

EUMETSAT Satellite Application Facility on
Support to Operational Hydrology and Water Management



**Product Validation Report (PVR-02)
for product H02 (PR-OBS-2)**

**Precipitation rate at ground by MW cross-track scanners (with
indication of phase)**

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DOCUMENT CHANGE RECORD

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1.1	30/09/2011	Updates, acknowledging ORR1 Part 2 review board recommendation
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Acronyms

AMSU	Advanced Microwave Sounding Unit (on NOAA and MetOp)
AMSU-A	Advanced Microwave Sounding Unit - A (on NOAA and MetOp)
AMSU-B	Advanced Microwave Sounding Unit - B (on NOAA up to 17)
ATDD	Algorithms Theoretical Definition Document
AU	Anadolu University (in Turkey)
BfG	Bundesanstalt für Gewässerkunde (in Germany)
CAF	Central Application Facility (of EUMETSAT)
CDOP	Continuous Development-Operations Phase
CESBIO	Centre d'Etudes Spatiales de la BIOSphere (of CNRS, in France)
CM-SAF	SAF on Climate Monitoring
CNMCA	Centro Nazionale di Meteorologia e Climatologia Aeronautica (in Italy)
CNR	Consiglio Nazionale delle Ricerche (of Italy)
CNRS	Centre Nationale de la Recherche Scientifique (of France)
DMSP	Defense Meteorological Satellite Program
DPC	Dipartimento Protezione Civile (of Italy)
EARS	EUMETSAT Advanced Retransmission Service
ECMWF	European Centre for Medium-range Weather Forecasts
EDC	EUMETSAT Data Centre, previously known as U-MARF
EUM	Short for EUMETSAT
EUMETCast	EUMETSAT's Broadcast System for Environmental Data
EUMETSAT	European Organisation for the Exploitation of Meteorological Satellites
FMI	Finnish Meteorological Institute
FTP	File Transfer Protocol
GEO	Geostationary Earth Orbit
GRAS-SAF	SAF on GRAS Meteorology
HDF	Hierarchical Data Format
HRV	High Resolution Visible (one SEVIRI channel)
H-SAF	SAF on Support to Operational Hydrology and Water Management
IDL [®]	Interactive Data Language
IFOV	Instantaneous Field Of View
IMWM	Institute of Meteorology and Water Management (in Poland)
IPF	Institut für Photogrammetrie und Fernerkundung (of TU-Wien, in Austria)
IPWG	International Precipitation Working Group
IR	Infra Red
IRM	Institut Royal Météorologique (of Belgium) (alternative of RMI)
ISAC	Istituto di Scienze dell'Atmosfera e del Clima (of CNR, Italy)
ITU	İstanbul Technical University (in Turkey)
LATMOS	Laboratoire Atmosphères, Milieux, Observations Spatiales (of CNRS, in France)
LEO	Low Earth Orbit
LSA-SAF	SAF on Land Surface Analysis
Météo France	National Meteorological Service of France
METU	Middle East Technical University (in Turkey)
MHS	Microwave Humidity Sounder (on NOAA 18 and 19, and on MetOp)
MSG	Meteosat Second Generation (Meteosat 8, 9, 10, 11)
MVIRI	Meteosat Visible and Infra Red Imager (on Meteosat up to 7)
MW	Micro Wave
NESDIS	National Environmental Satellite, Data and Information Services
NMA	National Meteorological Administration (of Romania)
NOAA	National Oceanic and Atmospheric Administration (Agency and satellite)
NWC-SAF	SAF in support to Nowcasting & Very Short Range Forecasting
NWP	Numerical Weather Prediction
NWP-SAF	SAF on Numerical Weather Prediction

O3M-SAF	SAF on Ozone and Atmospheric Chemistry Monitoring
OMSZ	Hungarian Meteorological Service
ORR	Operations Readiness Review
OSI-SAF	SAF on Ocean and Sea Ice
PDF	Probability Density Function
PEHRPP	Pilot Evaluation of High Resolution Precipitation Products
Pixel	Picture element
PMW	Passive Micro-Wave
PP	Project Plan
PR	Precipitation Radar (on TRMM)
PUM	Product User Manual
PVR	Product Validation Report
RMI	Royal Meteorological Institute (of Belgium) (alternative of IRM)
RR	Rain Rate
RU	Rapid Update
SAF	Satellite Application Facility
SEVIRI	Spinning Enhanced Visible and Infra-Red Imager (on Meteosat from 8 onwards)
SHMÚ	Slovak Hydro-Meteorological Institute
SSM/I	Special Sensor Microwave / Imager (on DMSP up to F-15)
SSMIS	Special Sensor Microwave Imager/Sounder (on DMSP starting with S-16)
SYKE	Suomen ympäristökeskus (Finnish Environment Institute)
T _{BB}	Equivalent Blackbody Temperature (used for IR)
TKK	Teknillinen korkeakoulu (Helsinki University of Technology)
TMI	TRMM Microwave Imager (on TRMM)
TRMM	Tropical Rainfall Measuring Mission UKMO
TSMS	Turkish State Meteorological Service
TU-Wien	Technische Universität Wien (in Austria)
U-MARF	Unified Meteorological Archive and Retrieval Facility
UniFe	University of Ferrara (in Italy)
URD	User Requirements Document
UTC	Universal Coordinated Time
VIS	Visible
ZAMG	Zentralanstalt für Meteorologie und Geodynamik (of Austria)

1 The EUMETSAT Satellite Application Facilities and H-SAF

The “EUMETSAT Satellite Application Facility on Support to Operational Hydrology and Water Management (H-SAF)” is part of the distributed application ground segment of the “European Organisation for the Exploitation of Meteorological Satellites (EUMETSAT)”. The application ground segment consists of a “Central Application Facility (CAF)” and a network of eight “Satellite Application Facilities (SAFs)” dedicated to development and operational activities to provide satellite-derived data to support specific user communities. See fig. 1.

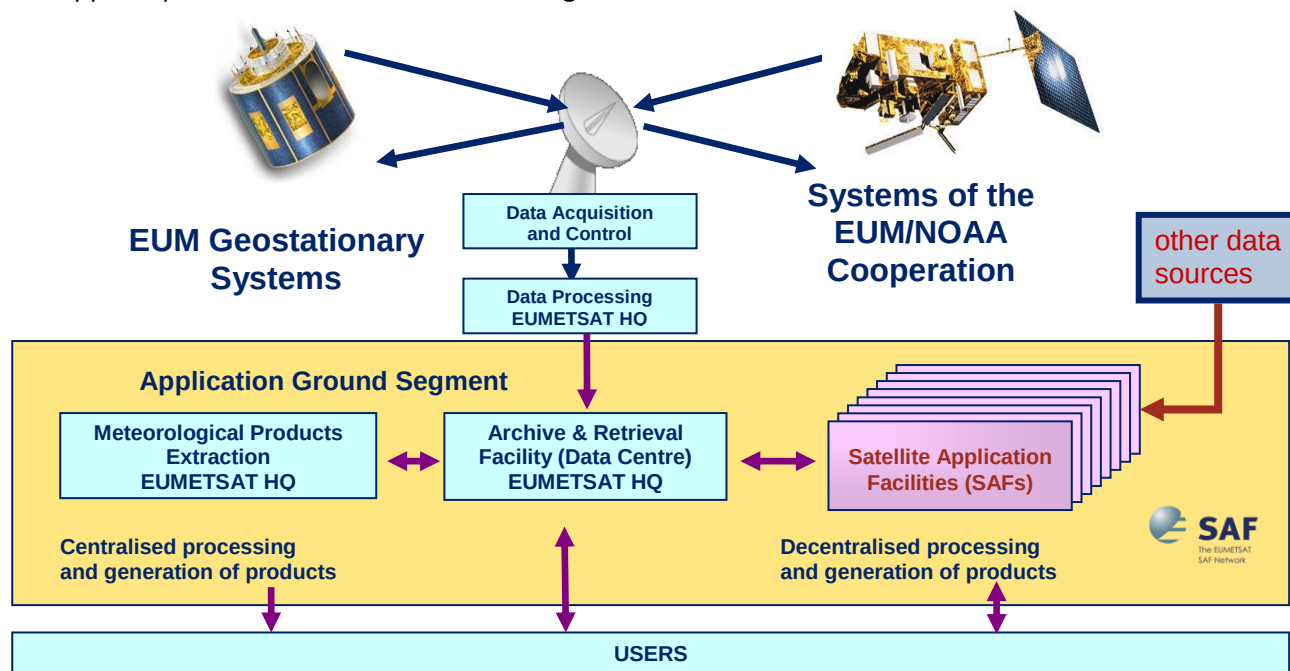


Figure 1 Conceptual scheme of the EUMETSAT application ground segment

Next figure reminds the current composition of the EUMETSAT SAF network (in order of establishment).

							
NWC SAF	OSI SAF	O3M SAF	CM SAF	NWP SAF	GRAS SAF	LSA SAF	H SAF
Nowcasting & Very Short Range Forecasting	Ocean and Sea Ice	Ozone & Atmospheric Chemistry Monitoring	Climate Monitoring	Numerical Weather Prediction	GRAS Meteorology	Land Surface Analysis	Operational Hydrology & Water Management

Figure 2 Current composition of the EUMETSAT SAF network (in order of establishment)

Conceptual scheme of the EUMETSAT application ground segment

The H-SAF was established by the EUMETSAT Council on 3 July 2005; its Development Phase started on 1st September 2005 and ended on 31 August 2010. The SAF is now in its first Continuous Development and Operations Phase (CDOP) which started on 28 September 2010 and will end on 28 February 2012. The list of H-SAF products is shown in Table 1:

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Acronym	Identifier	Name
PR-OBS-1	H-01	Precipitation rate at ground by MW conical scanners (with indication of phase)
PR-OBS-2	H-02	Precipitation rate at ground by MW cross-track scanners (with indication of phase)
PR-OBS-3	H-03	Precipitation rate at ground by GEO/IR supported by LEO/MW
PR-OBS-4	H-04	Precipitation rate at ground by LEO/MW supported by GEO/IR (with flag for phase)
PR-OBS-5	H-05	Accumulated precipitation at ground by blended MW and IR
PR-OBS-6	H-15	Blended SEVIRI Convection area/ LEO MW Convective Precipitation
PR-ASS-1	H-06	Instantaneous and accumulated precipitation at ground computed by a NWP model
SM-OBS-2	H-08	Small-scale surface soil moisture by radar scatterometer
SM-OBS-3	H-16	Large-scale surface soil moisture by radar scatterometer
SM-DAS-2	H-14	Liquid root zone soil water index by scatterometer assimilation in NWP model
SN-OBS-1	H-10	Snow detection (snow mask) by VIS/IR radiometry
SN-OBS-2	H-11	Snow status (dry/wet) by MW radiometry
SN-OBS-3	H-12	Effective snow cover by VIS/IR radiometry
SN-OBS-4	H-13	Snow water equivalent by MW radiometry

Table 1 H-SAF Product List

2 Introduction to product PR-OBS-1

2.1 Sensing principle

Product PR-OBS-2 is based on the instruments AMSU-A and AMSU-B or MHS flown on NOAA and MetOp satellites. These cross-track scanners provide images with constant angular sampling across track, that implies that the IFOV elongates as the beam moves from nadir toward the edge of the scan (see next figure). The elongation is such that:

- for AMSU-A the IFOV at nadir is: $48 \times 48 \text{ km}^2$, at the edge of the 2250 km swath: $80 \times 150 \text{ km}^2$;
- for AMSU-B and MHS the IFOV at nadir is: $16 \times 16 \text{ km}^2$; at the edge: $27 \times 50 \text{ km}^2$.

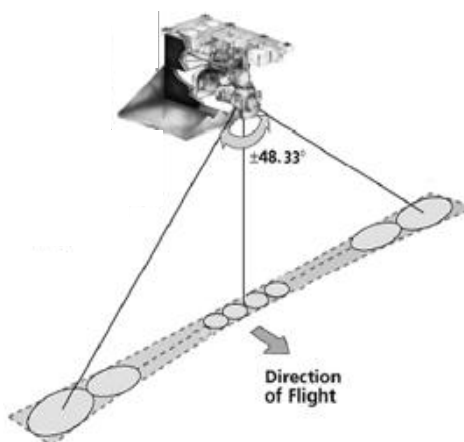


Figure 3 Geometry of cross-track scanning for AMSU

Since the incidence angle changes moving cross-track, the effect of polarisation also changes, thus the information stemming from dual polarisation would be very difficult to be used, and in effect the various frequencies are observed under a single polarisation, V or H. The resolution is constant for all frequencies in AMSU-A (48 km at s.s.p.) and AMSU-B/MHS (16 km at s.s.p.).

The NOAA satellites are managed by NOAA, MetOp by EUMETSAT. Both NOAA and MetOp provide direct-read-out (the real-time transmitter of MetOp suffered of a failure, but now transmission of data over Europe has been resumed).

For more information, please refer to the Products User Manual (specifically, volume PUM-02).

2.2 Algorithm principle

The baseline algorithm for PR-OBS-2 processing is described in ATDD-02. Only essential elements are highlighted here.

Next figure illustrates the flow chart of the AMSU-MHS processing chain.

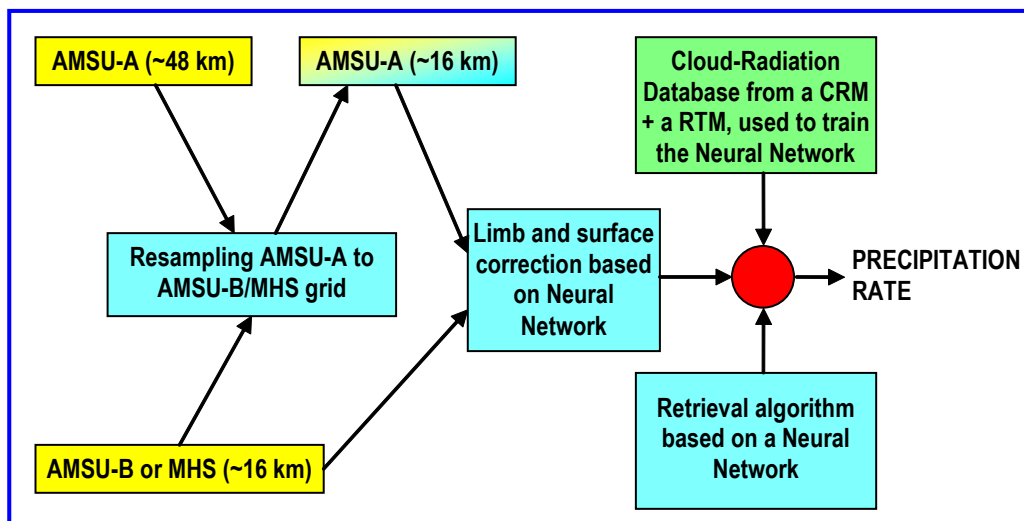


Figure 4 Flow chart of the AMSU-MHS precipitation rate processing chain

The first step is to resample AMSU-A brightness temperature (TB) to AMSU-B/MHS grid using bilinear interpolation. Then AMSU-A and AMUS-B/MHS radiometers are corrected for limb and surface effects, to report the viewing geometry changing across the image, to vertical viewing. This is obtained by applying procedures based on specific Neural Networks (one Net for each channel). The instantaneous rain field is finally retrieved by using a Neural Network on the corrected TBs.

In the initial product release the Neural Network had been trained by selected radars of the NEXRAD network. In the current release the Neural Network is trained by a Cloud-Radiation Database (CRD) built by applying a Radiative Transfer Model (RTM) to simulated cloud systems derived by a Cloud Resolving Model (CRM).

2.3 Main operational characteristics

The operational characteristics of PR-OBS-2 are discussed in PUM-02. Here are the main highlights.

The horizontal resolution (Δx) descends from the instrument Instantaneous Field of View (IFOV). AMSU-A and AMSU-B/MHS have constant resolution with frequency (different for AMSU-A, 48 km at nadir, and AMSU-B/MHS, 16 km at nadir), degrading across-scan (80 x 150 and 27 x 50 km² respectively, at the very edge of scan). Lower resolution AMSU-A data are resampled over the AMSU-B/MHS grid by means of bilinear interpolation. As a whole, a representative value for the final product could be ~ 40 km. Sampling is made at ~ 16 km intervals, the AMSU-B/MHS resolution at nadir. Thus:

- resolution $\Delta x \sim 40$ km - sampling distance: 16 km.

The observing cycle (Δt) is defined as the average time interval between two measurements over the same area. In the case of LEO, the observing cycle depends on the instrument swath and the number of satellites carrying the addressed instrument. For PR-OBS-2 there are one MetOp (orbit: 9:30 LST) and up to 5 NOAA satellites. However, AMSU-MHS on NOAA is in a good status only for NOAA-18 and NOAA-19, that follow approximately the same orbit, close to 14:00 LST. Therefore the total service is equivalent to that one of two satellites, around 9:30 and 14:00 LST. In average the observing cycle over Europe is $\Delta t \sim 6$ h, with actual interval ranging from 4.5 to 7.5 hours. Gaps are filled by product PR-OBS-1, that also has observing cycle $\Delta t \sim 6$ h, but LST around 7:00 and 18:00, with actual intervals ranging from 2 to 10 hours. The conclusion is:

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- for PR-OBS-2 as stand alone (from NOAA & MetOp satellites): cycle $\Delta t = 6$ h, sampling $4.5 \div 7.5$ h;
- for the composite PR-OBS-1 + PR-OBS-2 system: cycle $\Delta t = 3$ h, sampling $2 \div 4.5$ h.

The *timeliness (δ)* is defined as the time between observation taking and product available at the user site assuming a defined dissemination mean. The timeliness depends on the satellite transmission facilities, the availability of acquisition stations, the processing time required to generate the product and the reference dissemination means. Direct-read-out is provided by all NOAA satellites and, after partial recovery from the AHRPT transmitter failure, also by MetOp-A. After adding the processing time we have:

- timeliness $\delta \sim 0.5$ h.

The *accuracy (RMS)* is the convolution of several measurement features (random error, bias, sensitivity, precision, ...). To simplify matters, it is generally agreed to quote the root-mean-square difference [observed - reference values]. The accuracy of a satellite-derived product descends from the strength of the physical principle linking the satellite observation to the natural process determining the parameter. It is difficult to be estimated *a-priori*: it is generally evaluated *a-posteriori* by means of the *validation activity*.

3 Validation strategy, methods and tools

3.1 Validation team and work plan

To evaluate the satellite precipitation product accuracy a Validation Group has been established by the beginning of the Validation Phase in the H-SAF project. The Precipitation Product Validation team is composed of experts from the National Meteorological and Hydrological Institutes of Belgium, Bulgaria, Germany, Hungary, Italy, Poland, Slovakia, and Turkey (fig. 5). Hydrologists, meteorologists, and precipitation ground data experts, coming from these countries are involved in the product validation activities (Table 2).

H01 has been submitted to validation in all these countries except Bulgaria. Until now the Bulgarian data are used only for H05 validation activity according to the Project Plan. Their use in the next months is under consideration.

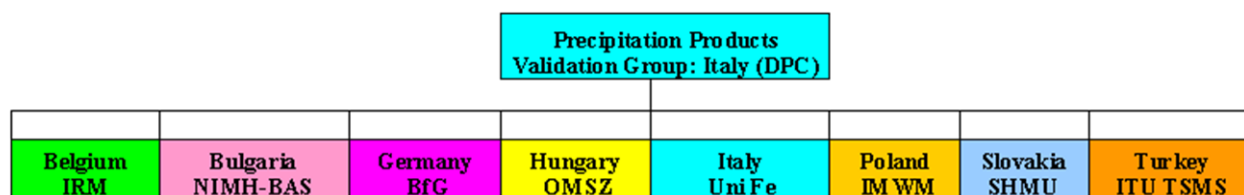


Figure 5 Structure of the Precipitation products validation team

Validation team for precipitation products			
Silvia Puca (Leader)	Dipartimento Protezione Civile (DPC)	Italy	silvia.puca@protezionecivile.it
Emanuela Campione	Dipartimento Protezione Civile (DPC)	Italy	emanuela.campione@protezionecivile.it
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Alexander Toniazzo	Dipartimento Protezione Civile (DPC)	Italy	alexander.toniazzo@protezionecivile.it
Emmanuel Roulin	Institut Royal Météorologique (IRM)	Belgium	Emmanuel.Roulin@oma.be

 The EUMETSAT Network of Satellite Application Facilities HSAF Support to Operational Hydrology and Water Management	Product Validation Report - PVR-02 (Product H02 – PR-OBS-2)	Doc.No: SAF/HSAF/PVR-02/1.1 Issue/Revision Index: 1.1 Date: 30/09/2011 Page: 19/177
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Table 2 List of the people involved in the validation of H-SAF precipitation products

The Precipitation products validation programme started with a first workshop in Rome, 20-21 June 2006, soon after the H-SAF Requirements Review (26-27 April 2006). The first activity was to lay down the Validation plan, that was finalised as first draft early as 30 September 2006. After the first Workshop, other ones followed, at least one per year to exchange experiences, problem solutions and to discuss possible improvement of the validation methodologies. Often the Precipitation Product Validation workshop are joined with the Hydrological validation group.

The results of the Product Validation Programme are reported in this Product Validation Report (PVR) and are published in the validation section of the H-SAF web page. A new structure and visualization of the validation section of H-SAF web page is in progress to take into account the user needs. This validation web section is continuously updated with the last validation results and studies coming from the Precipitation Product Validation Group (PPVG).

In the last Validation Workshop hosted by Slovenský Hydrometeorologický Ústav in Bratislava, 20-22 October 2010 it has been decided to introduce several Working Groups to solve specific items of validation procedure and to develop software used by all members of the validation cluster. The coordinators and the participants of the working groups are members of the PPVG or external experts

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of the institutes involved in the validation activities. The first results obtained by the Working Groups are here reported.

