Model 935 Quad Constant-Fraction 200-MHz Discriminator Operating and Service Manual

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Advanced Measurement Technology, Inc.

a/k/a/ ORTEC[®], a subsidiary of AMETEK[®], Inc.

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SAFETY INSTRUCTIONS AND SYMBOLS

This manual contains up to three levels of safety instructions that must be observed in order to avoid personal injury and/or damage to equipment or other property. These are:

- **DANGER** Indicates a hazard that could result in death or serious bodily harm if the safety instruction is not observed.
- **WARNING** Indicates a hazard that could result in bodily harm if the safety instruction is not observed.
- **CAUTION** Indicates a hazard that could result in property damage if the safety instruction is not observed.

Please read all safety instructions carefully and make sure you understand them fully before attempting to use this product.

In addition, the following symbol may appear on the product:





Please read all safety instructions carefully and make sure you understand them fully before attempting to use this product.

SAFETY WARNINGS AND CLEANING INSTRUCTIONS

DANGER Opening the cover of this instrument is likely to expose dangerous voltages. Disconnect the instrument from all voltage sources while it is being opened.

WARNING Using this instrument in a manner not specified by the manufacturer may impair the protection provided by the instrument.

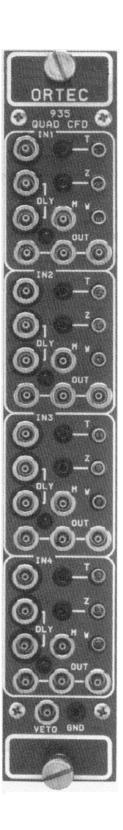
Cleaning Instructions

To clean the instrument exterior:

- Unplug the instrument from the ac power supply.
- Remove loose dust on the outside of the instrument with a lint-free cloth.
- Remove remaining dirt with a lint-free cloth dampened in a general-purpose detergent and water solution. Do not use abrasive cleaners.

CAUTION To prevent moisture inside of the instrument during external cleaning, use only enough liquid to dampen the cloth or applicator.

• Allow the instrument to dry completely before reconnecting it to the power source.





ORTEC MODEL 935 QUAD 200-MHz CONSTANT-FRACTION DISCRIMINATOR

1. DESCRIPTION

The Model 935 Quad 200-MHz Constant-Fraction Discriminator incorporates four separate and independently adjustable timing discriminators in a single-width NIM module. Except where indicated otherwise, the descriptions and specifications apply to each of the four channels in the module.

The ability of the Model 935 to provide constantfraction timing on fast, negative-polarity signals as narrow as 1 ns (FWHM) makes it ideal for use with microchannel plates, fast photomultiplier tubes, fast scintillators, and fast silicon detectors. The exceptionally low walk delivered by the Model 935 is vital in achieving the excellent time resolution inherent in these fast detectors over a wide dynamic range of pulse amplitudes. The Model 935 can also be used with scintillators such as Nal(TI) which have long decay times. To prevent multiple triggering on the long decay times, the width of the blocking output can be adjusted up to 1 μ s in duration.

The Model 935 uses the constant-fraction timing technique to select a timing point on each input pulse that is independent of pulse amplitude. When properly adjusted, the generation of the output logic pulse corresponds to the point on the leading edge of the input pulse where the input pulse has risen to 20% of its maximum amplitude. To achieve this constant-fraction triggering, the input pulse is inverted and delayed. The delay time is selected by an external delay cable (DLY) to be equal to the time taken for the input pulse to rise from 20% of maximum amplitude to maximum amplitude. Simultaneously, the prompt input signal is attenuated to 20% of its original amplitude. This attenuated signal is added to the delayed and inverted signal to form a bipolar signal with a zero crossing. The zero crossing occurs at the time when the inverted and delayed input signal has risen to 20% of its maximum amplitude. The zerocrossing discriminator in the Model 935 detects this point and generates the corresponding timing output pulse.

"Walk" is the systematic error in detecting the time for the 20% fraction as a function of input pulse amplitude. Minimizing walk is important when a wide range of pulse amplitudes must be used, because walk contributes to the time resolution. The Model 935 uses a patented transformer technique for constant-fraction shaping to achieve the exceptionally wide bandwidth essential for processing input signals with sub-nanosecond rise times. As shown in Fig. 1, this results in a walk guaranteed < ± 50 ps and typically < ± 25 ps over a I 00: 1 dynamic range of input pulse amplitudes. The patented shaping technique also provides a zero-crossing monitor output that facilitates quick and accurate walk adjustment, because it displays the full input signal amplitude range.

