3: 8 F Set Flag 6 High 4: 16 14: If  $(X \le F)$  (P89) 1: 99 X Loc [ \_\_\_\_\_ ] 2: 3 >= 3: 500 F ! time (s) for last measurement 4: 16 Set Flag 6 High 15: End (P95) 16: If Flag/Port (P91) 1: 16 Do if Flag 6 is High 2: 30 Then Do 17: Do (P86) 1: 10 Set Output Flag High 18: Sample (P70) ! output the day and decimal hour 1: 2 Reps 2: 91 Loc [\_\_\_\_\_]

! output the cross-over times 19: Sample (P70) 1: 8 Reps 2: 1 Loc [\_\_\_\_\_] 20: Do (P86) 1: 26 Set Flag 6 Low 21: Do (P86) 1: 25 Set Flag 5 Low 22: End (P95) 23: If Flag/Port (P91) 1: 11 Do if Flag 1 is High 2: 30 Then Do 24: Time (P18) 1: 2 Hours into current year (maximum 8784) 2: 8784 Mod/Bv 3: 91 Loc [\_\_\_\_\_] ! store day of year 25: Z=X\*F (P37) 1: 91 X Loc [ \_\_\_\_\_ ] 2: .04167 F 3: 91 Z Loc [ \_\_\_\_\_ ] 26: Z=INT(X) (P45) 1: 91 X Loc [ \_\_\_\_\_ ] 2: 91 Z Loc [ \_\_\_\_\_ ] 27: Z=Z+1 (P32) 1: 91 Z Loc [ \_\_\_\_\_ ] 28: Time (P18) Hours into current year (maximum 8784) 1: 2 2: 24 Mod/By Loc [ \_\_\_\_\_ ] 3: 92 29: Z=X\*F (P37) ! store the hour 1: 92 X Loc [ \_\_\_\_\_ ] 2: 100 F 3: 92 Z Loc [ \_\_\_\_\_ ] 30: Time (P18) Minutes into current day (maximum 1440) 1: 1 2: 60 Mod/Bv Loc [ \_\_\_\_\_ ] 3: 93 

 31: Z=X+Y (P33)
 ! store the decimal hour

 1: 92
 X Loc [\_\_\_\_\_\_]

 31: Z=X+Y (P33) 2: 93 Y Loc [ \_\_\_\_\_ ] 3: 92 Z Loc [ \_\_\_\_\_ ] 32: Beginning of Loop (P87) 1: 0 Delay 2: 90 Loop Count 

 33: Z=F (P30)
 ! reset all storage

 1: 0
 F

 2: 0
 Exponent of 10

 33: Z=F (P30) 3: 1 -- Z Loc [ \_\_\_\_\_ ]

34: End (P95) 35: Thermocouple Temp (SE) (P13) ! measure initial temp difference 1: 8 Reps 2: 1 2.5 mV Slow Range 3: 1 SE Channel 4: 1 Type T (Copper-Constantan) \_\_\_\_\_] Ref Temp (Deg. C) Loc [\_\_\_\_\_ ] Loc [\_\_\_\_\_] ! loc 41..48 = initial temp difference 5: 100 6: 41 7: 1 Mult 8: 0 Offset 36: Timer (P26) 1: 0 Reset Timer 37: Do (P86) 1: 21 Set Flag 1 Low 38: Do (P86) 1: 12 Set Flag 2 High 39: End (P95) 40: If Flag/Port (P91) ! fire the heat pulse 1: 12 Do if Flag 2 is High 2: 30 Then Do 41: Set Port(s) (P20) 1: 0 C8..C5 = low/low/low/low 2: 11 C4..C1 = low/low/high/high42: Beginning of Loop (P87) 1:1 Delay 2: 0 Loop Count 43: Timer (P26) 1: 99 Loc [ \_\_\_\_\_ ] 44: If (X<=>F) (P89) ! fire heater for just 0.75 s 44: If (X<=>F) (P89) 1: 99 X Loc [\_\_\_\_\_] 2: 3 >= F 3: .75 ! change as required Exit Loop if True 4: 31 45: End (P95) 46: Set Port(s) (P20) 1: 0 C8..C5 = low/low/low/low 2: 0 C4..C1 = low/low/low/low 47: Beginning of Loop (P87) 1:1 Delay 2: 0 Loop Count 48: Timer (P26) 1: 99 Loc [ \_\_\_\_\_ ]

2: 3 >= F 3: 10 ! change as required 4: 15 Set Flag 5 High 50: If Flag/Port (P91) 1: 15Do if Flag 5 is High2: 31Exit Loop if True 51: End (P95) 52: Do (P86) 1: 22 Set Flag 2 Low 53: End (P95) 54: Batt Voltage (P10) ! store battery voltage in loc 98 1: 98 Loc [\_\_\_\_\_] \*Table 2 Program 01: 0.0000 Execution Interval (seconds) \*Table 3 Subroutines End Program \*Table 2 Program 02: 0.0000 Execution Interval (seconds) \*Table 3 Subroutines

End Program