3.2 Validation objects and problems

The products validation activity has to serve multiple purposes:

- to provide input to the product developers for improving calibration for better quality of baseline products, and for guidance in the development of more advanced products;
- to characterise the product error structure in order to enable the Hydrological validation programme to appropriately use the data;
- to provide information on product error to accompany the product distribution in an open environment, after the initial phase of distribution limited to the so-called “beta users”.

Validation is obviously a hard work in the case of precipitation, both because the sensing principle from space is very much indirect, and because of the natural space-time variability of the precipitation field (sharing certain aspects with fractal fields), that places severe sampling problems.

It is known that an absolute ‘ground reference’ does not exist. In the H-saf project the validation is based on comparisons of satellite products with ground data: radar, rain gauge and radar integrated with rain gauge. During the Development phase some main problems have been pointed out. First of all the importance to characterize the error associated to the ground data used by PPVG. Secondly to develop software for all steps of the Validation Procedure, a software available to all the members of the PPVG. Three months ago the radar and rain gauge Working Group (WG) have been composed in order to solve these problems. The first results obtained by the working groups are reported in the following sections and a complete documentation is available as annex 1-7 of this document. In addition to the radar and rain gauge WG other WG have been composed on: integrate various sets of precipitation data sources – raingauge network, radar network, NWP models outputs and climatological standards into common precipitation product, which can describe the areal instantaneous and cumulated precipitation fields (*INCA -WG*) and to investigate the opportunity to create geographical maps of error distribution for providing information on test catchments to the Hydrological Validation Group (*GEO MAP –WG*).

3.3 Validation methodology

From the beginning of the project it was clear the importance to define a common validation procedure in order to make the results obtained by several institutes comparable and to better understand their meanings. The main steps of this methodology have been identified during the development phase inside the validation group, in collaboration with the product developers, and with the support of ground data experts. The common validation methodology is based on ground data (radar and rain gauge) comparisons to produce **large statistic** (multi-categorical and continuous), and **case study analysis**. Both components (**large statistic and case study analysis**) are considered complementary in assessing the accuracy of the implemented algorithms. Large statistics helps in identifying existence of pathological behaviour, selected case studies are useful in identifying the roots of such behaviour, when present.

The main steps of the validation procedure are:

- ground data error analysis: radar and rain gauge;
- point measurements (rain gauge) spatial interpolation;

- up-scaling of radar data versus SSMI grid;
- temporal comparison of precipitation products (satellite and ground);
- statistical scores (continuous and multi-categorical) evaluation;
- case study analysis.

3.4 Ground data and tools used for validation

Both rain gauge and radar data have been used until now for H01 validation. As said in the previous section during the last Precipitation Product Validation Workshop held in Bratislava, 20-22 October 2010 it has been decided to set up Working Groups to solve specific items of the validation procedure and to develop software used by all members of the validation cluster. A complete knowledge of the ground data characteristics used inside the PPVG has been the first item of the working groups; this is necessary to understand the validation results and to define the procedure to select the most reliable data to represent a “ground reference”. A complete report on the results obtained by the Working Group on rain gauge, radar and ground data integration are reported in the Chapter 4 with a complete inventory of the ground data used within the PPVG.

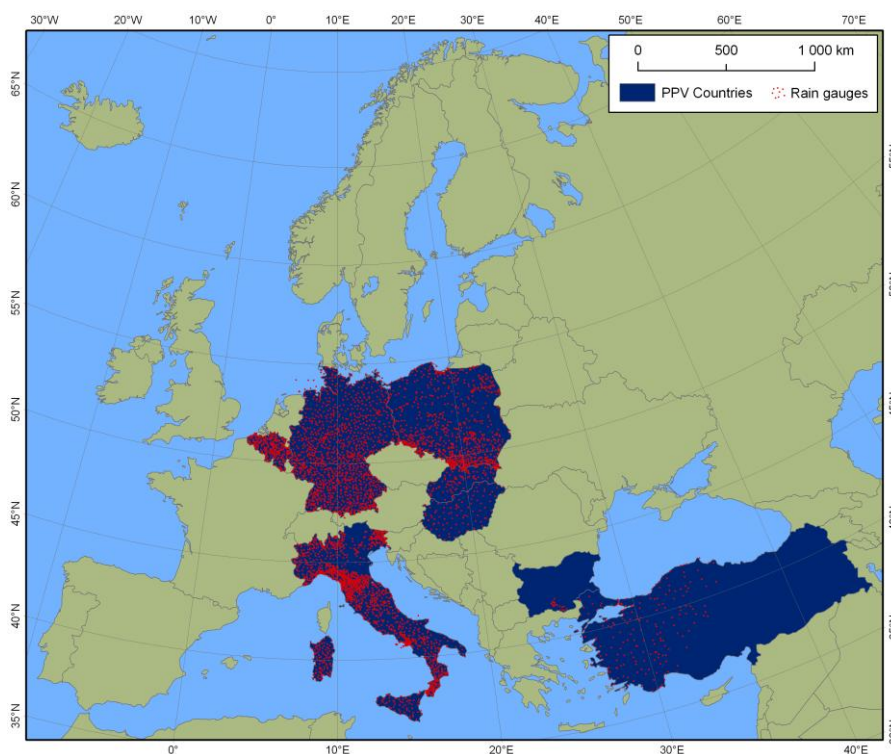


Figure 6 The network of 3500 rain gauges used for H-SAF precipitation products validation

The rain gauge networks of PPVG is composed of approximately 3500 stations across 6 Countries (Figure 6). A key characteristic of such networks is the distance between each raingauge and the closest one, averaged over all the instruments considered in the network and it is a measure of the raingauge density. Instruments number and density are summarized in Table 3.

Country	Total number of gauges *	Average minimum distance (km)
---------	--------------------------	-------------------------------

Belgium	89**	11.2
Bulgaria	37***	7
Germany	1300	17
Italy	1800	9.5
Poland	330-475	13.3
Turkey	193****	27

Table 3 Number and density of raingauges within H-SAF validation Group

* the number of raingauges could vary from day to day due to operational efficiency within a maximum range of 10-15%.

** only in the Wallonia Region

*** only in 3 river basins

**** only covering the western part of Anatolia

Most of the gauges used in the National networks by the PPVG Partners are of the tipping bucket type, and hourly cumulated (see Table 4).

The rain gauge inventory (Chapter 4) proposed by *rain gauge-WG* (annex 2) on the instruments, the operational network and the approach to match gauge data with the satellite estimates in the PPVG, has pointed out that the rain gauge networks available in the PPVG are surely appropriated for the validation of cumulated products (1 hour and higher), but probably not for instantaneous estimates. The comparison of satellite rain rate with hourly cumulated ground measurements surely introduces intrinsic errors in the matching scores, that can be estimated as very large. The validation of instantaneous estimates should be carried on only when gauges cumulation interval is 10 to 15 minutes (as in Poland). Values cumulated over shorter intervals (5 or even one minute, as it is done in Turkey) are affected by large relative errors in cases of low/moderate rain rates. Studies are undertaken in order to quantitatively estimate the errors introduced in the validation procedure comparing the instantaneous satellite precipitation estimation with the rain gauge precipitation cumulated on different intervals.

Moreover the revisiting time (3,4 hours) of H01 makes impossible or not reasonable to validate the product for 1-24 hours cumulated interval.

The WG has also pointed out that different approaches for the estimates matching are considered in the PPVG. One of the next step of the WG will be to define in collaboration with the *GeoMap-WG* (Annex 7) the spatial interpolation technique and to develop the related software to be used in side the PPVG.

Country	Minimum detectable rainrate (mm h ⁻¹)	Maximum detectable rainrate (mm h ⁻¹)	Heating system (Y/N)	cumulation interval (min)
Belgium	0.1	N/A	N	60
Bulgaria	0.1	2000	Y	120, 1440
Germany	0.05	3000	Y	60
Italy	0.2	300	Y/N*	60
Poland	0.1	300	Y	10
Turkey	0.2	288	Y	1

Table 4 Summary of the raingauge characteristics

* only 300 out of 1800 gauges are heated

An inventory on radar data, networks and products used in PPVG (Chapter 4), has pointed out that all the institutes involved in the PPVG declared the system are kept in a relatively good status and all of them apply some correction factors in their processing chain of radar data. In Figure 7 there is the map of the 54 C-band radars available in their H-SAF PPVG. Only the radar data which pass the quality control of the owner Institute are used by the PPVG for validation activities. However, these correction factors are diverse in the countries, depending on their capacities and main sources of error in the radar measurements. This also means that the corresponding rainfall estimates are different products in nature, and the estimation of their errors cannot be homogenized for all the countries of the PPVG. However, each country can provide useful information of the error structure of its rainfall products based on its own resources. The *Radar-WG* (Annex 3) is now working to define quality index (static or dynamic) in order to select the more reliable radar fields and to associate an error structure to the radar data. Quality information should take into account the radar site/geographical areas/event type/radar products. The study performed by the Slovakian team (Annex 4) and the scheme published by J. Szturc *et al* 2008, on the quality index evaluation are under consideration by the *Radar-WG*. In the future the satellite product testing will be carried out using only the data having a sufficient quality but the validation results showed in this document have been obtained using radar data which passed only data owner institute controls.

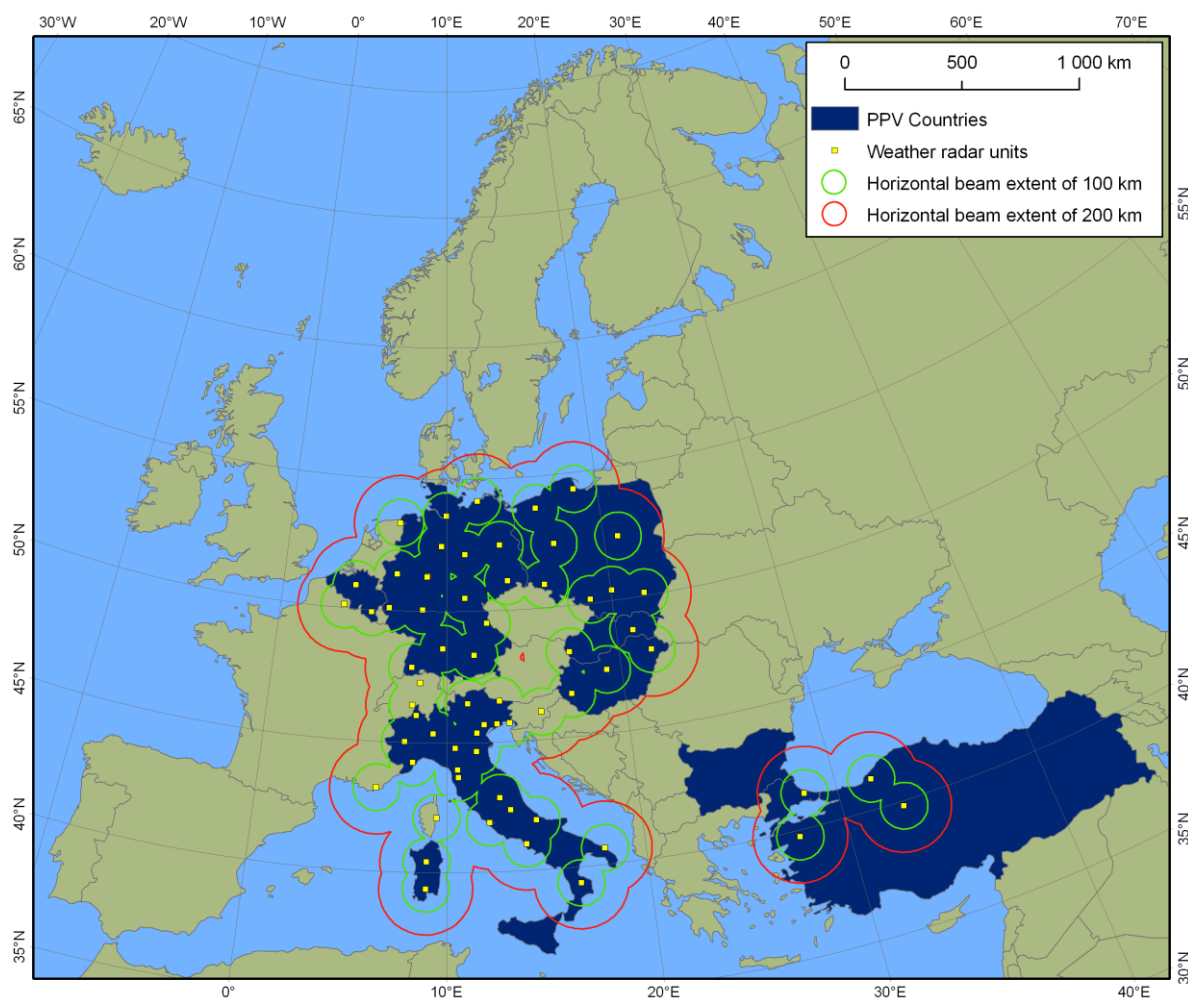


Figure 7 The networks of 54 C-band radars available in ther H-SAF PPVG

The studies that have been carried out in the PPVG on comparison of radar data with rain gauge data have shown that RMSE error associated with radar fields depends considerably on radar minimum visible height above the rain gauge in mountainous terrains like Slovakia, but less importantly in flat terrains like Hungary. In Slovakia, the RMSE% error (see Section 3.7) of radar accumulated fields is between 70-90%, whereas in Hungary, it is slightly lower, between 60-80%. Dataset for May-September 2010 have been used to derive these parameters.

In PPVG it is under investigation (*INCA-WG annex 5*) the possibility to use ground data integrated software to produce precipitation field. The results obtained by *INCA-WG* are reported in the chapter 4.

3.5 Spatial interpolation for rain gauges

The partners of the Validation Group have been using a variety of different strategies to treat gauge data. Some are using interpolation algorithms to get spatially continuous rainfall maps, while others process directly the measurements of individual gauges (Table 5). The first approach seems to be more convenient, especially when the “large” IFOV of H01 are concerned.

Country	Type of interpolation
Belgium	Barnes over 5x5 km grid
Bulgaria	Co kriging
Germany	Inverse square distance
Italy	Barnes over 5x5 km grid
Poland	No
Turkey	No

Table 5 Data pre-processing strategies

One of the next step of the *Rain Gauge-WG* will be to harmonize the different spatial interpolation techniques among partners developing a common software for the validation, collaborating with the *GeoMap-WG (Annex 7)*.

3.6 Techniques to make observation comparable: up-scaling technique for radar data

From the first Validation Workshop in 2006 it has been decided that the comparison between satellite product and ground data has to be on satellite native grid. Generally one or two rain gauges are in a SSMI pixel, but radar instruments provide many measurements within a single SSMI pixel. For this reason an up-scaling technique is necessary to compare radar data with the H01 precipitation estimations on the satellite native grid.

The precipitation data in the retrieval product (H02) is based on the instruments AMSU-A and AMSU-B or MHS flown on NOAA and MetOp satellites. These cross-track scanners provide images with constant angular sampling across track, that implies that the IFOV elongates as the beam moves from nadir toward the edge of the scan. The elongation is such that:

- for AMSU-A the IFOV at nadir is: 48 x 48 km², at the edge of the 2250 km swath: 80 x 150 km²;
- for AMSU-B and MHS the IFOV at nadir is: 16 x 16 km²; at the edge: 27 x 50 km².

H02 follows the scanning geometry and IFOV resolution of AMSU-B scan, so that each pixel along the scan has a precipitation value representative for an elliptical region next figure.

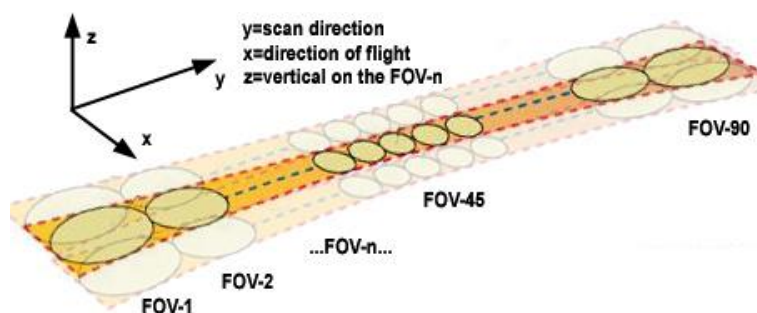


Figure 8 Geometry - Geometry of cross-track scanning for AMSU

3.6.1 Average of hi-res ground validation data

Radar instruments provide many measurements within a single AMSU pixel. Those measurements should be averaged following the AMSU-B antenna pattern.

- Establish the size in km of the axis for each elliptic FOV. You will have $N=90$ couples of values (Fx_n, Fy_n)
- Define a 2-dimensional Gaussian surface (matrix $G(N \times N)$), having resolution R (pixel size) $R \leq \text{radar resolution}$, and elliptical section at half high having axis (Ex_n, Ey_n) equal to the correspondent FOV (i.e. $Ex_n = Fx_n$ and $Ey_n = Fy_n$, see figures below; note that if the Radar resolution is 1km, $1px=1km$)

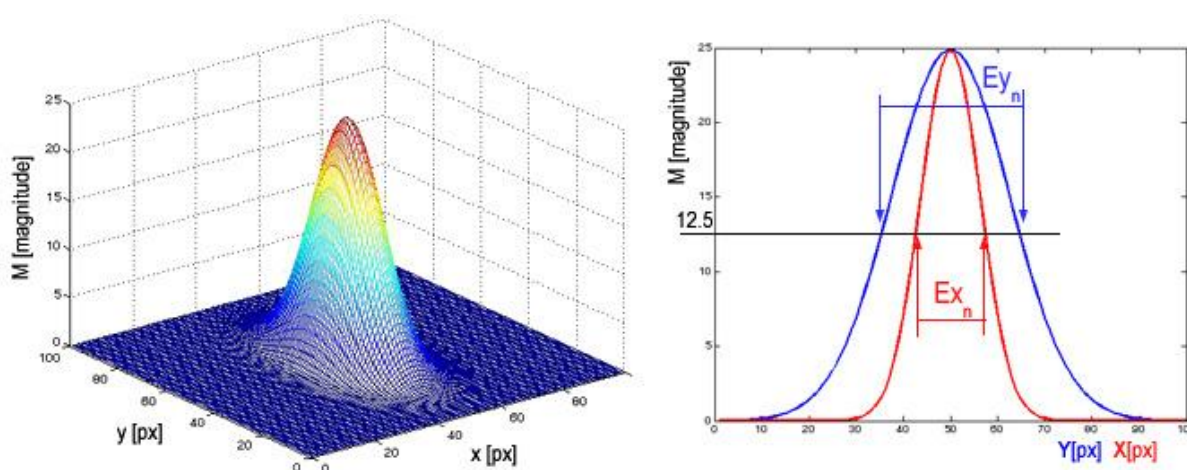


Figure 9 Left) Gaussian filter – Right) section of gaussian filter

- If the matrix $N \times N$ is too large, it can be reduced to a $M \times K$ matrix until the pixels (1,C), (C,1), (N,C), (C,N) are less than $(C,C)/100$

(1,1)		(...)		(1,C)		(...)		(1,N)
(...)								
(C,1)				(C,C)				(C,N)
(...)								
(N,1)		(...)		(N,C)		(...)		(N,N)

...				0.24				...
				0.25				
				...				
	0.23	0.25	...	25	...	0.25	0.23	
				...				
				0.25				
...				0.24				...

Table 6 Left) Original Gaussian matrix – Right) Reduced matrix to dimensions M xK

- Normalize the matrix G (MxK) obtaining the matrix **G'** having the sum of all elements equal to 1:

$$G'(m,k) = \frac{G(m,k)}{\sum_{m=1}^M \sum_{k=1}^K G(m,k)}$$

3.6.2 Smoothing of radar precipitation

For each FOV and for each SCANLINE in the file H02, make the gaussian filter overlapping radar data so that the central pixel (C,C) corresponds to (**H02_{lat}**, **H02_{lon}**) and the y axis has the same direction of the scanline.

Multiply each element of G' for the closest radar measurements (**RR_{high}(lat,lon)**), and sum the products:

$$RR_{low} = \sum_{m=1}^M \sum_{k=1}^K G'(m,k) \cdot RR_{high}$$

Following this procedure it is obtained, for each FOV and SCANLINE, a value **RR_{low}**. **RR_{low}(FOV,SCANLINE)** which represents the matrix of validation used versus AMSU-B estimates.

This scheme has been suggested by the precipitation developers of CNR-ISAC and it has been adopted by the PPVG.

One of the *Radar-WG* and *Rain Gauge-WG* next steps is to develop a common code for the up-scaling of radar data versus AMSU-B grids following this technique. The code will be an evolution and optimization of the code already available by Belgium (Van de Vyver, H., and E. Roulin, 2008) and Italy A. Rinollo. All participants of validation task will use not only the same technique but the same software.

3.7 Temporal comparison of precipitation intensity

Taking to account the revisiting time of the H02 (3,4 hours) it was decided (during the first validation workshop in 2006) to perform a direct comparison between the satellite and radar precipitation intensity maps. The revisiting time of the product does not allow to have a sensible accumulated precipitation map on 1-24 hours.

In the PPVG the satellite product is compared with the closest (up-scaled) radar and rain gauge data in time. The satellite time is considered the time in the BUFR4 file, provided by CNMCA, when validation area is first reached.

3.8 Large statistic: Continuous and multi-categorical

The large statistic analysis allows to point out the existence of pathological behaviour in the satellite product performance. It requires the application of the same validation technique step by step in all the institutes take part of the PPVG.