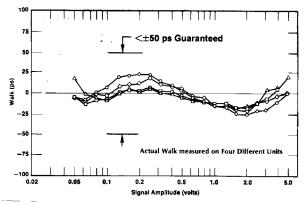


Fig. 1. Actual Walk Measured on Four Different Units. See Walk Specifications for Measurement Conditions.

The extremely short pulses from microchannel plate multipliers and ultra-fast photomultiplier tubes require very short constant-fraction shaping delays. To accommodate these detectors, the Model 935 incorporates a selectable compensation for the inherent internal delay.

The Model 935 includes a number of controls which considerably broaden its utility. The threshold discriminator is useful for rejecting low-level noise. A front-panel test point permits precise measurement of its setting in the range from -20 to -1 000 mV. Each channel provides three bridged, timing outputs. These are standard, fast negative NIM outputs. The outputs can be selected to have either updating or blocking characteristics. The updating mode is useful for reducing dead time in overlap coincidence experiments. The blocking mode simultaneously minimizes multiple triggering and dead time on scintillators with long decay times. The output pulse width is adjustable from <4 ns to >200 ns in the updating mode, and from <5 ns to > 1 μ s in the blocking mode. The pulse-pair resolution is <5 ns at minimum pulse width in the updating mode. Switches on the printed circuit board allow selection of which channels will respond to the front-panel fast-veto input. Additional fast gating capability is provided by individual gate inputs for each channel on the rear panel. The mode of these separate gate inputs can be individually selected to be either coincidence or anti-coincidence via DIP switches on the printed circuit board. Each channel ran also be programmed, for NIM bins incorporating that signal, to ignore or respond to the slow bin gate signal on pin 36 of the power connector.

2. SPECIFICATIONS

The Model 935 contains four independent and identical constant-fraction discriminators. Except where stated otherwise, the descriptions and specifications are given for an individual channel, and apply to each of the four channels.

2.1. PERFORMANCE

WALK Guaranteed < \pm 50 ps (typically < \pm 25 ps) over a 100:1 dynamic range. Measured under the following conditions: input pulse amplitude range from -50 mV to -5 V, rise time <1 ns, pulse width 10 ns, external shaping delay approximately 1.6 ns (33 cm or 13 in.), internal offset delay enabled, threshold approximately 20 mV.

CONSTANT FRACTION 20%.

PULSE-PAIR RESOLUTION <5 ns in the updating mode, <7 ns in the blocking mode.

INPUT/OUTPUT RATE Operates at burst rates >200 MHZ in the updating mode, and >150 MHZ in the blocking mode.

TRANSMISSION DELAY Typically < 13 ns with 1.6-ns external delay.

OPERATING TEMPERATURE RANGE 0 to 50 °C.

THRESHOLD TEMPERATURE SENSITIVITY <0.01%/°C, from 0 to 50°C. Threshold referenced to the -12 V supply level supplied by the NIM bin.

TRANSMISSION DELAY TEMPERATURE SENSITIVITY <±10 ps/°C from 0 to 50 °C.

2.2. CONTROLS

THRESHOLD (T) A front-panel, 20-turn screwdriver adjustment for each discriminator channel sets the minimum pulse amplitude that will produce a timing output. Variable from -20 to -1000 mV. A frontpanel test point located to the left of the threshold adjustment monitors the discriminator threshold setting. The test point voltage is 10x the actual threshold setting. Output impedance: $\leq 2 \ k\Omega$.

WALK ADJUSTMENT (Z) A front-panel, 20-turn screwdriver adjustment for fine-tuning the zerocrossing discriminator threshold to achieve minimum walk. Adjustable over a ± 15 mV range. A front-panel test point located to left of the walk adjustment monitors the actual setting of the zerocrossing discriminator. Output impedance, 1 k Ω .

OUTPUT WIDTH (W) A front-panel, 20-turn screwdriver adjustment for each discriminator channel sets the width of the three output logic pulses. The range of width adjustment depends on the positions of jumpers W2 and W3.