The large statistic analysis in PPVG is based on the evaluation of monthly and seasonal **Continuous verification** and **Multi-Categorical** statistical scores on one year of data (2010) for three precipitation classes (see next figure).

It was decided to evaluate both continuous and multi-categorical statistic to give a complete view of the error structure associated to H02. Since the accuracy of precipitation measurements depends on the type of precipitation or, to simplify matters, the intensity, the verification is carried out on three classes indicated by hydrologists during the development phase (see *next table*).

Precipitation Classes	1	2	3
	< 1 mm/h (light precipitation)	1 - 10 mm/h (medium precipitation)	> 10 mm/h (intense precipitation)

Table 7 Classes for evaluating Precipitation Rate products

The rain rate lower than 0.25 mm/h is considered no precipitation.

The main steps to evaluate the statistical scores are:

- all the institutes up-scale the national radar and rain gauge data on the satellite native grid using the up-scaling techniques before described;
- all the institutes compare H02 with the radar precipitation intensity and the rain gauge cumulated precipitation;
- all the institutes evaluate the monthly and seasonal continuous scores (below reported) and contingency tables for the precipitation classes producing numerical files called 'CS' and 'MC' files;
- all the institutes evaluate PDF producing numerical files called 'DIST' files and plots;
- the precipitation product validation leader collects all the validation files (MC, CS and DIST files), verifies the consistency of the results and evaluates the monthly and seasonal common statistical results;

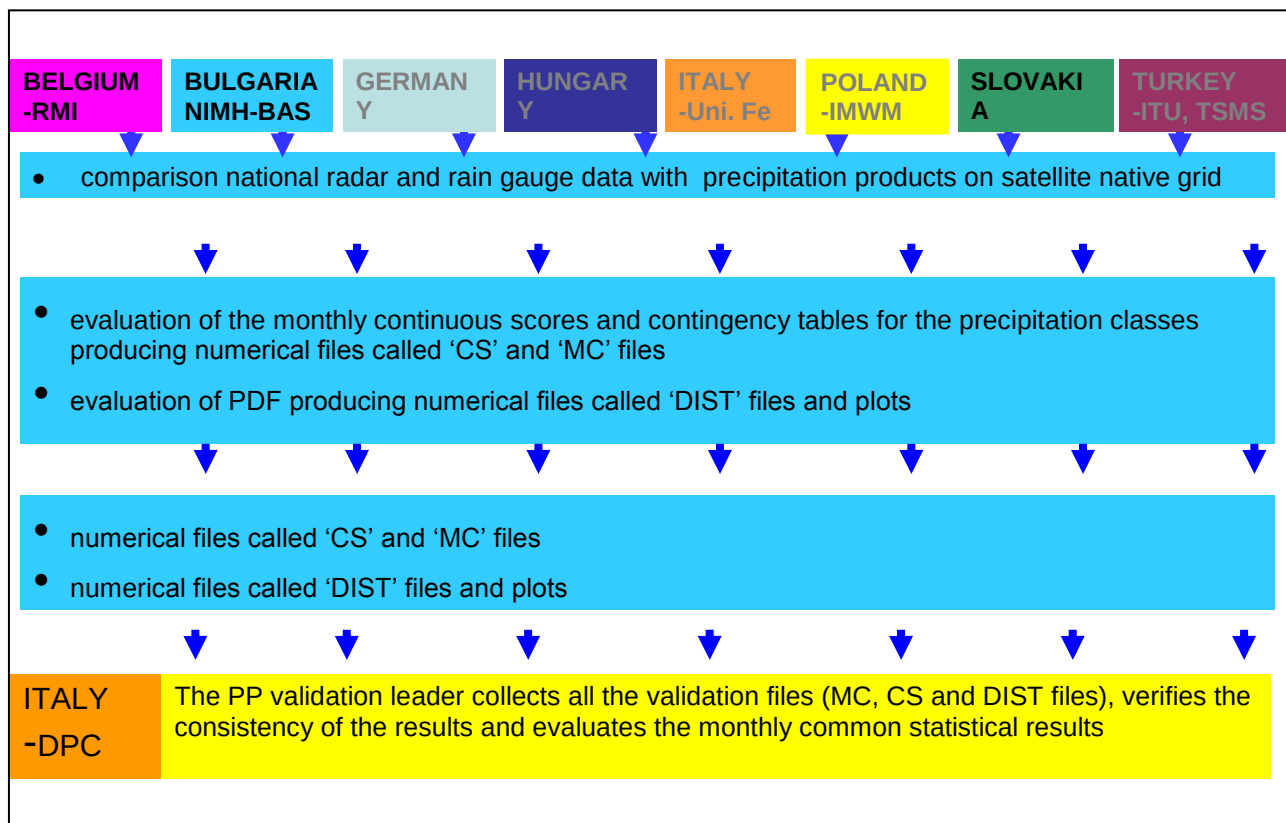


Figure 10 Main steps of the validation procedure in the PPVG

Statistical scores

The statistical scores evaluated in PPVG *for continuous statistics* are:

- Mean Error (ME)

$$ME = \frac{1}{N} \sum_{k=1}^N (sat_k - true_k)$$

Range: $-\infty$ to ∞ . Perfect score: 0

- Mean Absolute Error (MAE)

$$MAE = \frac{1}{N} \sum_{k=1}^N |sat_k - true_k|$$

Range: 0 to ∞ . Perfect score: 0

- Standard Deviation (SD)

$$SD = \sqrt{\frac{1}{N} \sum_{k=1}^N (sat_k - true_k - ME)^2}$$

Range: 0 to ∞ . Perfect score: 0

- Multiplicative Bias (MBias)

$$MB = \frac{\frac{1}{N} \sum_{k=1}^N sat_k}{\frac{1}{N} \sum_{k=1}^N true_k}$$

Range: $-\infty$ to ∞ . Perfect score: 1

- Correlation Coefficient (CC)

$$CC = \frac{\sum_{k=1}^N (sat_k - \overline{sat})(true_k - \overline{true})}{\sqrt{\sum_{k=1}^N (sat_k - \overline{sat})^2 \sum_{k=1}^N (true_k - \overline{true})^2}}$$

$$\text{with } \overline{sat} = \frac{1}{N} \sum_{k=1}^N sat_k \quad \text{and} \quad \overline{true} = \frac{1}{N} \sum_{k=1}^N true_k ;$$

Range: -1 to 1. Perfect score: 1

- Root Mean Square Error (RMSE)

$$RMSE = \sqrt{\frac{1}{N} \sum_{k=1}^N (sat_k - true_k)^2}$$

Range: 0 to ∞ . Perfect score: 0

- Root Mean Square Error percent (RMSE %), used for precipitation since error grows with rate.

$$RMSE \% = \sqrt{\frac{1}{N} \sum_{k=1}^N \frac{(sat_k - true_k)^2}{true_k^2}} * 100$$

Range: 0 to ∞ . Perfect score: 0

The statistical scores evaluated in PPVG for **multi categorical statistic** are derived by the following contingency table:

Contingency Table				
		ground		
		yes	no	total
satellite	yes	hits	false alarms	forecast yes
	no	misses	correct negatives	forecast no
	total	observed yes	observed no	total

where:

- hit: event observed from the satellite, and also observed from the ground
- miss: event not observed from the satellite, but observed from the ground
- false alarm: event observed from the satellite, but not observed from the ground
- correct negative: event not observed from the satellite, and also not observed from the ground.

The scores evaluated from the contingency table are:

- Probability Of Detection (POD)

$$POD = \frac{hits}{hits + misses} = \frac{hits}{observed\ yes}$$

Range: 0 to 1. Perfect score: 1

- False Alarm Rate (FAR)

$$FAR = \frac{false\ alarms}{hits + false\ alarms} = \frac{false\ alarms}{forecast\ yes}$$

Range: 0 to 1. Perfect score: 0

- Critical Success Index (CSI)

$$CSI = \frac{hits}{hits + misses + false\ alarm}$$

Range: 0 to 1. Perfect score: 1

- Equitable Threat Score (ETS)

$$ETS = \frac{hits - hits_{random}}{hits + misses + false\ alarm - hits_{random}} \quad \text{with} \quad hits_{random} = \frac{observed\ yes * forecast\ yes}{total}$$

ETS ranges from -1/3 to 1. 0 indicates no skill. Perfect score: 1.

- Frequency Bias (FBI)

$$FBI = \frac{hits + false\ alarms}{hits + misses} = \frac{forecast\ yes}{observed\ yes}$$

Range: 0 to ∞ . Perfect score: 1

- Probability Of False Detection (POFD)

$$POFD = \frac{false\ alarms}{correct\ negatives + false\ alarms} = \frac{false\ alarms}{observed\ no}$$

Range: 0 to 1. Perfect score: 0

- Fraction correct Accuracy (ACC)

$$ACC = \frac{hits + correct\ negatives}{total}$$

Range: 0 to 1. Perfect score: 1

- Heidke skill score (HSS)

$$HSS = \frac{(hits + correct\ negatives) - (expected\ correct)_{random}}{N - (expected\ correct)_{random}}$$

with

$$(expected\ correct)_{random} = \frac{1}{N} [(observed\ yes)(forecast\ yes) + (forecast\ no)(observed\ no)]$$

Range: $-\infty$ to 1. 0 indicates no skill. Perfect score: 1.

- Dry-to-Wet Ratio (DWR).

$$DWR = \frac{false\ alarm + correct\ negative}{hits + misses} = \frac{observed\ no}{observed\ yes}$$

Range: 0 to ∞ . Perfect score: n/a.

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3.9 Case study analysis

Each Institute, in addition to the large statistic verification produces a case study analysis based on ***the knowledge and experience of the Institute itself***. Each institute, following a standard format here reported decides whether to use ancillary data such as lightning data, SEVIRI images, the output of numerical weather prediction and nowcasting products.

The main sections of the standard format are:

- description of the meteorological event;
- comparison of ground data and satellite products;
- visualization of ancillary data;
- discussion of the satellite product performances;
- indications to Developers;
- indication on the ground data (if requested) availability into the H-SAF project.

More details on case study analysis will be reported in the Chapter 5.

3.10 Next steps

On the base of the development phase it is possible to say that the ground data error characterization is necessary and that a validation of a common protocol is not enough. Only the use of the same software can guarantee that the results obtained by several institutes are obtained in the same way. To improve the validation methodology and to develop software used by all members of the validation cluster several working groups have been composed during the last Validation Workshop held in Bratislava, 20-22 October 2010 (Annex 1 -7).

On the base of published papers and the characteristics of the ground data available inside the PPVG the main next steps are foreseen in order to improve the validation methodology:

- quantitative estimation of the errors introduced in the validation procedure comparing the instantaneous satellite precipitation estimation with the rain gauge precipitation cumulated on different intervals;
- definition of a rain gauge and radar data quality check;
- application of the data quality check to all radar and rain gauge data used in the PPVG;
- definition of the optimal and minimal spatial density of rain gauge stations to be representative of the ground precipitation in the view of satellite product comparison;
- development of the three software for raingauges, radar and INCA products up-scaling vs AMSU-B grids;
- definition and code implementation of the technique for the temporal matching of satellite rain rate with rain gauge and radar data;
- selection of the appropriate methodology for spatial distribution of precipitation products errors taking into consideration spatial and temporal characteristics of each product for selected areas as test catchments.

All these activities will be developed and coordinated inside the Working Groups (Annex 1 -7).

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4 Ground data used for validation activities

4.1 Introduction

In the following sections the precipitation ground data networks used in the PPVG are described: radar and rain gauge data of eight countries: Belgium, Bulgaria, Germany, Hungary, Italy, Poland, Slovakia, and Turkey. H02, has been submitted to validation in all these countries except Bulgaria. Until now the Bulgarian data are used only for H05 validation activity according to the Project Plan. Their use in the next months is under consideration.

It is well known that radar and rain gauge rainfall estimation is influenced by several error sources that should be carefully handled and characterized before using these data as reference for ground validation of any satellite-based precipitation products. In the last months working groups (Annex 1, 2, 3, 4, 5 and 7) have been composed in order to provide complete information on the ground data characteristics and to evaluate the associated errors.

In this chapter a complete analysis of the ground data available in the PPVG is reported by the rain gauge and radar data in PPVG summaries (Section 4.2 and 4.3), the Rain gauge and radar data integrated products in PPVG first report (Section 4.4) and a country by country ground data description (Section 4.5- 4.13). The chapter has the object to provide ground data information and to highlight their error sources.

4.2 Rain Gauge in PPVG

In this section the complete inventory of the raingauges used in the PPVG with some considerations are reported as first results of the *Rain gauge- WG* (Annex 2).

4.2.1 The networks

The validation work carried on with raingauges uses about 3500 instruments across the 6 Countries: Belgium, Bulgaria, Germany, Italy, Poland, and Turkey, as usual, irregularly distributed over ground. A key characteristic of such networks is the distance between each raingauge and the closest one, averaged over all the instruments considered in the network and it is a measure of the raingauge density. Instruments number and density are summarized in Table 8.

The gauges density ranges between 7 (for Bulgaria, where only 3 river basins are considered) to 27 km (for Turkey). These numbers should be compared with the decorrelation distance for precipitation patterns at mid-latitude. Usually the decorrelation distance is defined as the minimum distance between two measures to get the correlation coefficient (Pearson Coefficient) reduced to e^{-1} . A recent study on the H-SAF hourly data for Italy, shows this decorrelation distance varies from about 10 km in warm months (where small scale convection dominates) to 50 km in cold months, when stratified and long lasting precipitation mostly occur. In Figure 12 value of the linear correlation coefficient is computed between each raingauge pair in the Italian hourly 2009 dataset, as function of the distance between the two gauges.

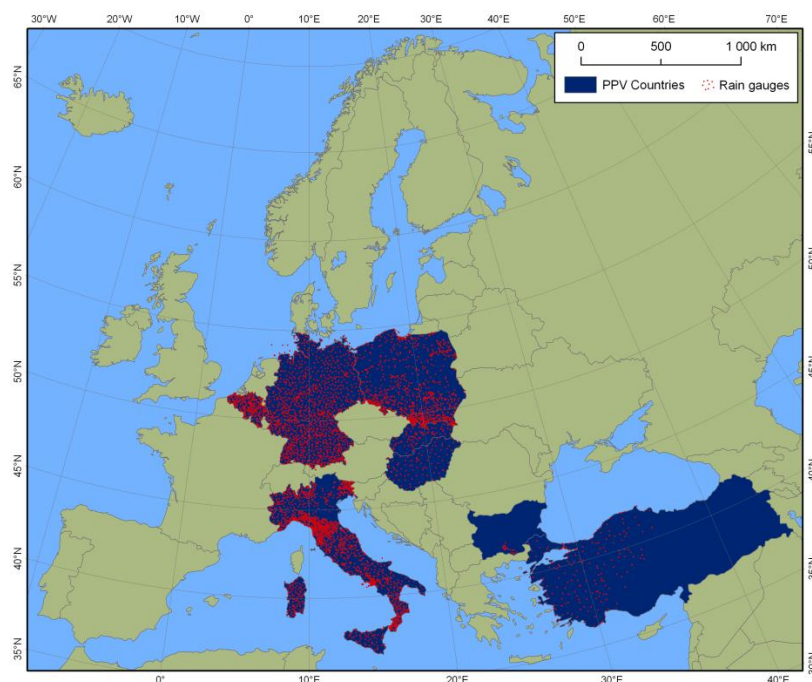


Figure 11 Rain gauge networks in PPVG

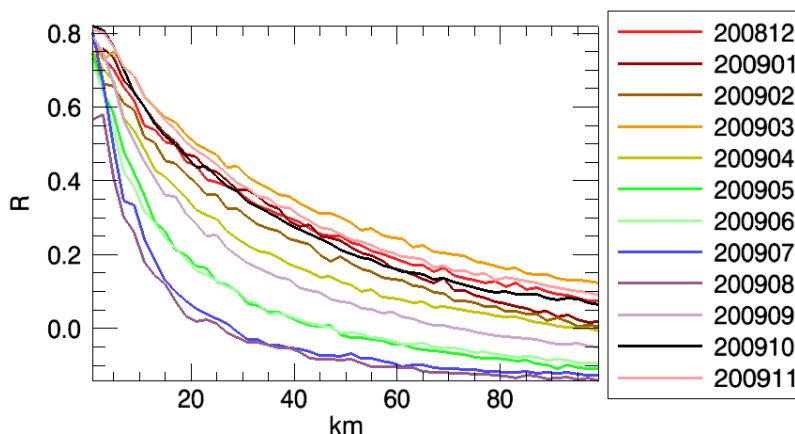


Figure 12 Correlation coefficient between raingauge pairs as function of the distances between the gauges. Colours refer to the months of the year 2009

Assuming these values significant for the other Countries involved in this study, we can conclude that the gauge network in PPVG is capable to resolve the spatial structure of rain patterns only for stratified systems but it is inadequate for small scale convective events.

Country	Total number of gauges *	Average minimum distance (km)
Belgium	89**	11.2
Bulgaria	37***	7
Germany	1300	17
Italy	1800	9.5
Poland	330-475	13.3

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Turkey	193****	27
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Table 8 Number and density of raingauges within H-SAF validation Group

* the number of raingauges could vary from day to day due to operational efficiency within a maximum range of 10-15%.

** only in the Wallonia Region

*** only in 3 river basins

**** only covering the western part of Anatolia

4.2.2 The instruments

Most of the gauges used in the National networks by the PPVG Partners are of the tipping bucket type, which is the most common device used worldwide to have continuous, point-like rainrate measurement. Nevertheless, several source of uncertainty in the measurements are well known but difficult to mitigate. First, very light rainrates (1 mm h^{-1} and less) can be incorrectly estimated due to the long time it takes the rain to fill the bucket (Tokay et al., 2003). On the other side, high rainrates (above 50 mm h^{-1}) are usually underestimated due to the loss of water during the tips of the buckets (Duchon and Biddle, 2010). Drifting wind can also greatly reduce the size of the effective catching area, if rain does not fall vertically, resulting in a rainrate underestimation quantitatively assessed in about 15% for an average event (Duchon and Essenberg, 2001).

Further errors occur in case of solid precipitation (snow or hail), when frozen particles are collected by the funnel but not measured by the buckets, resulting in a temporal shift of the measurements since the melting (and the measure) can take place several hours (or days, depending on the environmental conditions) after the precipitation event (Leitinger et al, 2010, Sugiura et al, 2003). This error can be mitigated by an heating system that melts the particles as soon as are collected by the funnel. All these errors can be mitigated and reduced, but in general not eliminated, by a careful maintenance of the instrument.

A number of *a posteriori* correction strategies have been developed in order to correct precipitation data measured by raingauges, but mainly apply at longer accumulation intervals, daily to monthly (Wagner, 2009)

Country	Minimum detectable rainrate	Maximum detectable rainrate (mm h^{-1})	Heating system (Y/N)	cumulation interval (min)
Belgium	0.1 mm	N/A**	N	60
Bulgaria	0.1 mm	2000	Y	120, 1440
Germany	0.05 mm h^{-1}	3000	Y	60
Italy	0.2 mm	N/A**	Y/N*	60
Poland	0.1 mm	N/A**	Y	10
Turkey	0.2 mm	720	Y	1

Table 9 Summary of the raingauge characteristics

* only 300 out of 1800 gauges are heated

** information not available at the moment: a value about 300 mmh^{-1} can be assumed for tipping bucket raingauges.

Most of these shortcomings could be avoided by using instruments based on different principle or mechanisms. The German network, and a part of the Bulgarian network, as an example, are equipped by precipitation weighting gauges, that allow continuous precipitation (both solid and liquid)

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measurements with higher accuracy. Other option could be the use of disdrometers, which give more information about the precipitation structure and a more accurate rainrate measure.

In previous table relevant characteristics of the raingauges used in the different countries are reported.

4.2.3 Data processing

The partners of the Validation Group have been using a variety of different strategies to treat gauge data and to compare them with satellite estimates. Some are using interpolation algorithms to get spatially continuous rainfall maps, while others process directly the measurements of individual gauges. All the data in the network (except for cold months in Poland) are quality controlled: there is no information about the techniques used, but usually quality control rejects data larger than a given threshold and in case of too high rainrate difference (exceeding given thresholds) among neighbouring gauges and between subsequent measures of the same instrument. Table 10 summarizes the data pre-processing performed in different Countries, while Table 11 reports the different matching approaches for H01-H02 respectively.

As for the temporal matching, the used approaches are rather homogeneous within the Groups: instantaneous measurements are matched with next ground cumulated values over the different available intervals, ranging from 1 minute (Turkey) to 1 hour (Italy, Germany). Cumulated estimates, obviously, are compared to ground measured rain amounts over the same cumulation intervals.

As for spatial matching, different approaches are considered, also taking into account the different spatial structure of the satellite IFOVs. Two basic ideas are pursued: pixel-by-pixel matching or ground measure averaging inside satellite IFOV. The second approach seems to be more convenient, especially when the “large” IFOV of H01 and H02 are concerned. Probably it is mandatory for H02 also take into account that the size of the IFOV changes across the track and could become very large. The first approach, e.g. nearest neighbour, can be more effective for H03 and H05 products.

Country	Type of interpolation	Quality control (Y/N)
Belgium	Barnes over 5x5 km grid	Y
Bulgaria	Co kriging	Y
Germany	Inverse square distance	Y
Italy	Barnes over 5x5 km grid	N
Poland	No	Y (except cold months)
Turkey	No	Y

Table 10 Data pre-processing strategies

Country	H01		H02	
	Spatial matching	Temporal matching	Spatial matching	Temporal matching
Belgium*	N/A	N/A	N/A	N/A
Bulgaria*	N/A	N/A	N/A	N/A
Germany	matching gauges are searched on a radius of 2.5 km from the IFOV centre	each overpass is compared to the next hourly rain amount	matching gauges are searched on a radius of 2.5 km from the IFOV centre	each overpass is compared to the next hourly rain amount
Italy	mean gauges value over 15x15 km area centred on satellite	each overpass is compared to the next hourly rain	Gaussian-weighted mean gauges value centred on satellite	each overpass is compared to the next hourly rain

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	IFOV	amount	IFOV	amount
Poland	mean gauges value over the IFOV area (rectangular)	each overpass is compared to the next 10-minutes rain amount	mean gauges value over the IFOV area (rectangular)	each overpass is compared to the next 10-minutes rain amount
Turkey	weighted mean of the gauge values estimated at the 3kmX3km grid structure within satellite IFOV by using semi variogram	each overpass is compared to 5 minute averaged rain" for Temporal matching	weighted mean of the gauge values estimated at the 3kmX3km grid structure within satellite IFOV by using semi variogram	each overpass is compared to 5 minute averaged rain" for Temporal matching

Table 11 Matching strategies for comparison with H01 and H02

*Belgium and Bulgaria use raingauges only for cumulated precipitation validation.

4.2.4 Some conclusions

After this inventory some conclusion can be drawn.

First, it seems the raingauge networks used in this validation activities are surely appropriated for the validation of cumulated products (1 hour and higher), while for instantaneous estimates the use of hourly cumulated ground measurements surely introduces intrinsic errors in the matching scores, that can be estimated as very large. The validation of instantaneous estimates should be carried on only when gauges cumulation interval is 10 to 15 minutes (as in Poland). Values cumulated over shorter intervals (5 or even one minute, as it is done in Turkey) are affected by large relative errors in cases of low/moderate rainrates.

Different approaches for the estimates matching are considered, and probably could be a good idea to harmonize them among partners. The ground data up-scaling procedure indicated in Section 3.5 has been already developed by E. Roulin (Van de Vyver, H., and E. Roulin, 2008) and A. Rinollo. An optimization of this code to be used by all the partners of the PPVG represent one of the next step.

Anyway, different approaches over different Countries are leading to very similar values in the considered skill scores, indicating probably two things: 1) none of the considered approaches can be considered as inadequate and (more important) 2) the differences between ground fields and satellite estimates are so large that different views in the data processing do not results in different numbers.

4.3 Radar data in PPVG

In this section the complete inventory of the radar data used in the PPVG with some considerations are reported as first results of the *Radar- WG* (Annex 3).

4.3.1 The networks

In the HSAF project, satellite-based precipitation estimations are compared regularly with the radar-derived precipitation fields. However, radar rainfall products are influenced by several error sources that should be carefully analyzed and possibly characterized before using it as a reference for validation purposes.

However, we have to emphasize that the radar data used for validation purposes is not developed by the validation groups themselves. They are developed within specialized radar working teams in many

of the countries. It is not the aim of the PPVG to improve the radar data used; however, it is specifically expected from the current activities to characterize radar data and error sources of the ground data coming from the radar networks of the PPVG.

Main error sources of radar rainfall estimations are listed in the Radar Working Group description document (Annex 3):

1. system calibration,
2. contamination by non-meteorological echoes, i.e. ground clutter, sea clutter, “clear air” echoes (birds, insects), W-LAN interferences,
3. partial or total beam shielding,
4. rain path attenuation,
5. wet radome attenuation,
6. range dependent errors (beam broadening, interception of melting snow),
7. contamination by dry or melting hail (“hot spots”),
8. variability of the Raindrop Size Distribution (RSD) and its impact on the adopted inversion techniques

Moreover, several studies have been on radar quality assessments like *S’ alek M, Cheze J-L, Handwerker J, Delobbe L, Uijlenhoet R. 2004.: Radar techniques for identifying precipitation type and estimating quantity of precipitation. COST Action 717, Working Group 1 – A review. Luxembourg, Germany; or Holleman, I., D., Michelson, G. Galli, U. Germann and M. Peura, Quality information for radars and radar data, Technical rapport: 2005, EUMETNET OPERA, OPERA_2005_19, 77p.*

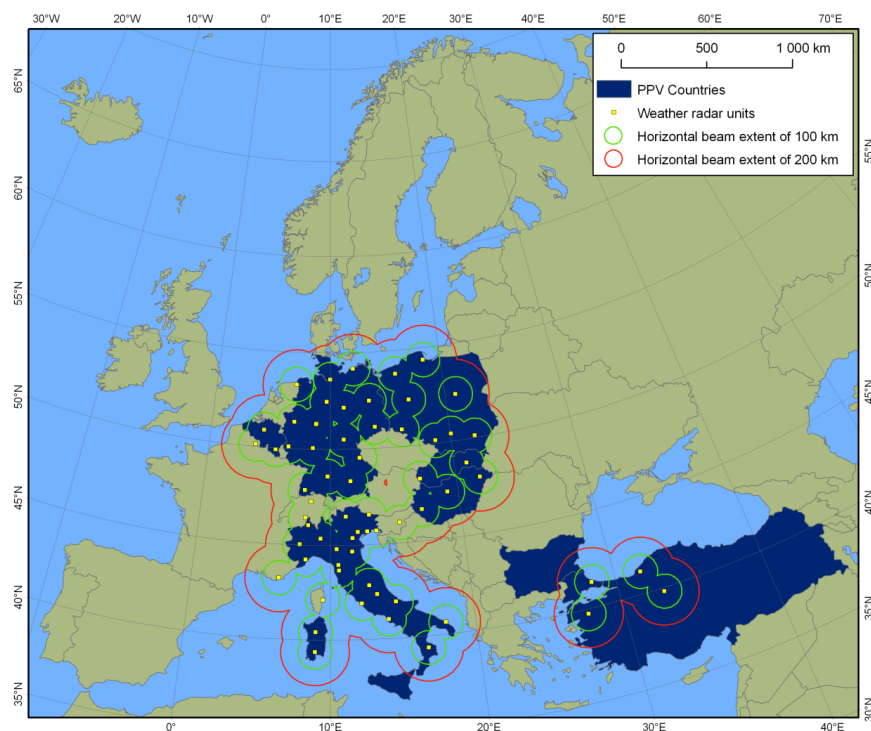


Figure 13 Radar networks in PPVG

The first step was to collect characteristics (polarization, beam width, maximum range, range, resolution, scan frequency, geographical coordinates, scan strategy [elevations]...) of the radar networks which composes the PPVG adopted processing chain; and the generated products (including

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the quality map, if any). The results of the overview of different radar capacities and instruments in each of the participating countries are here reported.

4.3.2 The instruments

In the PPVG group, there are 54 C-band radars used, or in the plan to be used. Their distribution in the countries is:

- Belgium (1 radar)
- Germany (16 radars – not BfG products)
- Hungary (3 radars)
- Italy (18 radars)
- Slovakia (2 radars)
- Poland (8 radars)
- Turkey (6 radars)

These radars cover wide range of geographical area: from the longitude 5.50562 in Wideumont, Belgium to the most Eastern area with longitude 32°58'15" in Ankara, Turkey; and from the Northern latitude of 54°23'03,17" in Gdańsk, Poland to the latitude of 36°53'24" in Mugla, Turkey and lat 37,462 in Catania, Italy. The Radars are built at different elevations above the sea level. In mountainous countries, they are placed at elevations more than 1000m above sea level; whereas in flat countries like Hungary or Belgium, their height position is not exceeding 400m. This information collected will be useful in the future steps of the Working Group to assess the partial or total beam shielding by mountains in the propagation way of the radar signals.

All radars are C-band radars, working at frequency in C-band, at 5.6 GHz. All radars are equipped by Doppler capacity which means that ground clutters can be removed from the radar data measurements effectively; however, not all of them have dual polarization which would be important to correct rain path attenuation.

The scan strategy for each of the radars used has been investigated. In this matter, all countries have shared their information on the number of elevations, minimum and maximum elevations, scan frequency, maximum nominal range distance, and range resolution.

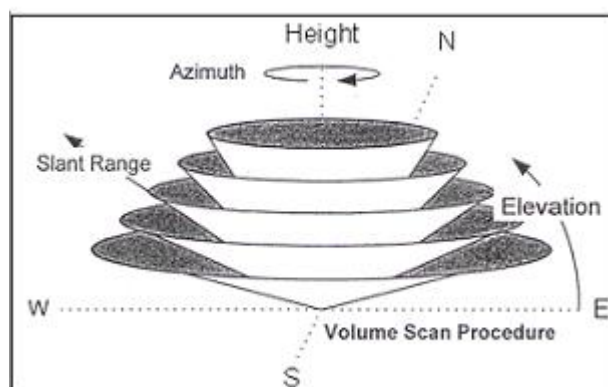


Figure 14 Radar scan procedure

In the PPVG the scan frequency ranges from 5 minutes in Belgium, Germany and Slovakia to 10 minutes in Turkey and Poland, and 15 minutes in Hungary; and varying frequency for Italian radars. The number of elevation stays between 4 and 15, in average around 10.

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The range distance used is 240 km in general. But in some places in Italy, and for the Turkish radars, the maximum range distance used is 120 km, or even less, e.g. 80 km.

Range resolution is 250 m in Belgium, 250, 340, 225, and sometimes 500 m for the Italian radars, 500 m for one of the Hungarian radars, and 250m for the other two, Polish radars can work with 125 m and 250 m resolution, and in Turkey it is 250 m for all the radars.

The scan strategies within the PPVG countries are well-balanced and similar to each other; though they vary from one radar to the other, even within countries.

All radars are regularly maintained and calibrated, which is a good indicator of the continuous supervision of quality of radar data, and the important element to sustain radar data quality.

4.3.3 Data processing

The Tab. 08 is provided to summarize the available products generated from radar measurements, and the processing chain used to generate them. Finally, the list of the radar products used for the validation work is included in the last row.

Radar rainfall products are obtained after processing the measured radar reflectivity at different elevations of the radar scan strategy. After each elevation, the PPI (Plan Position Indicator) products and the CAPPI (Constant Altitude PPI) products are calculated. PPI is the measurement of the radar antenna rotating 360 degrees around the radar site at a fixed elevation angle. CAPPI products are derived from this, by taking into account the radar displays which give a horizontal cross-section of data at constant altitude. The CAPPI is composed of data from several different angles that have measured reflectivity at the requested height of CAPPI product.

The PPVG group uses mostly CAPPI products for calculation of rainfall intensities; except for Hungary, which uses the CMAX data (maximum radar reflectivity in each pixel column among all of the radar elevations) for deriving rainfall intensities. However, the rest of the countries have also chosen different elevation angles for the CAPPI product which provides the basis for rain rate estimations. Additionally, we have to say that the countries apply different techniques of composition of radar data that were not specified in this questionnaire. The composition technique is important in areas which are covered by more than one radar measurements. Also, the projection applied is varying from one country to the other.

To sum up, the radar products used are not harmonized, different techniques are applied. However, each of them is capable to grasp rainfall and to estimate rainfall intensity.

As for the accumulated products, we see that Belgium uses 24-hourly accumulations, with rain gauge correction, Italy uses 3, 6, 12, 24h accumulations without gauge-correction; in Hungary 3, 6, 12, 24h data is used, but only the 12h and 24 hourly accumulations are corrected by rain gauges, in Poland and Slovakia no rain gauge correction is applied. Poland has only 6, and 24 hourly data. Turkey has 3,6,12,24h data, and applies rain gauge correction for 1 hourly data. It is important to note that techniques used for accumulation are numerous, even within the same country they can differ from one accumulation period to another. E.g. in Hungary, the 3,6h accumulations are derived from summing up the interpolation of the 15minute-frequent measurements into 1 minute-intervals; whereas the 12, and 24 h accumulations are summed up from 15 minute measurements, but corrected with rain gauge data.

All above implies that more probably the quality and error of rainfall and rain rate accumulations is differing from one country to another; and cannot be homogeneously characterized.

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4.3.4 Some conclusions

Maintenance

All the contributors declared the system are kept in a relatively good status.

Correction factors for error elimination:

These correction factors are diverse in the countries, not homogeneous distribution of correction methods:

- all contributors compensate for non-meteorological echoes (Clutter)
- RLAN interferences implemented in Hungary, Slovakia- in development.
- Poland and Slovakia correct attenuation. In other countries, it is not accounted for.
- Some of the countries are testing new procedures for dealing with VPR (Italy) and Partial Beam Blockage, PBB effects. VPR (Vertical Profile of Reflectivity) used in Turkey.

This means that the corresponding rainfall estimates are diverse, and the estimation of their errors cannot be homogenized.

However, each county can provide useful information of the error structure of its rainfall products based on its own resources: e.g. if they have already defined Quality Indicators, or estimations of errors based on studies of comparison of radar and rain gauge data in the country itself. The study performed by the Slovakian team (Annex 4) and the scheme published by J. Szturc, on the quality index evaluation are under consideration by the *Radar-WG*.

In the future, possible separation of reliable and quasi-reliable radar fields would be possible. Separation would be based on radar site/geographical areas/event type/radar products. Selected cases will be suitable enough to be used as a reference for the H-SAF products validation. A study on evaluation of radar measurements quality indicator with regards to terrain visibility has been conducted by the Slovakian team (see Annex 4).

Satellite product testing will be carried out in areas with higher reliability. Statistical results will be evaluated and compared to previous data. As such, the accuracy of statistical results of PPVG with radar data as ground reference will be able to be established.

	BELGIUM	ITALY	HUNGARY
List of Available Products	Rain rate 240 Km; rain rate 120 Km; velocity (120 Km); MAX (240 Km); VVP2 Windprofiles; Hail Probability; Hail Probability 24h Overview; 1, 3, 24 Hr Rainrate accumulation;		CMAX, PPI, CAPPI(2.5 km), VIL, ETops, Base, HailProbability
Is any quality map available?	NO	YES	NO
Processing chain	Clutter removal (time-domain Doppler filtering and static clutter map);	Clutter suppression by Fuzzy Logic scheme using Clutter map, Velocity,	RLAN(wifi) filter; Clutter removal; attenuation correction + beam

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	Z-R: a=200, b=1.6	Texture. Z-R: a=200, b=1. VPR correction under testing.	blocking correction => next Year (2012) VPR => No Z-R: a=200, b=1.6
Description of instantaneous radar product used in HSAF Validation Activities	PCAPPI-1500m Cartesian grid, 600m resolution	Nationale composite: CAPPI 2 km, CAPPI 3 km, CAPPI 5 km, VMI, SRI Projection: Mercator Resolution: 1 km Threshold: No	National composite, (CMAX) Projection: stereographic (S60) Resolution: 2 km Threshold: 7dBZ No rain gauge correction
Description of accumulated radar product used in HSAF Validation Activities	24-h accumulation with range-dependent gauge adjustment, Cartesian grid, 600m resolution	Acc. periods: 1, 3, 6, 12, 24h Projection: Mercator Resolution: 1 km Threshold: No No rain gauge correction	Acc.periods: 3,6,12,24h National composite, (CMAX) Projection: stereographic (S60) Resolution: 2 km Threshold: 7dBZ Rain gauge correction applied for 12, 24 hourly data

Table 12 Inventory of the main radar data and products characteristics in Belgium, Italy, Hungary

	POLAND	SLOVAKIA	TURKEY
List of Available Products.	PPI, PCAPPI, RHI, MAX, EHT, SRI, PAC, VIL, VVP, HWIND, VSHEAR, HSHEAR, LTB, SWI, MESO, WRN. List of non-operational products: LMR, CMAX, UWT, VAD, SHEAR, SWI, MESO, ZHAIL, RTR, CTR, WRN.	CAPPI 2 km, Etops, PPI 0.2, Base, Cmax, Hmax, VIL, Precip. Intensity, 1h-, 3h-, 6h-, 24h-acc. precip., 1h-acc. SRI 1km, 2km agl	MAX, PPI, CAPPI, VIL, ETOPS, EBASE, RAIN Accumulation (1,3,6,12,24h)
Processing chain	Doppler method clutter removal; attenuation correction - yes; VPR => No Z-R: a=200, b=1.6	Clutter filtering: frequency-domain IIR filter; Atmospheric attenuation correction; Z-R: a=200, b=1.6 RLAN filtering in development	Clutter Removal, VPR Correction, Z-R: A=200 b=1.6
Is any quality map available?	NO, in development	NO	NO

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Description of instantaneous radar product used in HSAF Validation Activities	National composite, (SRI); Projection: azimuthal equidistant (standard: ellipsoid); Resolution: 1 km; Threshold: 5 dBZ; No rain gauge correction.	National composite CAPPI 2 km Projection: Mercator Resolution: 1 km Threshold: -31.5 dBZ No rain gauge correction	CAPPI, Projection: Azimuthal Equidistant Resolution: 250 m Threshold: ? Rain Gauge Correction (with limited number of gauges)
Description of accumulated radar product used in HSAF Validation Activities	Acc. Periods: 1, 6, 24h; National composite (PAC), Projection: azimuthal equidistant (standard: ellipsoid); Resolution: 1 km; Threshold: 0,1 mm; No rain gauge correction	Acc. periods: 3, 6, 12, 24h National composite CAPPI 2 km Projection: Mercator Resolution: 1 km Threshold: -31.5 dBZ No rain gauge correction	Acc.periods: 1,3,6,12,24h Projection: Azimuthal Equidistant Resolution: 250 m Threshold: ? Rain gauge correction applied for 1h Rain Acc.

Table 13 Inventory of the main radar data and products characteristics in Poland, Slovakia, Turkey

4.4 Rain gauge and radar data integrated products in PPVG

In order to investigate the possible improvement of the ground precipitation field estimation a WG “INCA-WG” has been introduced in the validation activities of PPVG. In this section the first results with some considerations of the *INCA- WG* (Annex 5) are reported.

Within the WG participating countries (Slovakia, Poland and Germany) there are two types of systems providing precipitation analyses usable for H-SAF validation: **INCA** (developed by ZAMG, Austria) and **RADOLAN** (DWD, Germany).

The INCA system is currently under development as INCA-CE (Central Europe) and it is used in pre-operational mode in Slovakia and Poland. The RADOLAN system is used in Germany operationally and it is already utilized for the H-SAF products validation. Both systems consist of computational modules which enable to integrate various sets of precipitation data sources – raingauge network, radar network, NWP models outputs and climatological standards into common precipitation product, which can describe well the areal instantaneous and cumulated precipitation fields.

Here below a brief description of the INCA and RADOLAN systems follows. More information on both systems can be found in the documentation which is available on the H-SAF ftp server: [/hsaf/WP6000/precipitation/WG_groups/WG3-inca/documentation](ftp://hsaf/WP6000/precipitation/WG_groups/WG3-inca/documentation) .

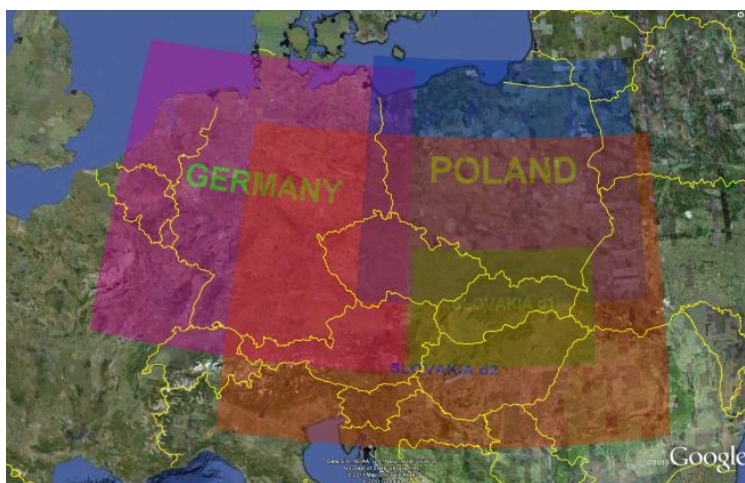


Figure 15 Coverage of Europe by the INCA and RADOLAN systems

4.4.1 INCA system

The INCA (Integrated Nowcasting through Comprehensive Analysis) analysis and nowcasting system is being developed primarily as a means of providing improved numerical forecast products in the nowcasting and very short range forecasting. It should integrate, as far as possible, all available data sources and use them to construct physically consistent analyses of atmospheric fields. Among the input data sources belong:

- NWP model outputs in general (P, T, H, clouds ...)
- Surface station observations (T, precipitation)
- Radar measurements (reflectivity, currently 2-d, 3-d in development)
- Satellite data (CLM, Cloud type, in development for use in precipitation analysis)
- Elevation data (high resolution DTM, indication of flat and mountainous terrain, slopes, ridges, peaks)

The INCA system provides:

- **High-resolution analyses** – interest of validation WG-3
- Nowcasts
- Improved forecasts

of the following variables:

- Temperature (3-d field)
- Humidity (3-d)
- Wind (3-d)
- **Precipitation (2-d)** – interest of validation WG-3
- Cloudiness (2-d)
- Global radiation (2-d)

The INCA precipitation analysis is a combination of station data interpolation including elevation effects, and radar data. It is designed to combine the strengths of both observation types, the accuracy of the point measurements and the spatial structure of the radar field. The radar can detect precipitating cells that do not hit a station. Station interpolation can provide a precipitation analysis in areas not accessible to the radar beam.

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The precipitation analysis consists of the following steps:

- i. Interpolation of station data into regular INCA grid (1x1 km) based on distance weighting (only nearest 8 stations are taken into account to reduce bull-eyes effect)
- ii. Climatological scaling of radar data by means of monthly precipitation totals of raingauge to radar ratio (partial elimination of the range dependence and orographical shielding)
- iii. Re-scaling of radar data using the latest rain gauge observations
- iv. Final combination of re-scaled radar and interpolated rain gauge data
- v. Elevation dependence and orographic seeding precipitation

In the final precipitation field the raingauge observations are reproduced at the raingauge station locations within the limits of resolution. Between the stations, the weight of the radar information becomes larger the better the radar captures the precipitation climatologically.