Table 1. The Dependence of the Output Pulse Width Range on W2 and W3 Jumper Positions.

W3 Jumper	Output Pulse Width Adjustment Range		
Position	W2 = U Updating	W2 = B Blocking	
open	<4 to >100 ns	<5 to >100 ns	
S	<4 to >200 ns	<5 to >200 ns	
S + L	Not functional	<30 ns to >400 ns	

B GATE ON/OFF Rear-panel switch turns the Bin Gate on or off for all channels programmed to accept the Bin Gate.

GATE COIN/ANTI A printed wiring board DIP switch selects either the coincidence or anticoincidence mode for the individual channel's response to the rear-panel gate input.

VETO YES/NO A printed wiring board DIP switch selects whether or not an individual channel will respond to the front-panel VETO input.

BIN GATE YES/NO A printed wiring board DIP switch selects whether or not an individual channel will respond to the bin gate signal.

INTERNAL OFFSET DELAY (WI) Printed wiring board jumper W1 is normally omitted to enable the 1.7-ns internal offset delay. This delay compensates for internal delays and makes it possible to implement the very short shaping delays required with 1-ns input pulse widths. With jumper W1 installed, the minimum shaping delay is limited by a +0.7-ns internal contribution. With W1 omitted, the internal delay contribution is effectively -1.0 ns. The Model 935 is shipped from the factory with the W1 jumper omitted. Spare jumpers for this position are located in the storage area towards the rear of the module.

UPDATING/BLOCKING MODE (W2) The printed wiring board jumper W2 selects either the updating mode (U), or the blocking mode (B) for the output pulse widths. In the blocking mode, a second input pulse will generate no output pulse if it arrives within the output pulse width W caused by a previous input pulse. In the updating mode, a second input pulse arriving within the output pulse width W from a previous pulse will extend the output pulse, from the time of arrival, by a length W. The Model 935 is shipped from the factory in the updating mode.

OUTPUT PULSE WIDTH RANGE (W3) The printed wiring board jumper W3 selects the range of output width adjustment as listed in Table 1. The Model 935 is shipped from the factory with the W3 jumper omitted. Spare jumpers for this position are located in the storage area toward the rear of the module.

2.3. INPUTS

IN1, IN2, IN3, or IN4 A front-panel LEMO connector input on each channel accepts the fast linear signal from a detector for constant-fraction timing. Linear range from 0 to -10 V. Signal input impedance, 50Ω , dc-coupled; input protected with diode clamps at ±10 V. Input reflections <10% for input rise times > 2 ns.

GATE INPUTS 1, 2, 3, or 4 A rear-panel BNC connector for each channel accepts a negative, fast NIM logic signal to gate the respective constant-fraction timing output. Coincidence or anticoincidence gating is selected by a printed wiring board DIP switch (See GATE COIN/ANTI). Input impedance, 50Ω . For proper gating operation, the leading edge of the GATE INPUT should precede the IN1 (IN2, IN3, or IN4) signal by 1 ns and have a width equal to the CF Shaping Delay plus 5 ns.

VETO A single, front-panel LEMO connector accepts NIM negative fast logic pulses to inhibit the timing outputs on all the channels chosen with the VETO YES/NO switch. Input impedance, 50Ω . For proper FAST VETO operation, the leading edge of the VETO signal must precede the IN1 (IN2, IN3, or IN4) signal by 3 ns and have a width equal to the CF Shaping Delay plus 5 ns.

BIN GATE A slow master gate signal enabled by the rear-panel B GATE ON/OFF switch permits gating off the timing outputs when the Model 935 is installed in a bin that provides a bin gate signal on pin 36 of the NIM power connector. Clamping pin 36 to ground from +5 V inhibits operation of all channels selected by the BIN GATE YES/NO switch.

2.4. OUTPUTS

CF SHAPING DELAY (DLY) A front-panel pair of LEMO connectors for selecting the required constant-fraction shaping delay. A $50-\Omega$ cable is required. For triggering at a 20% fraction, the length of the shaping delay is approximately equal to the time taken for the input pulse to rise from 20% of its full amplitude to full amplitude.

CF MONITOR (M) Permits observation of the constant-fraction shaped signal through a LEMO connector on the front panel. Output impedance,

50 Ω , ac-coupled. The monitor output is attenuated by a factor of approximately 5 with respect to the input when driving a terminated 50- Ω cable.

OUT Three bridged, updating or blocking, fast negative NIM output signals, furnished through front-panel LEMO connectors, mark the CF zerocrossing time. Amplitude -800 mV on 50- Ω load. Each output connector has its own 50- Ω resistor in series with the common output driver.

GND Front-panel test point provides a convenient ground connection for test probes.

EVENT-OCCURRED LED Front-panel LED for each channel indicates that an output signal has occurred.

2.5. ELECTRICAL AND MECHANICAL

POWER REQUIREMENTS The Model 935 derives its power from a NIM bin power supply. Required dc voltages and currents are: +12 V at 33 mA, + 6 V at 225 mA, -6V at 1400 mA, -12V at 169 mA, -24 V at 55 mA.

WEIGHT

Net 1.1 kg (2.6 lb). Shipping 2.0 kg (4.4 lb)

DIMENSIONS NIM-standard single-width module 3.43 x 22.13 cm (1.35 x 8.714 in.) per TID-20893 (Rev).

3. INSTALLATION

3.1. GENERAL

The Model 935 power requirements must be furnished from a NIM-standard bin and power supply that includes ± 6 V power distribution such as the ORTEC 4001C/4002E, 4001C/4002D, or 4001A/4002D NIM Bins/Power Supplies.

The bin and power supply in which the Model 935 will normally be operated is designed for relay rack mounting. If the equipment is rack mounted, be sure that there is adequate ventilation to prevent any localized heating in the Model 935. The temperature of equipment mounted in racks can easily exceed the maximum limit of 50 °C (323 K) unless precautions are taken.

3.2. CONNECTION TO POWER

Due to the very high speed electronic components used in the Model 935 to achieve its excellent performance, the Model 935 exceeds the normal fair share of power per slot of normal NIM power supplies. As many as eight Model 935s, a total of 32 channels, can be operated in a ORTEC 4002C/4002E NIM Bin/Power Supply. To be sure of proper operation, check the de voltage levels of the power supply after all modules have been installed in the bin. ORTEC bins and power supplies include convenient test points on the power supply control panel to permit monitoring these levels.

3.3. INPUT CONNECTIONS

Each discriminator channel includes an input connector on the front panel that is terminated internally in 50 Ω . Connect the source of negative input signals to this connector through a 50 Ω coaxial cable and a mating LEMO connector. Any of the four channels can be provided with an input signal and will operate independently from all other channels.

3.4. OUTPUT CONNECTIONS

There are three output connectors for each channel. These connectors furnish three identical, simultaneous, negative NIM logic signals for each input pulse that exceeds the adjusted threshold level. The output pulse width can be adjusted by the front-panel W control associated with that channel. When operating in the updating mode, the range of width adjustment can be increased by adding a PWB jumper to the "S" pins at W3. When operating in the blocking mode, the range of width adjustment can be increased by adding jumpers to either or both the "S" and "L" pins at W3.

Each output connection should be furnished through a mating LEMO connector and a $50-\Omega$ coaxial cable to a $50-\Omega$ load impedance. For best results, terminate all unused output connectors in each active channel with a $50-\Omega$ terminator on the front panel. Termination is not necessary for unused channels.

3.5. GATING

Each channel of the Model 935 can be externally gated by one of three conditions. A front-panel Veto input can block the output. Each channel can be separately gated by rear-panel Gate inputs. A NIM bin signal, the B (bin) Gate operating through pin 36 of the power connector in the NIM bin, can inhibit an output, providing that the rear-panel B Gate switch is set to On. The gating conditions for each channel of the Model 935 are controlled by PWB DIP switches. The Veto input can be selected as either Yes or No, the Gate input can be selected as either Coincidence or Anticoincidence, and the B Gate can be selected as either Yes or No.

For proper gating operation, certain timing conditions must be satisfied between the leading edge of the input signal and the gating signal. When using the front-panel fast Veto input, its leading edge should precede the input signal by 3 ns, and its width should be equal to the CF shaping delay plus 5 ns. When using the rear-panel Gate input, its leading edge should precede the input signal by 1 ns, and its width should be equal to the CF shaping delay plus 5 ns. The B (bin) Gate signal is a slow logic signal, and it must overlap the input signal to be effective.