Important factor affecting the final precipitation analysis is accuracy and reliability of the raingauge stations. In order to eliminate the influence of raingauge stations providing evidently erroneous data, the SHMÚ is developing the blacklisting technique which temporarily excludes such stations from the analysis. Currently, the stations can be put into the blacklist only manually but development of the automated blacklisting is expected in near future.

4.4.2 RADOLAN system

RADOLAN is a routine method for the online adjustment of radar precipitation data by means of automatic surface precipitation stations (ombrometers) which has started on a project base at DWD in 1997. Since June 2005, areal, spatial and temporal high-resolution, quantitative precipitation data are derived from online adjusted radar measurements in real-time production for Germany.

The data base for the radar online adjustment is the operational weather radar network of DWD with 16 C-band sites on the one hand, and the joined precipitation network of DWD and the federal states with automatically downloadable ombrometer data on the other hand. In the course of this, the precipitation scan with five-minute radar precipitation data and a maximum range of 125 km radius around the respective site is used for the quantitative precipitation analyses. Currently, from more than 1000 ombrometer station (approx. 450 synoptic stations AMDA I/II-and AMDA III/S-of DWD; approx. 400 automatic precipitation stations AMDA III/N of DWD; approx. 150 stations of the densification measurement network of the federal states) the hourly measured precipitation amount is used for the adjustment procedure.

In advance of the actual adjustment different preprocessing steps of the quantitative radar precipitation data are performed. These steps, partly already integrated in the offline adjustment procedure, contain the orographic shading correction, the refined Z-R relation, the quantitative composite generation for Germany, the statistical suppression of clutter, the gradient smoothing and the pre-adjustment. Further improvements of these procedures are being developed.

Precipitation distribution of the rain gauge point measurements

Precipitation distribution of the areal original radar measurements

RADOLAN precipitation product

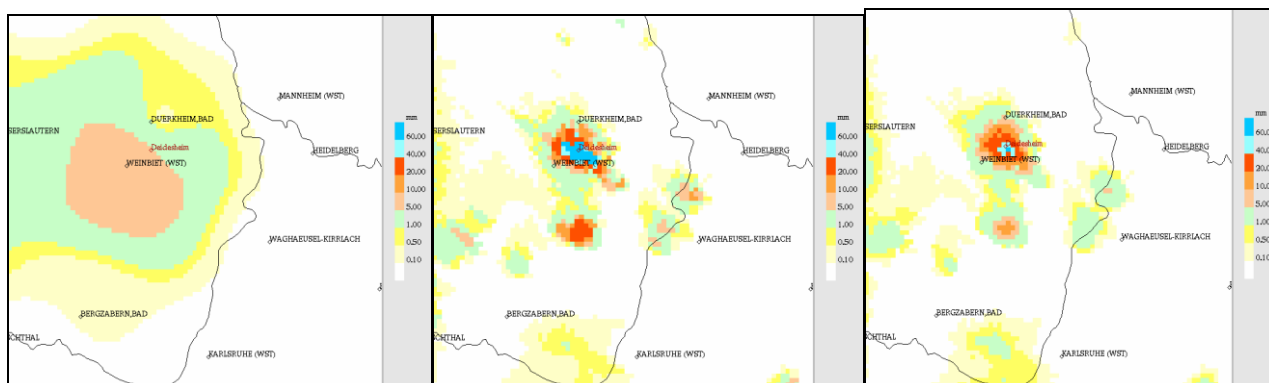


Figure 16 Procedure of the RADOLAN online adjustment (hourly precipitation amount on 7 August 2004 13:50 UTC)

In order to collect more detailed information about both types of systems a questionnaire was elaborated and completed by Slovakia, Poland and Germany. The questionnaire provided details such as geographical coverage (see Fig. 17), input data inventory or availability of different instantaneous and cumulated precipitation products.

The final version of the questionnaire is shown in the next table and is also available as annex 5.

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Group of information	Item	GERMANY	POLAND	SLOVAKIA domain1	SLOVAKIA domain2
Availability of documentation for INCA or similar (German) system [Yes/No]	If possible please attach link or documentation	Dokumentation received during Helsinki validation meeting	Documentation available from ZAMG	Documentation available from ZAMG	Documentation should be issued in future
Definition of geographical area covered by INCA or similar (in Germany) system	Grid size in pixels	900x900	741x651	501x301	1193x951
	Min longitude	3.5943 E	13.82 E	15.99231 E	8,9953784943 E
	Max longitude	15.71245 E	25.334 E	23.09630 E	25,9996967316 E
	Min latitude	46.95719 N	48.728 N	47.13585 N	45,0027313232 N
	Max latitude	54.73662 N	55.029 N	50.14841 N	53,000579834 N
	Space resolution	1 km	1 km	1 km	1 km
Input data	Number of radars in network	Composite of 16 national radars	Composite of 8 national radars	Composite of 2 national radars	Composite of 5 international radars
	Number of precipitation stations	1300	475 (Poland only)	397 (SHMU, CHMI, ZAMG, IMWM)	TBD
	Blacklist for precipitation stations [Yes/No]	?	Yes	Yes	Yes
Density of raingauge stations	Map of density of precipitation stations [Yes/No]	?	TBD	TBD	TBD
Output data	Instantaneous precipitation based only on raingauge network, time resolution, timelines	5 min	No	Yes, 15 min	Yes, 15 minute
	Instantaneous precipitation based only on radar network, time resolution, timelines	5 min	No	Yes, 5 minute	Yes, 5 minute
	Instantaneous precipitation based on combined raingauge and radar network, time resolution, timelines	5 min	Yes, 10 minutes	Yes, 5 minutes	Yes, 5 minutes
	Cumulative precipitation based only on raingauge network, time intervals, timelines	5 min, 1,3,6,12,18,24 hours	No	Yes, min 5 min, available 1,3,6,12,24 hours	Yes, min 5 min, available 1,3,6,12,24 hours
	Cumulative precipitation based only on radar network, time intervals, timelines	5 min, 1,3,6,12,18,24 hours	No	Yes, min 5 min, available 1,3,6,12,24 hours	Yes, min 5 min, available 1,3,6,12,24 hours
	Cumulative precipitation based on combined raingauge and radar network, time intervals, timelines	5 min, 1,3,6,12,18,24 hours	Yes, min 10 minutes, available in future	Yes, min 5 min, available 1,3,6,12,24 hours	Yes, min 5 min, available 1,3,6,12,24 hours
Dates for selected case studies	Case 1	will be set	No	29.3.2009	
	Case 2		No	1.-3.6.2010	
	Case 3		No	20.6.2010	
	Case 4		No	15.-16.8.2010	
	Case 5		No		
Availability of own software for upscaling INCA data into native satellite grid	H01	yes	No	No	No
	H02	yes	No	No	No
	H03	yes	No	No	No
	H04	no	No	No	No
	H05	yes	No	No	No
	H06	yes	No	No	No

Table 14 INCA Questionnaire

4.4.3 Some conclusions

The INCA system as a potential tool for the precipitation products validation is available in Slovakia and Poland, in both countries being run in pre-operational mode. It is still relatively new system undergoing continuous development. More sophisticated algorithms of the precipitation analysis (e.g. assimilation of the 3-D radar data) can be expected from its development in frame of the ongoing INCA-CE project.

In Germany similar precipitation analysis system called RADOLAN is being run operationally. This tool is already used for validation of the H-SAF precipitation products in this country.

The accuracy and reliability of the raingauge stations significantly affect final precipitation analysis of the INCA or INCA-like systems and therefore need to be checked. In order to solve this problem an

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automated blacklisting technique is going to be developed at SHMÚ (currently blacklisting is used in manual mode).

The software for upscaling the INCA precipitation field into the H-SAF products grid will have to be developed. Since the grids of INCA and RADOLAN have similar horizontal resolution to the common radar grid, the radar upscaling techniques can be applied also on the INCA or RADOLAN data. In frame of the unification of the validation methodologies the same common upscaling software could be shared between both radar and INCA working groups in the future.

4.5 Ground data in Belgium (IRM)

4.5.1 Radar data

The network

Belgium is well covered with three radars (see **next figure**). Further radar is currently under construction in the coastal region.

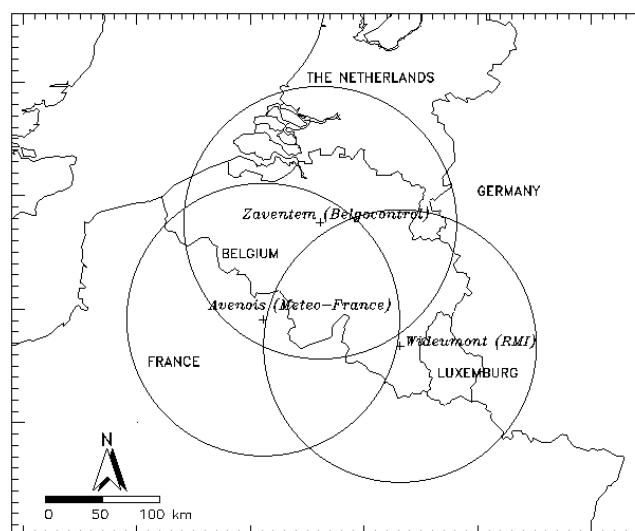


Figure 17 Meteorological radar in Belgium

The instruments

These are Doppler, C-band, single polarization radars with beam width of 1° and a radial resolution of 250 m. Data are available at 0.6, 0.66 and 1 km horizontal resolution for the Wideumont, Zaventem and Avesnois radars respectively.

In this report, only the Wideumont radar has been used. The data of this radar are controlled in three steps.

Data processing

First, a long-term verification is performed as the mean ratio between 1-month radar and gauge accumulation for all gauge stations at less than 120 km from the radar. The second method consists in fitting a second order polynomial to the mean 24 h (8 to 8 h local time) radar / gauge ratio in dB and the range; only the stations within 120 km and where both radar and gauge values exceed 1 mm are taken into account. The third method is the same as the second but is performed on-line using the 90 telemetric stations of the SETHY (Ministry of the Walloon Region). Corrected 24 h images are then

calculated. New methods for the merging of radar and raingauge data have been recently evaluated (Goudenhoofdt and Delobbe 2009)¹. In this report, only instantaneous radar images are used.

4.6 Ground data in Bulgaria (NIMH)

4.6.1 Rain gauge

The network

The maximum number of available raingauges for this project is 37, distributed over 3 basins.

The average distance between stations is about 7 km, with a very high variance. Generally in the plain area distance is lower than in the mountainous areas



Figure 18 Distribution of the raingauge stations of Iskar River Basin

¹ Goudenhoofdt E. and L. Delobbe, 2009: "Evaluation of radar-gauge merging methods for quantitative precipitation estimates". *Hydrol. Earth Syst. Sci.*, 13, 195-203.

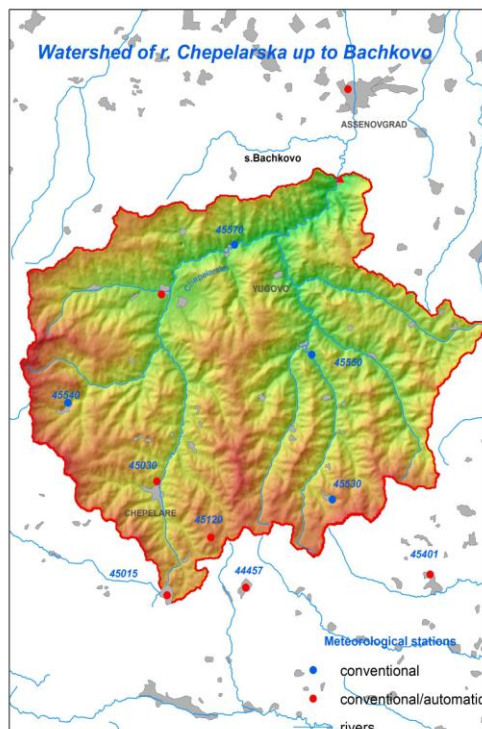


Figure 19 Distribution of the raingauge stations of Chepelarska River Basin

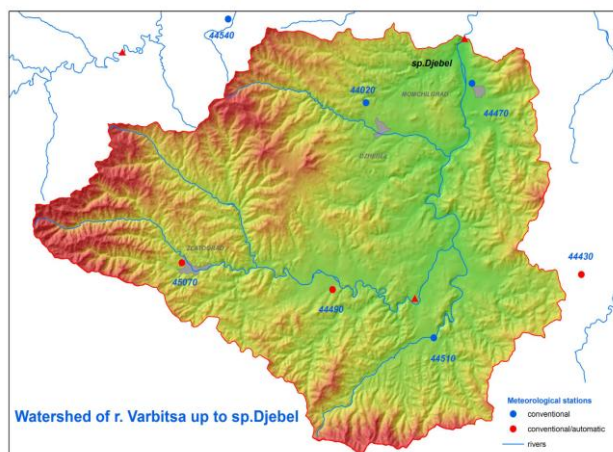


Figure 20 Distribution of the raingauge stations of Varbica River Basin

The instrument

The following information should be provided in this section:

- Tipping bucket with heating (measures the precipitation with increments of 0.1 mm) - quality index of the measurements (between 1 and 10) - 7-8.
- Weighing type measurement with heating rim (measures the precipitation with increments of 0.1 mm) - quality index of the measurements (between 1 and 10) - 8-9.
- Conventional precipitation gauges type Wild measuring 24 hourly totals of precipitation

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The rainrate is given only by the automatic stations for a 60 minutes interval. Those stations are located in Varbica and Chepelarska river basins. There are no automatic stations in Iskar river basin.

Data processing

There is quality control on the data.

In this Project the point-like gauges data are interpolated for using Co kriging interpolation of the ground measurements taking into account orography .

4.7 Ground data in Germany (BfG)

The H-SAF products are validated for the territory of Germany by use of two observational ground data sets: SYNOP - precipitation data based on the network of synoptical stations, provided by the German Weather Service (DWD) and RADOLAN-RW - calibrated precipitation data based on the radar network of DWD and calibrated by DWD by use of measurements at precipitation stations.

Data	Number/Resolution	Time interval	Delay	Annotation
Synoptical stations	~ 200	6h / 12h	Near-real-time	
Precipitation stations	~ 1100	hourly	Near-real-time	Automatic precipitation stations
RADOLAN RW	16 German radar sites, ~1 km x ~1 km	1 hour,	Near-real-time	Quantitative radar composite product RADOLAN RW (Radar data after adjustment with the weighted mean of two standard procedures)

Table 15 Precipitation data used at BfG for validation of H-SAF products

4.7.1 Rain gauge

The network

The data used are compiled from ~1300 rain gauges. About 1000 are operated by DWD while about 300 are operated by other German authorities. The average minimum distance between stations is 17 km.

The instruments

The measurement instruments are precipitation sensors OTT PLUVIO of Company Ott^{2 3}. They continually and precisely measure quantity and intensity of precipitation in any weather, based on balance principle with temperature compensation (heated funnel) and by an electronic weighing cell. The absolute measuring error is less than 0.04 mm for a 10 mm precipitation amount and the long-term (12months) stability is better than 0.06 mm. The operating temperature ranges from –30°C to +45°C. The minimum detected quantity (sensitivity) is 0,05 mmh⁻¹. The maximum possible measured rain rate is 3000 mmh⁻¹. The operational accumulation interval theoretically is one minute.

The data processing

Continuous, automatic measurement of liquid and solid precipitation data are collected, accumulated (intervals: from 1hour until 1day) and provided as SYNOP tables by DWD. These data are error

² http://www.ott.com/web/ott_de.nsf/id/pa_ottpluvio2_vorteile.html?OpenDocument&Click=

³ Precipitation amount and intensity measurements with the Ott Pluvio, Wiel Wauben, Instrumental Department, INSA-IO, KNMI, August 26, 2004

corrected and quality controlled in four steps with checks of completeness, climatologic temporal/spatial consistency and marginal checks.

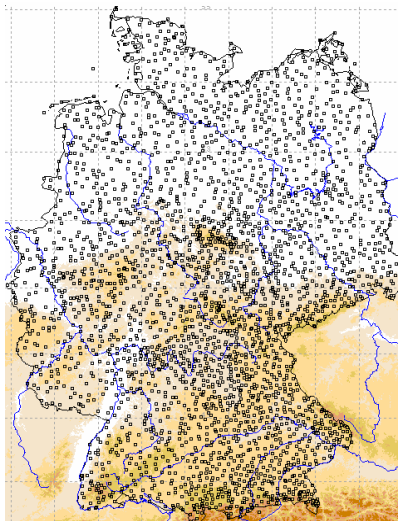


Figure 21 Network of rain gauges in Germany



Figure 22 Pluvio with Remote Monitoring Module

4.7.2 Radar data

Radar-based real-time analyses of hourly precipitation amounts for Germany (RADOLAN) is a quantitative radar composite product provided in near-real time by DWD. Spatial and temporal high-resolution, quantitative precipitation data are derived from online adjusted radar measurements in real-time production for Germany. Radar data are calibrated with hourly precipitation data from automatic surface precipitation stations.⁴

4

http://www.dwd.de/bvbw/appmanager/bvbw/dwdwwwDesktop?_nfpb=true&_windowLabel=dwdwww_main_book&T14609949251144921180881gsbDocumentPath=Navigation%2FWasserwirtschaft%2FUnsereLeistungen%2FRadarniederschlagsprodukte%2FRADOLAN%2Fradolan_node.html%3F_nnn%3Dtrue&switchLang=en&_pageLabel=dwdwww_spezielle_nutzer_forschung_fkradar

The combination of hourly point measurements at the precipitation stations with the five-minute-interval radar signals of the 16 weather radars (C-Band Doppler) provides gauge-adjusted hourly precipitation sums for a ~1km x ~1km raster for Germany in a polar stereographic projection.

Radar site	Latitude (N)	Longitude (E)	WMO No.	Radar site	Latitude (N)	Longitude (E)	WMO No.
München	48° 20' 14"	11° 36' 46"	10871	Rostock	54° 10' 35"	12° 03' 33"	10169
Frankfurt	50° 01' 25"	08° 33' 34"	10630	Ummendorf	52° 09' 39"	11° 10' 38"	10356
Hamburg	53° 37' 19"	09° 59' 52"	10147	Feldberg	47° 52' 28"	08° 00' 18"	10908
Berlin-Tempelhof	52° 28' 43"	13° 23' 17"	10384	Eisberg	49° 32' 29"	12° 24' 15"	10780
Essen	51° 24' 22"	06° 58' 05"	10410	Flechtingen	51° 18' 43"	08° 48' 12"	10440
Hannover	52° 27' 47"	09° 41' 54"	10338	Neuheilenbach	50° 06' 38"	06° 32' 59"	10605
Emden	53° 20' 22"	07° 01' 30"	10204	Türkheim	48° 35' 10"	09° 47' 02"	10832
Neuhaus	50° 30' 03"	11° 08' 10"	10557	Dresden	51° 07' 31"	13° 46' 11"	10488

Table 16 Location of the 16 meteorological radar sites of the DWD

Radarverbund des DWD mit 150 km Radien

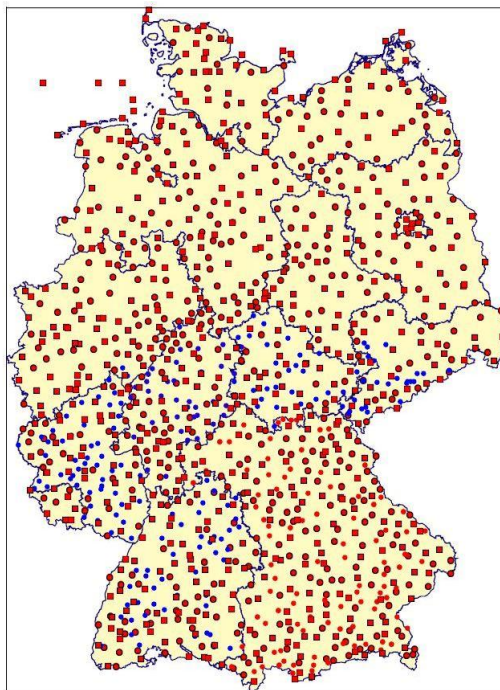
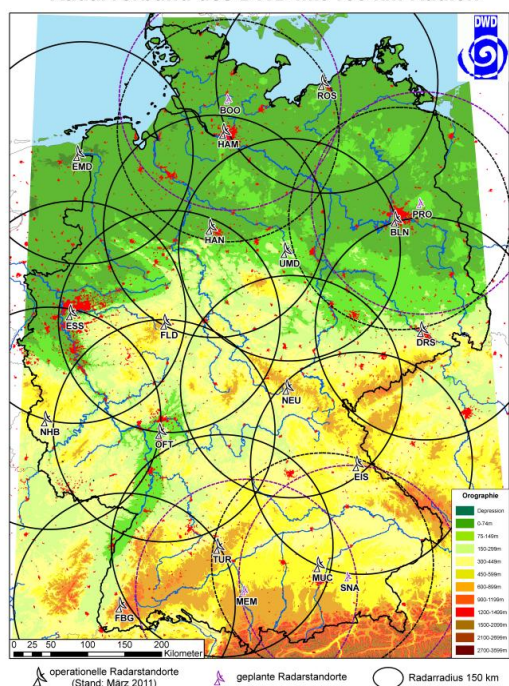


Figure 23 Left: radar compound in Germany (March 2011) ; Right: location of ombrometers for online calibration in RADOLAN; squares: hourly data provision (about 500), circles: event-based hourly data provision (about 800 stations) .