3.6. CF SHAPING DELAY CABLE SELECTION

The CF shaping delay for each channel is adjusted by selecting an appropriate length of $50-\Omega$ coaxial cable and adding it between the two Delay (DLY) LEMO connectors on the front panel. The length of cable determines the amount of external signal delay that is added to the internal delay to constitute the total constant-fraction shaping delay. Since the Model 935 is equipped with a jumperselectable internal offset delay, the external CF shaping delay will depend on the position of internal jumper W1. With jumper W1 removed (placed in the storage area at the rear of the PWB), the total constant-fraction shaping delay, $t_{d(Total)}$, is approximated by

 $t_{d(Total)} \sim t_{d(External)}$ - 1.0 ns, W1 removed. (3.1)

$$t_{d(Total)} \sim t_{d(External)} + 0.7 \text{ ns}, W1 \text{ in place.}$$
 (3.2)

The primary usage of the Model 935 is expected to be in fast timing or counting experiments with scintillators and photomultiplier tubes (PMTs) and Silicon Surface Barrier Detectors. In these applications, the CF Shaping Delay $t_{d(Total)}$ is selected so that the zero-crossing of the bipolar timing signal occurs just as the peak of the attenuated, undelayed portion of the CF signal has reached its maximum amplitude. Thus, the zero-crossing occurs at the same fraction of the input pulse height, regardless of the amplitude of the input signal.

Selection of the CF Shaping Delay for best timing performance with a given scintillator and PMT is usually accomplished experimentally. The randomly generated signals from the anode of the PMT are applied to the input of one channel of the discriminator. Each of the two CF Delay connectors should be terminated with a 50- Ω terminator. The CF Monitor signal can be observed on a fast oscilloscope (bandwidth > 300 MHZ), which is terminated in 50- Ω and triggered internally. The Monitor signal represents the attenuated, undelayed portion of the constant-fraction signal with no delayed signal subtracted from it. The addition of the appropriate external CF Shaping Delay $t_{d(External)}$ causes the resulting bipolar signal at the CF Monitor to cross the baseline at the peak of the attenuated, undelayed signal. When using the internal offset delay (i.e., jumper W1 removed), a useful formula for the initial trial selection of the CF Shaping Delay is

 $t_{d(External)} = T + 1.0 \text{ ns}, W1 \text{ removed},$ (3.3)

where T is the time for the leading edge of the pulse to rise from 20% of maximum amplitude to maximum amplitude. The 20% number corresponds to the 20% triggering fraction designed into the Model 935. With jumper W1 in place (i.e., when not using the internal offset delay), a useful formula for the initial trial selection of the CF Shaping Delay is

$$t_{d(External)} = T - 0.7 \text{ ns}, W1 \text{ in place}.$$
 (3.4)

In normal operation, jumper W1 is removed and placed in the storage area at the rear of the PWB. This setting will work properly for all input signals. The Model 935 is shipped with jumper W1 in the storage area. For input signals having rise times greater than 2 ns, jumper W1 can be used to short the internal offset delay, allowing for shorter external CF Shaping Delays.

3.7. WALK SETTING

The Walk adjustment is a front-panel, 20-turn screwdriver adjusted potentiometer for each channel. A Walk Monitor front-panel test point is used to monitor the actual setting of the dc zerocrossing adjustment. A nominal value for this dc level is +1.5 mV, but the optimal value is best determined experimentally.

Walk adjustment can be accomplished while observing the delayed CF Monitor signal on a fast oscilloscope (bandwidth >300 MHZ), which is triggered externally by the output signal of the Model 935. The Walk potentiometer (Z) should be adjusted so that the bipolar constant-fraction signals for all amplitudes cross through the baseline at approximately the same time.

Figure 3(a) shows the anode signals from a Hamamatsu 1332 PMT with a 12.9-cc BC418 truncated cone scintillator exposed to a 60Co source. Figure 3(b) shows the delayed CF Monitor signal triggered by the Model 935 output signal with the walk properly adjusted. Adjusting the Walk potentiometer counterclockwise results in the waveform shown in Figure 3(c), where the extra line near the baseline indicates leading-edge timing. Proper Walk adjustment can be achieved by adjusting the Walk potentiometer counter-clockwise to obtain the waveform shown in Figure 3(c), then turning the Walk adjustment clockwise to just eliminate the leading-edge timing line. An additional 1 to 2 turns clockwise should give the waveform in Figure 3(b) and optimum walk adjustment. The final optimization of the Walk adjustment is best accomplished by optimizing the symmetry and minimizing the width of the coincidence peak in the time spectrum (see Section 4).

4. OPERATING INSTRUCTIONS

4.1. GENERAL

The actual timing performance of a timing system depends on many variables. The type of detector and the energy range of interest are two important system variables that are independent of the electronics. In general, detectors having fast rise time signals and higher energies give the best timing performance.

A simple timing system is shown in Figure 4. This system consists of two detectors each with their own high voltage supply, two Model 935 CFDs, a Delay unit for timing calibration and signal offset, a Time-to-Amplitude Converter (TAC) and a multichannel analyzer (MCA). Also shown is a Preamplifier (PA), a spectroscopy amplifier (Amp), and a Gate and Delay Generator (GDG) used for energy calibration.

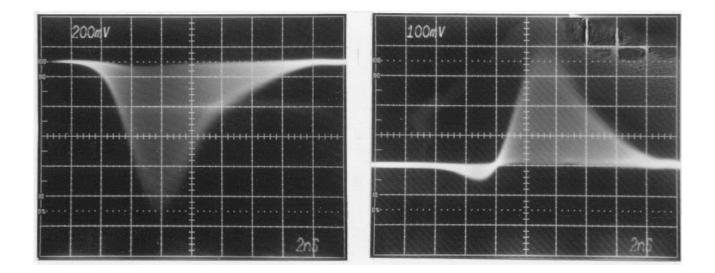
The detectors shown in Figure 4 consist of fast scintillators mounted on fast photomultiplier tubes (PMTs). Each PMT is connected to a PMT Base for distribution of the high voltage. Care must be taken in preparing and mounting the scintillator to ensure very efficient coupling between the scintillator and the PMT.

The high voltage setting for the PMT depends on the type of PMT, and the manufacturer of the PMT should be consulted. The gain of the PMT depends directly on the value of the high voltage and provides a convenient method for adjusting the output signal amplitude from the PMT. In general, the high voltage should be set sufficiently high to ensure a large signal input to the CFD. However, the high voltage should not be set so high as to cause the onset of saturation in the PMT. The final adjustment of the high voltage is a compromise that can best be determined experimentally.

4.2. THRESHOLD ADJUSTMENT

The Model 935 will produce an output signal each time the input signal crosses the threshold. Setting the threshold is equivalent to setting the lowest energy of interest. While it is possible to set the threshold using an oscilloscope, a far more accurate method is to use the actual detector, a radioactive source, and an MCA gated by the Model 935. A Gate and Delay Generator is used to convert the Model 935 output to a signal suitable for gating the MCA.

To adjust the threshold level, measure the dc voltage from the front-panel Threshold monitor test point to ground for the active channel. The Threshold monitor test point is located to the left of the threshold potentiometer on the front panel. A convenient ground test point is located at the



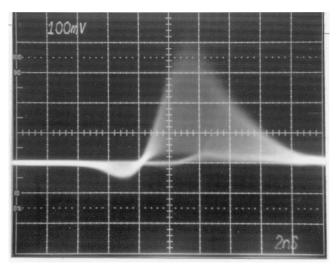


Fig. 3. (a) Anode signal from PMT and scintillator, (b) the Model 935 CF Monitor signal showing proper walk adjustment, and (c) the Model 935 CF Monitor signal showing improper walk adjustment. See text for discussion.

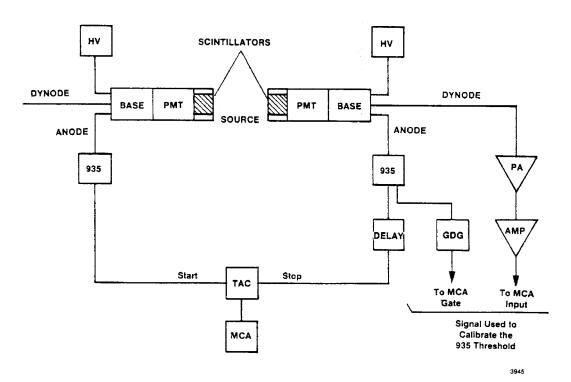


Fig. 4. A Simple Timing System.

bottom of the front panel to the right of the Veto Input connector. The nominal range of voltages at the Threshold test point is -200 mV to -10 V, corresponding to the actual threshold which is 10%of the test point voltage. Use a screwdriver to set the threshold level with the control marked T.