The flowchart of online calibration method applied in RADOLAN is depicted in next figure.

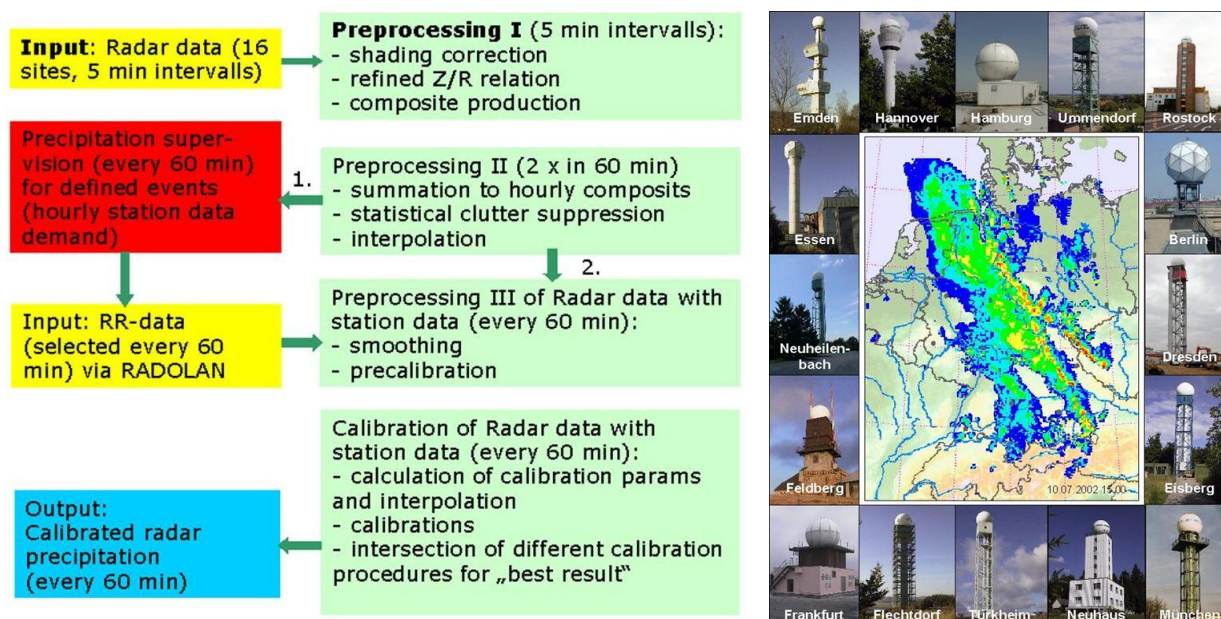


Figure 24 Flowchart of online calibration RADOLAN (DWD, 2004)

4.8 Ground data in Hungary (OMSZ)

4.8.1 Radar data

The network

The main data used for validation in Hungary would be the data of meteorological radars. There are three C-band dual polarized Doppler weather radars operated routinely by the OMSZ-Hungarian Meteorological Service. The location and coverage of the three Hungarian radars are shown in next figure the measurement characteristics are listed in Table 18.

All three radars are calibrated periodically, with an external (calibrated) TSG, the periodicity is kept every 3 months.

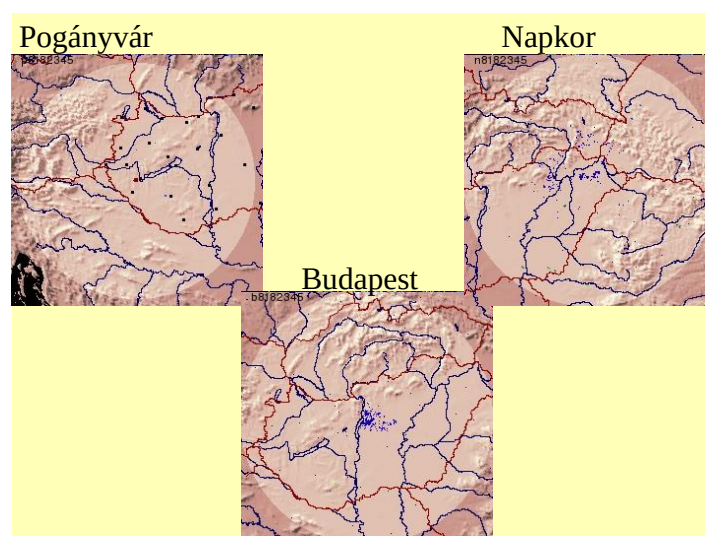


Figure 25 The location and coverage of the three meteorological Doppler radars in Hungary

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Year of installation	Location	Radar type	Parameters measured
1999	Budapest	Dual-polarimetric Doppler radar	Z, Z _{DR}
2003	Napkor	Dual-polarimetric Doppler radar	Z, Z _{DR} , K _{DP} , Φ _{DP}
2004	Poganyvar	Dual-polarimetric Doppler radar	Z, Z _{DR} , K _{DP} , Φ _{DP}

Table 17 Main characteristics of the Hungarian radar network

The instruments

The Hungarian radar network is composed by three Doppler radars, which are measuring in the C-band, mainly at same frequencies. The scan strategy is the same for all the radars, the Budapest radar has a resolution lower than the two other radars which are newer types. The parameters of the instruments and the measurement campaigns are listed in next table.

	Budapest	Napkor	Poganyvar
Frequency band	C-Band, 5625MHz	C-Band, 5610MHz	C-Band, 5610MHz
Polarization (Single/Double)	single	single	single
Doppler capability (Yes/No)	Yes	Yes	Yes
Scan strategy: elevations, maximum nominal range distance, range resolution	scan freq: 15 min Elevaions(deg): 0 0.5 1.1 1.8 2.7 3.8 5.1 6.6 8.5 Range 240 Km Resolution:500m	scan freq: 15 min Elevaions(deg): 0 0.5 1.1 1.8 2.7 3.8 5.1 6.6 8.5 Range 240 Km Resolution:250m	scan freq: 15 min Elevaions(deg): 0 0.5 1.1 1.8 2.7 3.8 5.1 6.6 8.5 Range 240 Km Resolution:250m

Table 18 Characteristics of the three radar instruments in Hungary

The data processing

Radar measurements are influenced by many error sources that should be minimized as much as possible. As such, in case of the Hungarian radar data many correction methods are applied, or planned to be applied int he near future to filter out false radar reflectivity measurements. Clutter removal, and WLAN filter is already implemented int he processing chain of all three radar data; and a filter to disregard signals below 7dBz is also applied because in general, these data is not coming from real rain drops, but false targets.

According to experiences, beam blockage can result in serious underestimation of precipitation amounts (e.g. behind the Börzsöny mountains at the north of Budapest). So the bleam blockage

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correction is planned to be implemented during year 2012. Also, the attenuation correction (the attenuation of electromagnetic waves in water environment, water drops) is planned for 2012.

Hungary does not apply VPR (Vertical Profile Reflectivity) correction.

Precipitation intensity is derived from radar reflectivity with the help of an empirical formula, the Marshall-Palmer equation ($R=a*Z^b$, where $a=200$, $b=1.6$). From the three radar images a composite image over the territory of Hungary is derived every 15 minutes applying the maximum reflectivity in one column method, in order to make adjustments in overlapping regions.

Description of instantaneous and accumulated radar product used in HSAF Validation Activities

Rain gauge correction

The non-corrected precipitation field can be corrected by rain gauge measurements. In Hungary, we do not make corrections to instantaneous 15 minutes radar data. In our institute, we only use a correction for the total precipitation for 12 and 24 hour periods.

For the 3h and 6h accumulated products, we use a special method to accumulate rainfalls: we interpolate the 15-minutes measurements for 1-minute grid by the help of displacement vectors also measured by the radar, and then sum up the images which we got after the interpolation. It is more precise especially when we have storm cells on the radar picture, because a storm cell moves a lot during 15 minutes and thus we do not get continuous precipitation fields when we sum up only with 15.minutes periods. This provides satisfying results. However, there is still a need for rain-gauge adjustment because there are obviously places (behind mountains) that the radar does not see.

The radars are corrected with rain gauge data every 12 hours. The correction method using rain gauge data for 12 hour total precipitation consists of two kinds of corrections: the spatial correction which becomes dominant in the case of precipitation extended over a large area, whereas the other factor, the distance correction factor prevails in the case of sparse precipitation. These two factors are weighted according to the actual situation. The weighting factor depends on the actual effective local station density, and also on the variance of the differences of the bias between radar and rain gauge measurements. On the whole, we can say that our correction method is efficient within a radius of 100 km from the radar. In this region, it gives a final underestimation of about 10%, while at bigger distance; the underestimation of precipitation fields slightly increases. Besides, we also produce 12 hour total composite images: first the three radar data are corrected separately, and then the composite is made from them. The compositing technique consists of weighting the intensity of each radar at a given point according to the distance of the given point from the radars. This is also true for the 24-hourly accumulations.

Resolution, projection, threshold of detection

The resolution of the radar data used for validation is 2km by 2km. This is true for the accumulated and the instantaneous products as well. As We have already mentioned, the threshold of detection in Hungary is 7dB. Hungarian radar data is available operationally in stereographic (S60) projection.

References

Péter Németh: Complex method for quantitative precipitation estimation using polarimetric relationships for C-band radars. Proceed. of 5th European Radar Conference (ERAD), Helsinki (Finland); <http://erad2008.fmi.fi/proceedings/extended/erad2008-0270-extended.pdf>

4.9 Ground data in Italy (DPC, Uni Fe)

4.9.1 Rain gauge

The network

The maximum number of available raingauges is about 1800, irregularly distributed over the surface. On the average, however, a number of stations have low quality data, failure or data transmission problems and their data are missing (-9999 recorded). This number of no data stations is highly varying on hourly/daily basis and ranges from few units to a hundred. In case of data acquired but not transmitted/recorded, the first transmitted measure is the cumulated value over the time when the data were not transmitted.

The average minimum distance between closest stations is about 9.5 km, with a very high variance: in some regions (such as Tuscany in central Italy) it is below 5 km, while in Emilia Romagna (Po Valley) it is more than 20 km. A study of the decorrelation distance between stations as function of the mutual distance has been carried out for the 2009 dataset. The decorrelation distance is defined as the minimum distance between two observations that makes the Pearson correlation coefficient between the two measures decrease below e^{-1} . Results are shown in next figure, where the decorrelation distance is plotted as function of the distance between stations. It appears that there is a large variability of this parameter from higher values (around 60 km for cold months when large precipitating systems dominate and reduces to roughly 10 km when small scale convection is more likely to occur (warm months).

This points out that the distribution of gauges could be able to describe the spatial structures of precipitation fields in case of wintertime rainfall, while may be inadequate for spring/summer convective events.

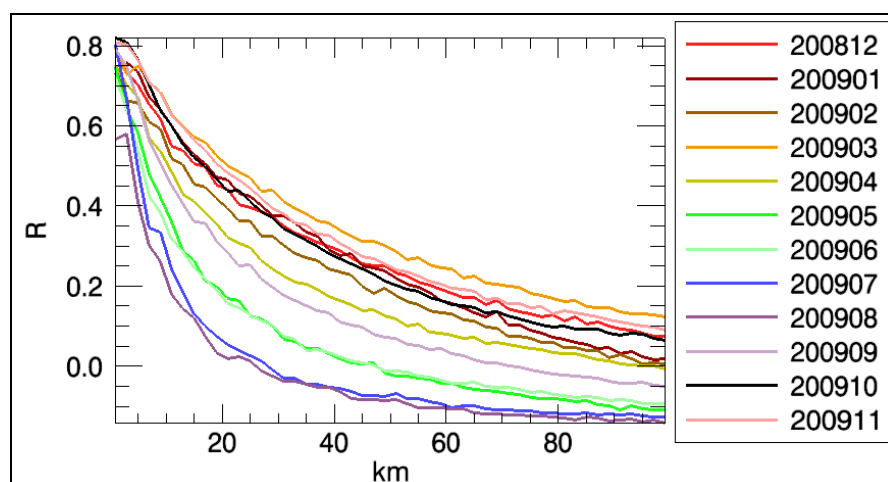


Figure 26 Correlation between rainrates detected by two close by stations as function of the distance between the two stations. Colors refer to the month along 2009

In next figure the distribution of working stations over Italy is shown for a given day.

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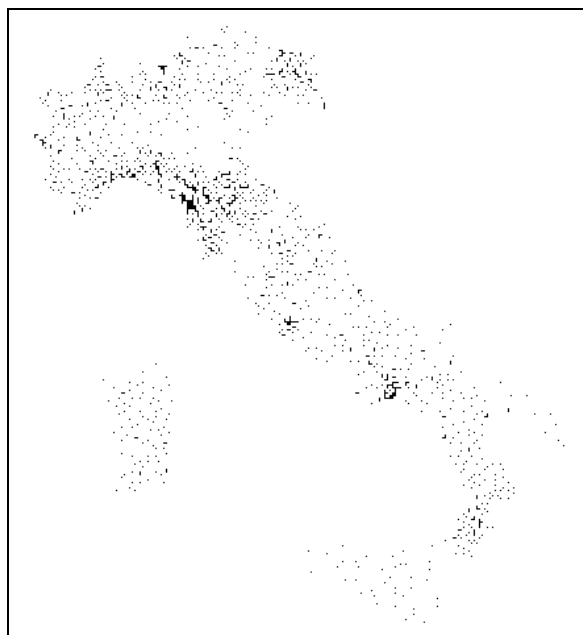


Figure 27 Distribution of the raingauge stations of the Italian network collected by DPC

The instruments

The following information should be provided in this section:

- All the available raingauge are of tipping bucket type;
- Most of the raingauge have a minimum detected quantity of 0.2 mm, others have 0.1 mm.
- The maximum rainrate that can be measured by the gauges ranges between 300 and 500 mm⁻¹ over one minute, depending on the manufacturer.

The rainrate is measured over different cumulation intervals by the different local administrations managing the network, but the data disseminated are all integrated over 60 minutes.

At the moment, the National network made available by DPC provides only hourly data, Shorter cumulation times could be available for case studies after specific agreements with local management authorities.

Only a small subset (about 300 stations) of gauges have heated funnel, especially in alpine regions (such as Valle d'Aosta and Piedmont), and this is a clear source of errors in both summer (due to hailfall) and in autumn/winter (due to snowfall).

The data processing

No quality control is performed on the data right now.

In this Project the point-like gauges data are interpolated by using the Barnes method (Barnes, 1964; Koch et al, 1983) widely used to interpolate station data. It works by defining a regular output grid (5x5 km in our case) and a “radius of influence” of each station (in our case it was 10 km). The point information from a raingauge is “spread” in the neighbour by an exponential function, limited by the influence radius, and the rainfall value for each grid-point is computed as the contribution of all the closest measurements.

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The resulting grid is a 5x5 km regular grid with 240 columns and 288 lines. Moreover, a Digital elevation model is used to provide a mask of Italy in order to: 1) screen out sea-pixels too far from the coastlines and 2) process the pixels with the elevation above sea level.

4.9.2 Radar data

The network

The Italian radar data have been not used for the validation of the current version of H01 but the verification of the satellite product with those data is in progress. The results will be presented at the next review of the project.

The Italian Department of Civil Protection (DPC) is the authority leading the national radar coverage project in order to integrate the pre-existent regional systems, made of ten C band fixed regional installations (five of them polarimetric and one transportable X-band polarimetric radar), two systems owned by the Italian company for air navigation services (ENAV), and three managed by the Meteorological Department of the Italian Air Force (AMI).

After its completion, the Italian radar network will include twenty-five C-band radars (including seven polarimetric systems) and five transportable dual-polarized X-band radars (next figure). The Italian Department of Civil Protection is developing the radar network in Southern Italy and, thanks also to the fruitful collaborations with Regional Authorities, ENAV and AMI, integrated all the existing radars in one national network with a clear advantage for both severe weather monitoring and civil protection purposes.

National Weather Radar Coverage - 125km

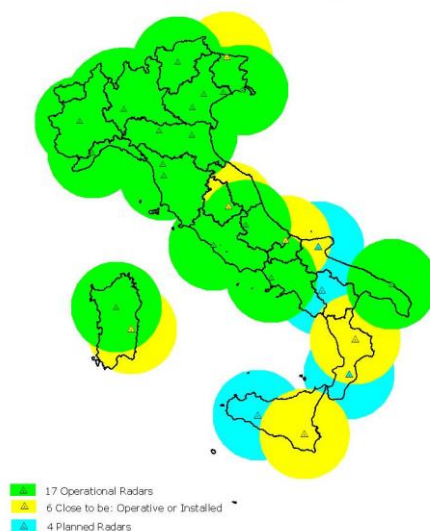


Figure 28 Italian radar network coverage

The existing sixteen C-band weather radars that belong to Regional Authorities ENAV and AMI are listed below:

- Bric della Croce (Owner: Regione Piemonte; Polarization: on going upgrade to polarimetry)
- Settepani (Owner: Regione Piemonte and Regione Liguria; Polarization: dual)
- San Pietro Capofiume and Gattatico (Owner: Regione Emilia Romagna; Polarization: dual)
- Monte Macaion (Owner: Regione Trentino Alto Adige and Provincia autonoma Trento; Polarization: single)

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- Teolo and Loncon (Owner: Regione Veneto; Polarization: single)
- Monte Midia (Owner: Regione Abruzzo; Polarization: single)
- Monte Rasu (Owner: Regione Sardegna; Polarization: single)
- Fossolon di Grado (Owner: Regione Friuli Venezia Giulia; Polarization: single)
- Linate and 12) Fiumicino (Owner: ENAV; Polarization: single)
- Brindisi (Owner: Italian Air Force; Polarization: single)
- Grazzanise (Owner: Italian Air Force; Polarization: single)
- Pisa, (Owner: Italian Air Force; Polarization: single)
- Istrana, (Owner: Italian Air Force; Polarization: single)

The first C-band radar of new generation, directly managed by DPC (located in Tuscany, Italy), is operational since the beginning of 2008, whereas six C-band radars (including two dual-polarized systems) will be operational by the end of 2008 (see Figure 29). As an example, the national mosaic CAPPI at 2000 m is shown in next figure relatively to the event of 04/18/08 at 0015 U.T.C.

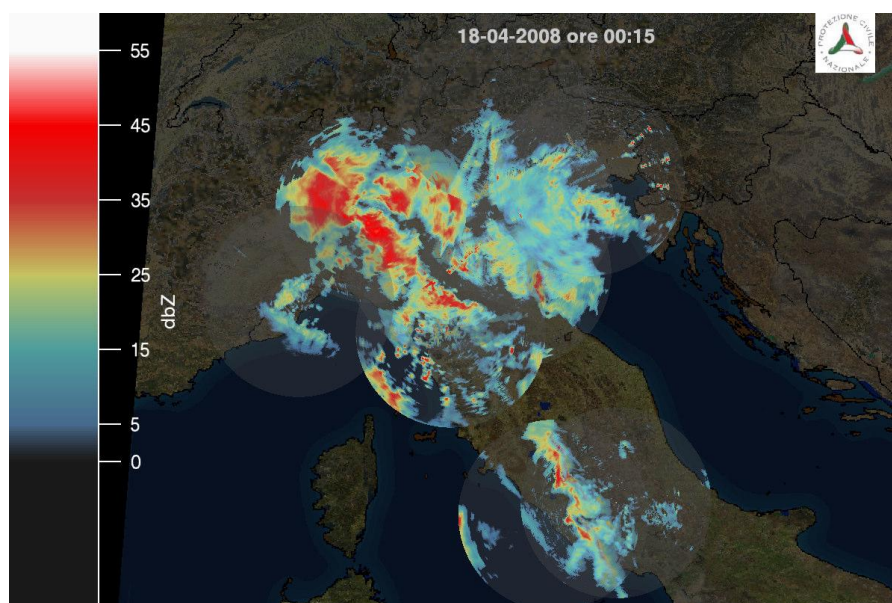
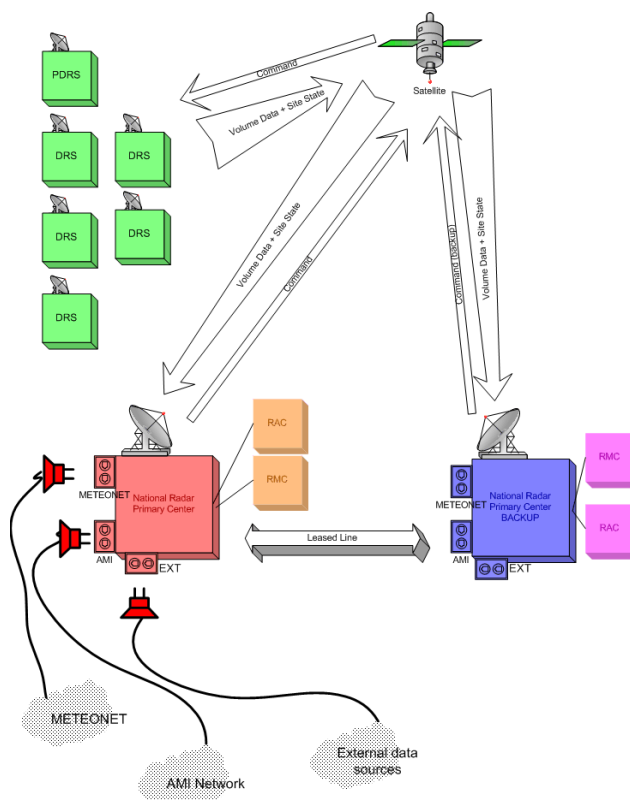


Figure 29 Graphical mosaic of reflectivity (CAPPI at 2000 m) for the event of 04/18/08 at 0015 U.T.C.