4.3. OUTPUT WIDTH ADJUSTMENT

To adjust the output width, provide an input pulse that exceeds the adjusted threshold at a rate less than 0.5 MHZ and observe the width of an output pulse from any of the three output connectors. Terminate the other output connectors in 50 Ω . Use a screwdriver to set the control marked W for the output width in the active channel. When operating in the Updating mode, the output width can be adjusted from <4 ns to >100 ns. Adding a PWB jumper to the S position of W3 changes the range of adjustment to >200 ns. When operating in the blocking mode, an additional jumper can be added to the L position of W3, increasing the Blocking output width to > 1000 ns.

4.4. CONSTANT-FRACTION SHAPING DELAY ADJUSTMENT

Selection of the initial value for the CF Shaping Delay is described in Section 3.6. For input signals

having widths approaching 1 ns, it is necessary to fine tune the CF Shaping Delay to achieve optimum performance. The optimum value is determined for a given detector using the timing system shown in Figure 4. Repeated measurements of timing resolution FWHM and FWHM are made as a function of CF Shaping Delay length to determine the optimum value of the CF Shaping Delay.

4.5. WALK ADJUSTMENT

To adjust the Walk characteristics, connect the signal source to be used to the Input connector in the active channel and connect the signal from the constant-fraction Monitor connector to a fast oscilloscope (bandwidth greater than 300 MHZ) through a 50- Ω delay. Select the CF Shaping Delay according to the information in Section 3.6. The constant-fraction shaped signal can be observed on the oscilloscope, triggered by an undelayed output signal from the active discriminator. Adjust the Walk (Z) control, which sets the zero-crossing reference, so that the bipolar constant-fraction signals for all input amplitudes cross through the baseline at approximately the same time. The adjacent test point can be used for resettability of the zero-crossing reference. Under most operating conditions, the dc voltage level at the test point should be in the range from -1.0 mV to +2.0 mV. Use a screwdriver to adjust the Z control.

4.6. GATING ADJUSTMENTS

The gating conditions for each channel of the Model 935 are set by PWB DIP switches located near the rear panel of the Model 935. The DIP switches located nearest the top of the module set the Gate input to operate in either the Anticoincidence mode or the Coincidence mode. In the Anticoincidence mode, a Gate input that satisfies the timing conditions relative to the Input signal blocks the output of that channel. In the Coincidence mode, a Gate input enables the output of that channel. If no Gate input is to be used, place the DIP switch in the Anticoincidence position. The middle set of DIP switches controls the front-panel fast Veto input. With the DIP switch corresponding to a given channel in the On position, the fast Veto signal can block or veto the output of that channel, providing that the timing conditions of the fast Veto input relative to the Input are satisfied. The lowest set of DIP switches controls the bin gate input. The bin gate DIP switches are effective only K the rearpanel B Gate switch is in the On position. With the B Gate switch in the On position, and the DIP switch in the On position, a bin gate blocks the output of the corresponding channel, provided that the timing conditions relative to the input signal are satisfied. The timing conditions for all the gating inputs are described in Section 3.5.

5. THEORY OF OPERATION

Figure 5 is a simplified block diagram of the instrument that can be used as a reference to describe how it operates.

An input of 0 to -10 V amplitude starts at time zero and is applied to the 50- Ω Splitter. One output of the Splitter is delayed by the internal offset delay DL1 before it is applied to the leading-edge arming discriminator (LEAD) and the CF attenuator, ATTN. The ATTN circuit sets the constant-fraction attenuation factor of f = 0.2, and its output is applied to the transformer, XFMR. The second output of the Splitter is delayed by the external CF Shaping Delay and applied to the second input to the XFMR. The XFMR output is a bipolar-shaped signal whose zero-crossing time is used to derive the Model 935 output. This signal is amplified by the constant-fraction amplifier (CFA) prior to being connected to the zero-crossing gate GI.