As depicted before, each Doppler Radar System either dual or single-polarized (PDRS or DRS) are connected by satellite links to the two National Radar Primary Centres (RPC), located in Roma (DPC) and Savona (CIMA Research Foundation) in order to mainly ensure the remote control (through the RRC server) and products generation (through the RPG server). The RPC located in Savona works as “backup centre” in order to continuously ensure the system functioning. The subsystem RAC (Radar Archive Centre) is devoted to archive and manage radar data and products by means of a relational database. The generated products are then disseminated to all institutions composing the national network.

**Figure 30 Architecture of the Italian radar network**

Data processing

Data processing and product generation are here briefly described. In particular, attenuation correction, hydrometeor classification, vertical profile of reflectivity correction and rainfall estimation will be treated in the following sections

Radar data quality

As known, any fruitful usage of radar data either for quantitative precipitation estimation or just for operational monitoring, must deal with a careful check of data quality. Figure 31 schematically shows the operational processing chain that is applied within the system DATAMET[®] (software system for radar remote control, product generation, visualization, system maintenance, and data archive) developed by DATAMAT S.P.A. Ground clutter, anomalous propagation, beam blockage effects are routinely mitigated through the application of the decision-tree method proposed by Lee et al., (1995) for single polarized systems. Dual-polarized systems provide additional observables such as differential reflectivity, correlation coefficient (and their texture) that can be used to further reinforce the traditional techniques. Furthermore, as soon as the polarimetric systems directly managed by DPC will be operational (end of summer 2008), the property of the rain medium at vertical incidence are planned to be used for differential reflectivity calibration according to the procedure proposed by Gorgucci et al. (1999). Redundancy of polarimetric variables will also be used for absolute calibration (Gourley et al., 2005).

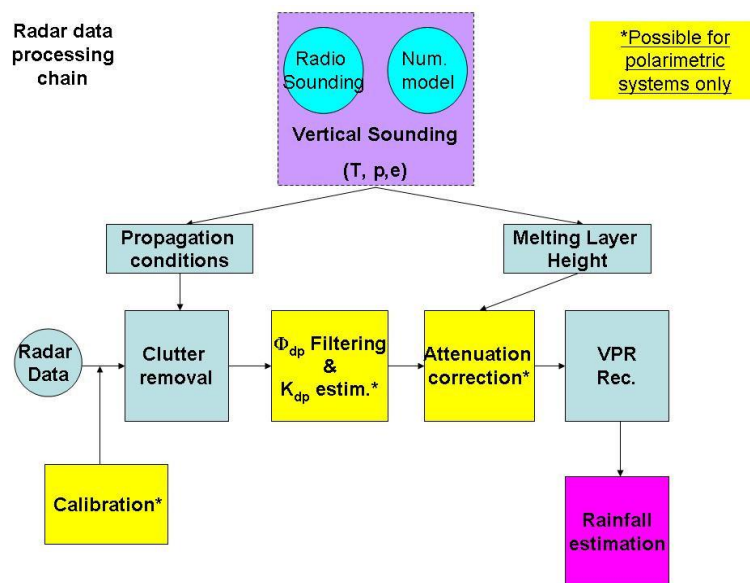


Figure 31 Schematic representation of radar data processing chain

Attenuation correction and hydrometeor classification Polarimetric radar systems enable the use of reliable algorithms for correcting rain path attenuation. Based on the paradigm that specific attenuation $a_{h,dp}$ and specific differential phase K_{dp} ($K_{dp}=0.5 \text{ dFdp/dr}$) are linearly related in rain ($a_{h,dp} = g_{h,dp} K_{dp}$), cumulative attenuation effects can be corrected through the use of F_{dp} (Carey et al., 2000).

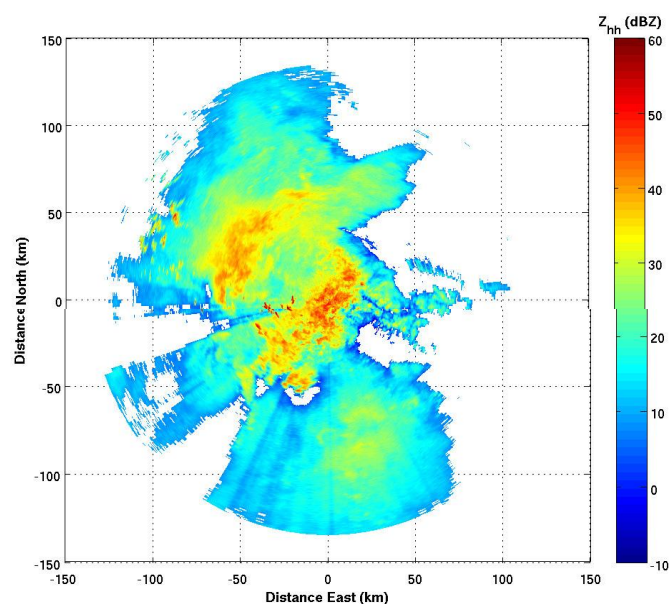
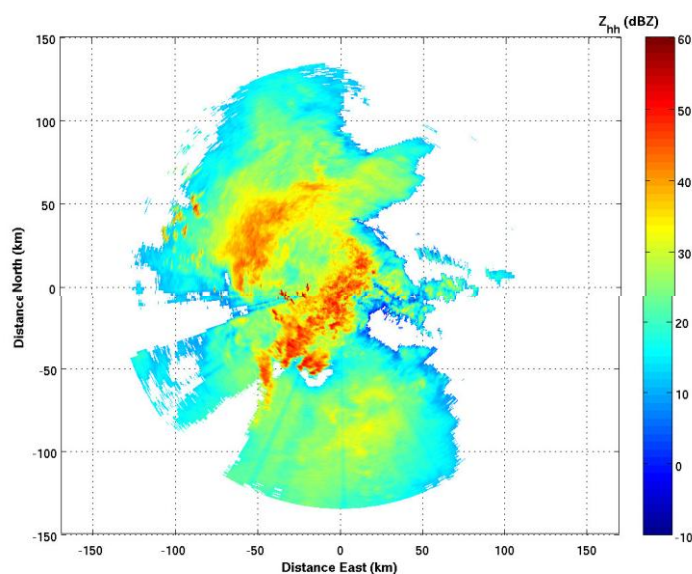
a) Observed**b) Corrected**

Figure 32 Measured (upper panel) and attenuation corrected (lower panel) PPI (1.0 deg) of reflectivity observed on 09/14/08 at 0500 U.T.C. by the polarimetric radar operated by Piemonte and Liguria regions

Although, several approaches with different degree of sophistication have been proposed in the last years, the procedure (named APDP) proposed in Vulpiani et al. (2007) has been chosen to be implemented for its physical adaptability and operationally-oriented architecture. APDP (Adaptive PhiDP method) is an iterative correction of attenuation, based on the use of F_{dp} , that taking advantage from the classification of hydrometeors (Marzano et al., 2006, 2007), adapt the coefficients $g_{h,dp}$ to the observed physical conditions.

As an example, previous figure shows the 1.0 degree PPI of measured (upper panel) and attenuation corrected (lower panel) reflectivity observed on 09/14/08 at 0500 U.T.C. by the polarimetric radar (located in mount Settepani) operated by Piemonte and Liguria regions. Next figure shows the hydrometeor classes detected by the classification algorithm corresponding to the event illustrated before.

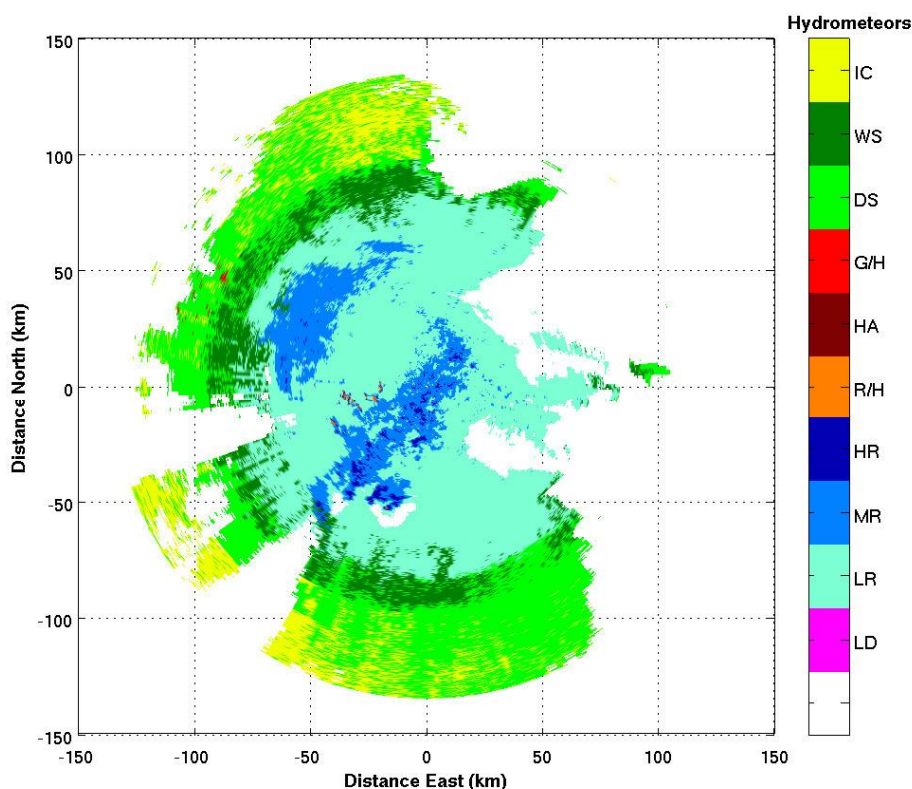


Figure 33 Hydrometeor classes as detected by the classification algorithm starting from the radar variables observed on 09/14/08 at 0500 U.T.C. by the polarimetric radar operated by Piemonte and Liguria regions

Note: LD (Large Drops), LR (Light Rain), MR (Moderate Rain), HR (Heavy Rain), R/H (Rain/ Hail mixture), HA (Hail), G/H (Graupel or small Hail), DS (Dry Snow), WS (Wet Snow), IC (Ice Crystals).

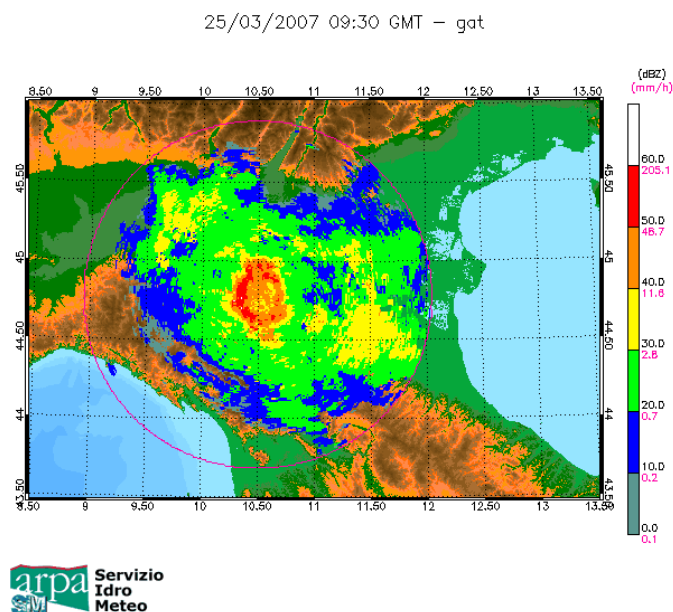
Reconstruction of vertical profile of reflectivity

Rainfall estimation might be heavily perturbed by the presence of melting snow due to the enhancement of reflectivity factor (caused by the increase in size and dielectric constant), without a corresponding increase of rain rate. This well known problem is usually handled by retrieving the Vertical Profile of Reflectivity (VPR) and correcting the observed measures.

The algorithm developed by ARPA-SIM for VPR retrieval and correction is currently under test in order to be implemented within the DATAMET system. It is based on the computation of mean VPR shape (Germann and Joss, 2002) and, assuming it to be uniform in the whole radar domain, on the retrieval of the reflectivity at the desired level by the simple adding of a constant quantity (in dBZ units). The original algorithm is modified and integrated with a VPR diagnosis and analysis phase, to handle different operative problems (Fornasiero et al., 2008).

As an example, next figure shows the measured (upper panel) and VPR-corrected (lower panel) PPI of reflectivity observed on 03/25/07 at 0930 U.T.C. by the polarimetric radar located in Gattatico (Emilia Romagna, Italy).

.a)



b)

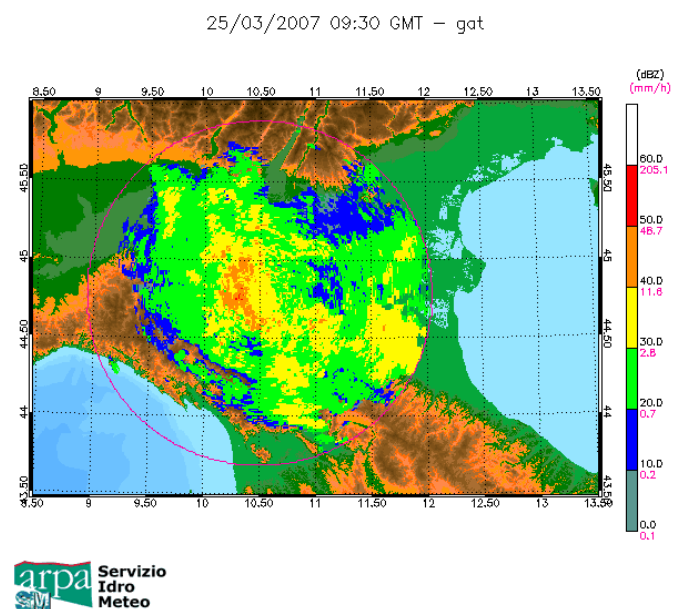


Figure 34 Measured (upper panel) and VPR corrected (lower panel) PPI of reflectivity observed on 03/25/07 at 0930 U.T.C. by the polarimetric radar located in Gattatico (Emilia Romagna, Italy)

Rainfall estimation

Quantitative rainfall estimation is one of the first application of the radar network. The estimation of rainfall at the ground takes advantage of the dense network of raingauges spread all over Italy. This

network is one of the most dense in the world with more than 1700 gages and it is used for tuning and correcting the operational Z-R algorithms of non-polarimetric radars.

In order to evaluate the benefits of upgrading the new radar installations to full-polarimetric radars and for considering the benefit of existing polarimetric radars, many studies have been carried on by Research Centres and Regional Authorities belonging to the network (e.g., Silvestro et al 2008). As an example, in next figure is shown the cumulated rainfall estimates versus gage measurements obtained for the event observed on 06/01/2006 by the dualpolarized C-Band radar of Mt. Settepani. The figure shows the comparison between a multi-parameter algorithm that uses polarimetric data (Silvestro et al., 2008) and a simple ZR relationship (Marshall-Palmer).

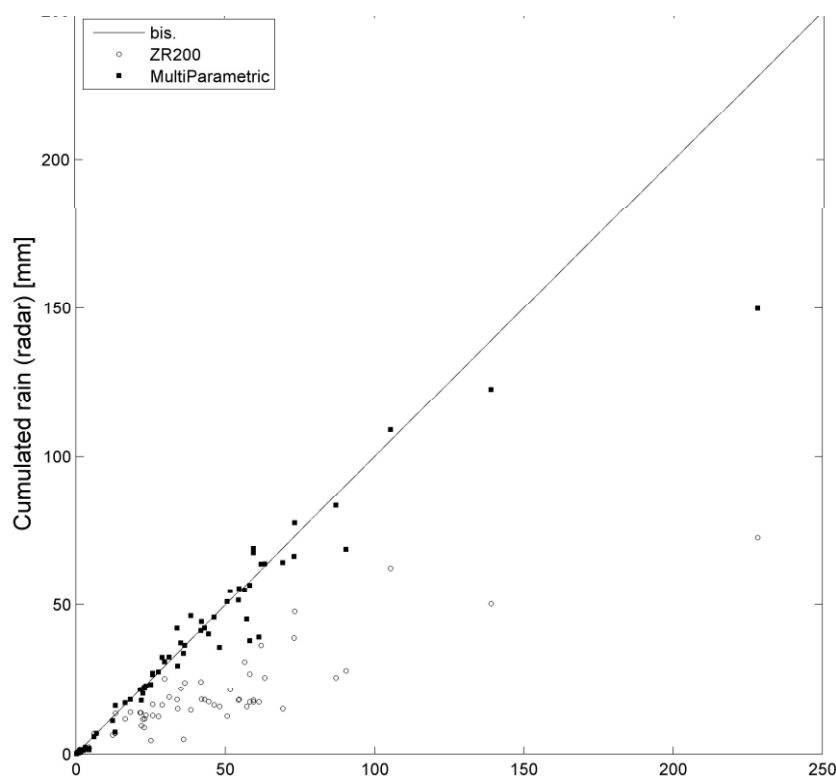


Figure 35 Cumulated radar rainfall estimates versus gage measurements for the event observed on 06/01/2006 by the dualpolarized radar located in Settepani (Liguria, Italy)

4.10 Ground data in Poland (IMWM)

4.10.1 Rain gauge

The network

The maximum number of rain gauges in the Polish ATS (Automatic Telemetric Station) national network is 950. Each ATS post is equipped with two independent rain gauges of the same sort. One of them is heated during the winter period and the other one is not. Therefore precipitation information is derived from 475 points at the time. Fact that rainfall is measured by two equally sensitive instruments two meters away from each other at the same post, enables to apply simple in situ data quality control during summertime. During winter non-heated rain gauge is covered with a cup to prevent it from being clogged by the ice and damaged. Because of that the precipitation information

derived from ATS network in winter cannot be verified using this method. It can be stated that during the wintertime precipitation information might be burdened by a slightly bigger measuring error. The number of rain gauges available for H-SAF validation activities varies from day to day due to operational efficiency of ATS network in Poland and depends on large number of independent factors. It can be stated that the number varies between 330 and 475 rain gauges for each day of operational work.

Mean minimum distance between precipitation measuring ATS posts (between each pair of rain gauges) in Polish national network is 13,3 km.

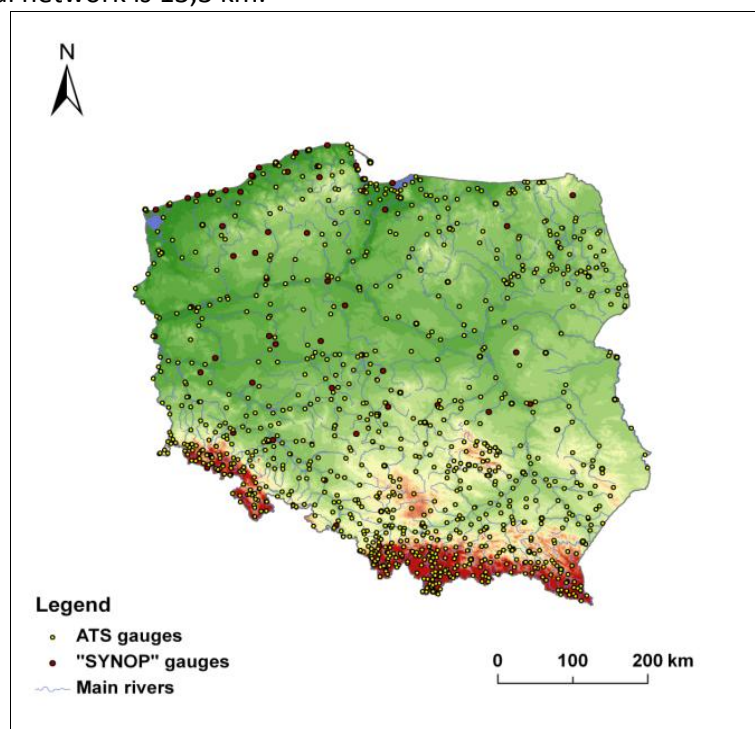


Figure 36 ATS national network in Poland

The instruments

All rain gauges working within Polish ATS national network are MetOne tipping bucket type instruments. Minimum detected quantity that can be measured by those rain gauges is 0,1 mm/h which means that each tilt of rain gauge bucket adds 0,1mm to the total sum of the measured precipitation. During very heavy precipitation events MetOne rain gauges tend to underestimate real precipitation by factor of 10%. Maximum measured rainrate (mmh^{-1}) by MetOne instruments in Poland was recorded in 5.06.2007 at ATSO Koscielisko Kiry at the foot of Tatra Mountains. The recorded values reached 65 mm/h. Operational cumulation interval (*min*) of ATS network rain gauges is set for 10 minutes and can be adjusted according to given needs. There is possibility to have very short cumulation intervals for case studies - theoretically 1 minute - but not on every given precipitation post. It depends on local DCS settings.

The data processing

As stated above the data quality control can be achieved by comparison on two rainfall datasets collected by two independent rain gauges at the same ATS post. It is done operationally during summertime. There is no such possibility during the winter because of lack of non-heated rain gauge

dataset. In case that one pair of rain gauges at the same ATS post provide two different rainfall readings the higher one is taken into account.

No specialization technique is used for standard validation process. However, for some case studies, the Natural Neighbor technique is applied for satellite and ground precipitation data. To match the precipitation information with satellite data spatial and temporal matching are applied.

- Spatial matching: for each given satellite pixel, the posts situated within that pixel were found. The pixel size was taken into account, however, its shape was assumed to be rectangular. If more than one rain gauge were found within one satellite pixel, the ground rain rate value was calculated as a mean of all rain gauges measurements recorded within that pixel;
- Temporal matching: satellite derived product is combined with the next corresponding ground measurement. As the ground measurements are made with 10 minute time resolution, the maximum interval between satellite and ground precipitation is 5 minutes.