The LEAD has an adjustable threshold, ranging from -20 mV to -1 V, that determines the minimum input signal amplitude that is required to produce an output pulse from the Model 935. If the input

signal exceeds the LEAD threshold, that comparator produces an output pulse that arms zero-crossing gate G1.

The timing logic signal from gate G1 triggers a fast one-shot, comprised of an ECL type D masterslave flip-flop FF1 and a stretcher circuit. All gating input signals are ORed by G2 and applied to the D input of FF1. One output of FF1 drives A2, which controls the front-panel event LED. The other output of FF1 drives the stretcher circuit, which controls the width of the output signals.

The output driver circuit provides a fast voltage output signal that is capable of driving three $50-\Omega$ loads simultaneously with NIM-standard negative fast logic pulses. The output signals are either updating or blocking, depending on the setting of PWB jumper W2.

The dc power requirements are shown in the specifications in Section 2. The power levels are +6 V, -6 V, +12 V, -1 2 V, and -24 V, and they are all obtained directly from the bin power supply.

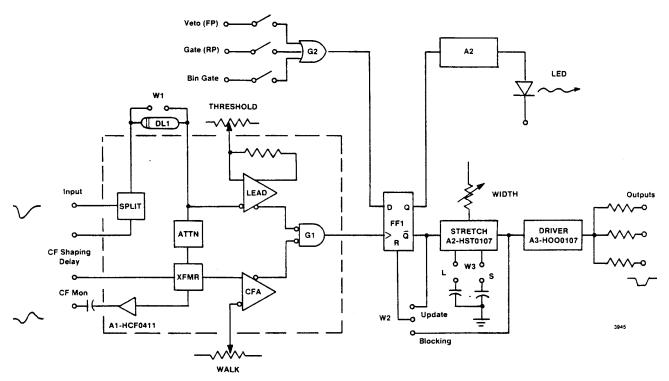


Fig. 5. Simplified Block Diagram of One Section of the Model 935.

6. MAINTENANCE

6.1. CALIBRATION

Most adjustments to the Model 935 are made via front-panel controls. The only internal adjustment is the Threshold Cal potentiometer, R. Should recalibration be required, connect a 50-mV, 20-nswide signal to the input of the section being adjusted. Adjust the front-panel Threshold potentiometer such that the front-panel Threshold Test Point reads 500 mV. Adjust the Threshold Cal potentiometer so that the Model 935 output halffires.

6.2. TYPICAL DC VOLTAGES

All voltages listed on the schematic drawing are measured with respect to ground, with the

Threshold and Width controls set at minimum, and the Walk set at + 1.5 mV.

6.3. FACTORY SERVICE

This instrument can be returned to the ORTEC factory for service and repair at a nominal cost. The ORTEC standard procedure for repair ensures the same quality control and checkout that are used for a new instrument. Always contact Customer Services at ORTEC before sending an instrument for repair to obtain shipping instructions and so that the required Return Authorization Number can be assigned to the unit. This number should be written on the address label and on the package.

Pin	Function	Pin	Function
1	+3 V	23	Reserved
2	-3 V	24	Reserved
3	Spare bus	25	Reserved
4	Reserved bus	26	Spare
5	Coaxial	27	Spare
6	Coaxial	*28	+24 V
7	Coaxial	*29	–24 V
8	200 V dc	30	Spare bus
9	Spare	31	Spare
10	+6 V	32	
11	-6 V	*33	117 V ac (hot)
12	Reserved bus	*34	Power return ground
13	Spare	35	Reset (Scaler)
14	Spare	36	Gate
15	Reserved	37	Reset (Auxiliary)
*16	+12 V	38	Coaxial
*17	–12 V	39	Coaxial
18	Spare bus	40	Coaxial
19	Reserved bus	*41	117 V ac (neutral)
20	Spare	*42	High-quality ground
21	Spare	G	Ground guide pin
22	Reserved		

 Table 2. Bin/Module Connector Pin Assignments For Standard

 Nuclear Instrument Modules per DOE/ER-0457T.

Pins marked (*) are installed and wired in ORTEC's 4001A and 4001C Modular System Bins.