4.11 Ground data in Slovakia (SHMU)

4.11.1 Rain gauge

The network

In Slovakia there are overall 98 automatic rain gauge stations potentially available for the H-SAF project. The real number of usable gauges varies with time because on average about 20 of them are out of operation.

Mean minimum distance between rain-gauges in the complete network is 7,74 km. Map of the rain gauge network in Slovakia containing also climatological and selected hydrological stations is shown in next figure.

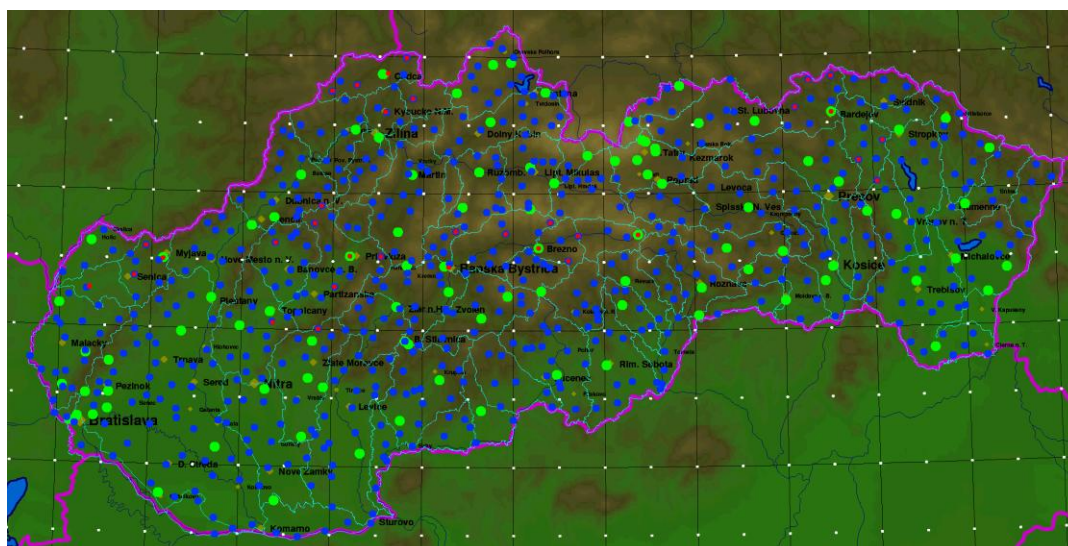


Figure 37 Map of SHMU rain gauge stations: green – automatic (98), blue – climatological (586), red - hydrological stations in H-SAF selected test basins (37)

The instruments

Type of all the automatic rain gauges is tipping bucket (without heating of the funnel). The gauges are able to measure precipitation rates ranging from 0,1 to 200 mm/h at 10 min operational accumulation

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interval. Shorter accumulation interval of 1 min is also possible which makes the instruments suitable for case studies in the H-SAF project.

The data processing

The rain gauge data are not used at SHMÚ directly for the H-SAF precipitation validation but they are utilized as the input to the INCA precipitation analysis system which is supposed to become a new validation tool. Prior the INCA analysis the rain gauge data are interpolated onto the regular 1x1 km grid using the inverse-distance-squared (IDS) interpolation method. Only the 8 nearest rain gauge stations are taken into account in the interpolation in order to reduce occurrence of precipitation bull-eyes artifact.

SHMÚ performs the offline automatic and manual quality check of the rain gauge data. In frame of the INCA system a quality control technique called blacklisting has been developed which avoids the data from systematically erroneous rain gauges to enter the analysis. Currently the blacklisting is used in manual mode only.

4.11.2 Radar data

The network

The Slovak meteorological radar network consists of 2 radars (see next figure). One is situated at the top of Malý Javorník hill near city Bratislava and second one is on the top of Kojšovská hora hill close to the city Kosice. Both are Doppler, C-band radars; the newer one at Kojšovská hora is able to measure also the dual polarization variables (non-operational).

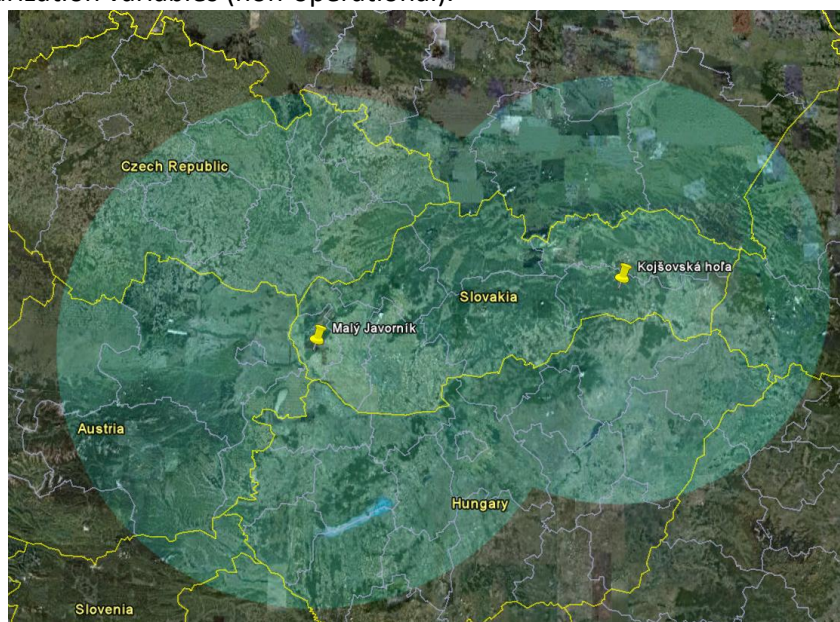


Figure 38 Map of SHMÚ radar network; the rings represent maximum operational range – 240 km for radar at Malý Javorník (left), 200 km for radar at Kojšovská hora (right)

The instruments

The radars are operated and technically maintained by SHMÚ. Receivers of radars are calibrated regularly by means of internal test signal generator (TSG). In case of radar at Malý Javorník calibration is performed every 3 months and in case of radar at Kojšovská hora every 1 month.

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The basic parameters of both SHMÚ radars are summarized in next table.

	Maly Javornik	Kojsovska hola
Frequency band	C-Band, 5600 MHz	C-Band, 5617 MHz
Polarization (Single/Double)	Single	Double (but so far only single pol. products generated)
Doppler capability (Yes/No)	Yes	Yes
Scan strategy: scan frequency, elevations, maximum nominal range distance, range resolution	Scan frequency: 5 min Elevations (deg): 0.2 0.7 1.4 2.5 3.8 5.4 7.3 9.5 13.0 17.0 25.0 Range: 240 Km Resolution: 1000m	Scan frequency: 5 min Elevations (deg): -0.5 0.0 0.5 1.0 1.5 2.5 4.0 6.0 10.0 20.0 Range: 200 Km Resolution: 125m

Table 19 Characteristics of the SHMÚ radars

The data processing

For ground clutter removal the Doppler filtering is used. In case of radar at Maly Javornik the frequency-domain IIR filter is used, at Kojsovska hola the Doppler filtering is supplemented with moving target identification (MTI) technique. Isolated radar reflectivity and Doppler velocity bins are removed by the Speckle removal filter. The data with signal to noise ratio below the specified threshold are also eliminated.

The measured radar reflectivity is corrected for atmospheric (clear-air) attenuation of the radar beam. Neither beam blocking correction nor vertical profile of reflectivity (VPR) is applied at SHMÚ. However implementation of the beam blocking correction is being considered for the H-SAF validation due to complicated orographical conditions in Slovakia.

Precipitation intensity is derived from radar reflectivity according to the Marshall-Palmer equation ($Z=a \cdot R^b$) with constant coefficients valid for stratiform rain ($a=200$, $b=1.6$). Polarimetric techniques for quantitative precipitation estimation in case of dual polarization radar at Kojsovska hola are not used because the measured polarimetric data are not operational (calibration would be required). Software filter for the RLAN interference detected by radars is currently in development at SHMÚ.

Radar composite based on CAPPI 2 km products from both radars is used for the H-SAF validation. The composition algorithm used selects the higher value measured by the two radars in the overlapping area.

No raingauge correction of the derived instantaneous precipitation is applied. Effect of elevating radar beam with increasing range and beam attenuation is reduced by limiting the validation area to rain effective range of 120 km for both radars in the composite.

The instantaneous precipitation products are provided in Mercator projection with approximately 1 km resolution. Threshold for precipitation detection is 0,02 mm/h. Time resolution of the current instantaneous products is 5 minutes, for the products prior to April 2010 it was 10 minutes and prior to August 2009 15 minutes.

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Precipitation accumulation in case of 3-hourly interval is based on integration of 5 (10 or 15) minutes instantaneous measurements in time period of 3 hours. Accumulated precipitation for intervals of 6, 12 and 24 hours is calculated as a sum of the 3-hourly accumulated precipitation. At least 92% of instantaneous measurements must exist in relevant time period for the 3-hourly accumulated product to be produced.

No rain gauge correction of the accumulated precipitation is applied but the same limitation of validation area is used as for the instantaneous product. Threshold for precipitation detection of the 3-hourly accumulated product is 0,5 mm. Geographical projection and space resolution of the accumulated products are the same as those of instantaneous product (see above).

For validation of H-SAF precipitation products it is necessary to know errors distribution of used ground reference data – in case of SHMÚ it is precipitation intensity and accumulated precipitation measured by Slovak radar network. For this purpose a study called “SHMU study on evaluation of radar measurements quality indicator with regards to terrain visibility” has been elaborated. To find distribution of errors in radar range next steps had to be done:

- simulations of terrain visibility by radar network using 90m digital terrain model
- statistical comparison of radar data against independent rain gauge data measurements
- derivation of dependence (regression equation) describing the errors distribution in radar range with regard to terrain visibility, based on rain gauge and radar data statistical evaluation
- computation of error distribution maps using regression equation and terrain visibility

Main results of this study are shown in next figure. It is evident that the best visibility of SHMU radars corresponds to the lowest URD-RMSE of 60% displayed by light violet colors. URD-RMSE is of quite homogeneous distribution with average of 69% in prevalent lowlands of Slovakia displayed by bluish colors. But in central and north-west mountainous areas this error exceeds 100%.

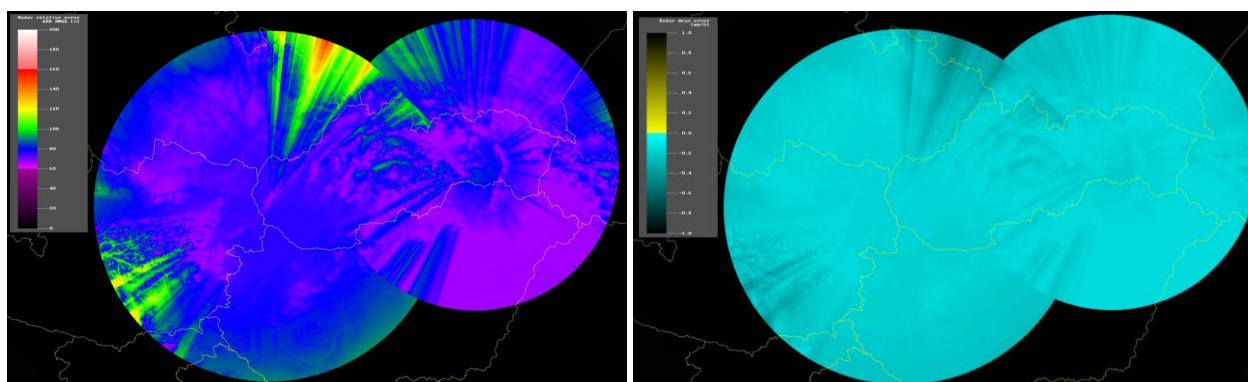


Figure 39 Map of relative RMSE (left) and Mean Error (right) over the SHMÚ radar composite

Similar studies that have been carried out in the PPVG on comparison of radar data with rain gauge data have shown in general that RMSE error associated with radar fields depends considerably on radar minimum visible height above the rain gauge especially in mountainous countries. In lowlands this dependence is not so significant, but not negligible. The reason can be the location of radar sites at the top of hills and impossibility of the lowest elevation to reach the lowland's surface. In case of Slovakia The URD-RMSE error of radar accumulated fields is between 60-90%, with an average URD-RMSE value of 69,3%. Mean Error specified for 24-hours cumulated precipitation is -4,42mm or converted into instantaneous precipitation -0,184 mm/h. RMSE specified for 24-hours cumulated precipitation is 9,48mm or converted into instantaneous precipitation 0,395 mm/h.

Complete SHMU study is available on the H-SAF ftp server:
/hsaf/WP6000/WP6100/precipitation/WG_groups/WG2-radar/WG-2-3_radar quality
indication_v1.doc

4.12 Ground data in Turkey

4.12.1 Rain gauge

The network

193 Automated Weather Observation Station (AWOS) located in the western part of Turkey are used for the validation of the satellite precipitation products in the HSAF project. The average distance between the AWOS sites is 27 km. The locations of the AWOS sites are shown in next figure.

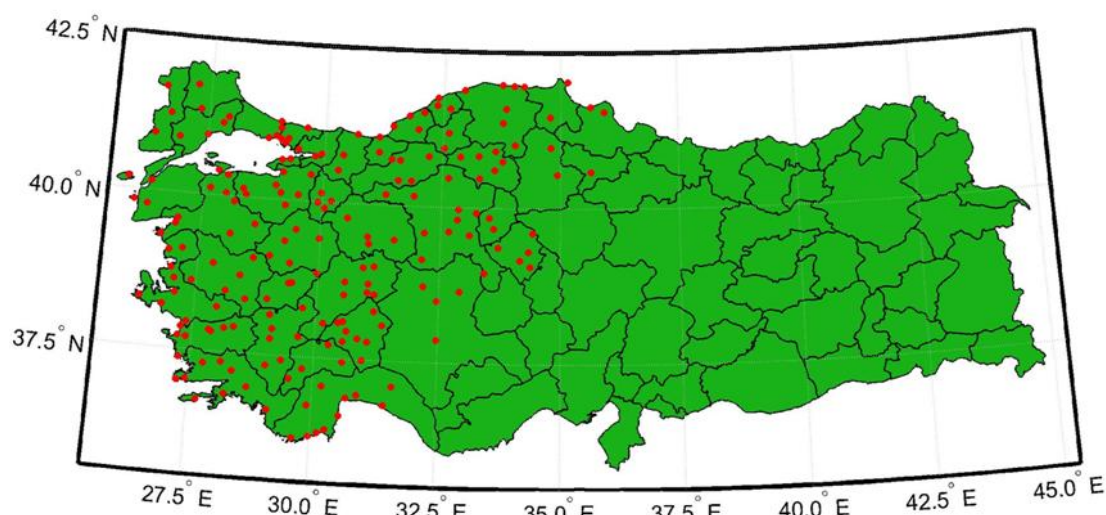


Figure 40 Automated Weather Observation System (AWOS) station distribution in western part of Turkey

The instruments

The gauge type of the network is tipping bucket where each has a heated funnel. The minimum detection capability of the gauge is 0.2mm per tip. In the maximum capacity of the instrument is 720 mm/h at most. The operational accumulation interval is 1 minute, so that alternative cumulation intervals such as 5, 10, 20, 30 minutes are possible.

Data processing

Quality control

High quality of the ground data is critical for performing the validation of the precipitation products. The validation results or statistics can provide meaningful feedbacks for the product developers and additionally the products can be used reliably only if there is a confidence present about the ground data at a certain level. For this reason, some predefined quality assurance (QA) tests are considered for the precipitation data in order to define the confidence level. First of all, a flagging procedure is defined as described in next table.

QA Flag Value	QA Status	Brief Description

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0	Good	Datum has passed all QA Test
1	Suspect	There is concern about accuracy of datum
2	Failure	Datum is unstable

Table 20 QA flags descriptions (modified from Shafer et al., 1999)

The precipitation data QA tests are summarized as follows.

Range Test

This test is used to see if any individual precipitation observation falls within the climatological lower and upper limits. The test procedures applied in the study are as follows.

IF $\text{Lim}_{\text{Lower}} \leq \text{Obser}_{j,t} \leq \text{Lim}_{\text{Upper}}$ **THEN** $\text{Obser}_{j,t}$ flag is ‘**Good**’

IF $\text{Obser}_{j,t} > \text{Lim}_{\text{Upper}}$ **OR** $\text{Obser}_{j,t} < \text{Lim}_{\text{Lower}}$ **THEN** $\text{Obser}_{j,t}$ flag is ‘**Failure**’

$\text{Lim}_{\text{Lower}}$ and $\text{Lim}_{\text{Upper}}$ thresholds are separately determined for each station on a monthly basis. At any specific site, all the observed monthly data is considered for determination of the upper and lower limits. By applying this test, each observation is flagged either by ‘Good’ or ‘Failure’ label depending on the comparison tests mentioned above.

Step Test

It is used to see if increment/decrement between sequential observations in time domain is in acceptable range or not. The applied test procedure is,

IF $|\text{Obser}_{j,t} - \text{Obser}_{j,t-1}| < \text{Step}_j$ **THEN** $\text{Obser}_{j,t}$ flag is ‘**Good**’

IF $|\text{Obser}_{j,t} - \text{Obser}_{j,t-1}| > \text{Step}_j$ **THEN** $\text{Obser}_{j,t}$ flag is ‘**Suspect**’

Step_j threshold is determined again for each site on a monthly basis. For each site, the dataset containing the absolute difference of the sequential observations is determined by considering the observations for the matching month. The 99.9 % cumulative histogram value of the dataset is set as the Step_j threshold for the related site and month.

Persistence Test

Persistence test is used to determine if any group of observations are due to instrument failures. The test procedure applied is defined as,

IF $T < \Delta$ **THEN** Flag for all Obser in T : ‘**Good**’

IF $T > \Delta$ **THEN** Flag for all Obser in T : ‘**Suspect**’

where T is the total number of the sequentially repeating observations forward in time and Δ is the possible maximum number of sequentially repeating observations. As in the other two tests, Δ threshold is determined for each site on a monthly basis. For any site, the data belonging to the same month is taken into account to determine the repeating number of the sequential observations. Then, 99.9 % cumulative histogram value of the repeating number dataset is assigned as the Δ amount for the corresponding site and month. Since there is a high possibility of no-precipitation data (zero), the sequential zero observations are excluded in this test during the determination of the Δ threshold amount and application of the test.

QA Test procedure

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By applying the control procedures of the QA test mentioned above, each individual precipitation observation receives three flags referring to the corresponding test. For the corresponding observation if all the test flag is not 'Good' then the observation is excluded from the validation process.

Use of spatialization technique

Due to the time and space structure of precipitation and to the sampling characteristics of both the precipitation products and observations used for validation, care has to be taken to bring data into comparable and acceptable range. At a given place, precipitation occurs intermittently and at highly fluctuating rates. Various maps, time series analysis, statistical and probabilistic methodologies are employed in the validation procedure classically, but some additional new aspects such as the spatial coverage verification model of point cumulative semivariogram (PCSV) approach (Şen and Habib, 1998) are proposed for usage in this work.

Each precipitation product within the H-SAF project represents a foot print geometry. Among these, H01 and H02 products represent an elliptical geometry while H03 and H05 have a rectangular geometry. On the other hand, the ground observation (rain gauge) network consists of point observations. The main problem in the precipitation product cal/val activities occurs in the dimension disagreement between the product space (area) and the ground observation space (point). To be able to compare both cases, either area to point (product to site) or point to area (site to product) procedure has to be defined. However, the first alternative seems easier. The basic assumption in such an approach is that the product value is homogenous within the product footprint. Next figure presents satellite foot print (FOV) centers of the H01 and H02 products, an elliptical footprint for the corresponding center (area within the yellow dots) and Awos ground observation sites. The comparison statistic can be performed by considering just the sites in the footprint area. Although this approach is reasonable on the average but it is less useful in spatial precipitation variability representation. The comparison is not possible when no site is available within the footprint area.

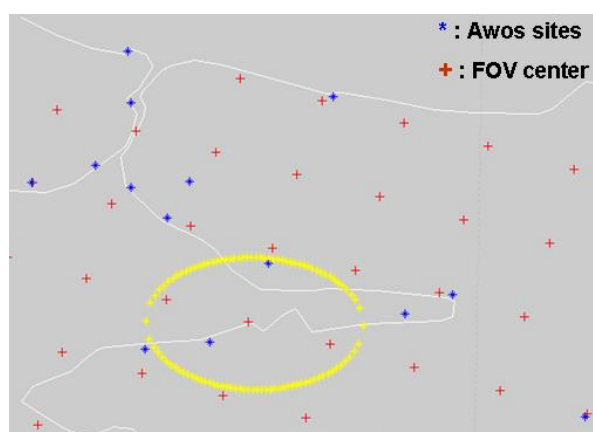


Figure 41 H01 and H02 products footprint centers with a sample footprint area as well as the Awos ground observation sites

Alternatively, the point to area approach is more appealing for the realistic comparison of the precipitation product and the ground observation. This approach is simply based on the determination of the reference precipitation field underneath the product footprint area. To do so, the footprint area is meshed and precipitation amounts are estimated at each grid point by using the precipitation observations at the neighboring Awos sites as shown in next figure. A 3x3 km grid spacing is

considered for the products with elliptical geometry while 2x2 km spacing is considered for the products with rectangular geometry. For any grid point, Awos sites within the 45 km for the time period of April-September (convective type) and 125km for the rest(stratiform type) are taken into consideration. At each grid point, the precipitation amount is estimated by,

$$Z_m = \frac{\sum_{i=1}^n W(r_{i,m}) Z_i}{\sum_{i=1}^n W(r_{i,m})} \quad (4.13.1)$$

where Z_m is the estimated value and $W(r_{i,m})$ is the spatially varying weighting function between the i -th site and the grid point m .

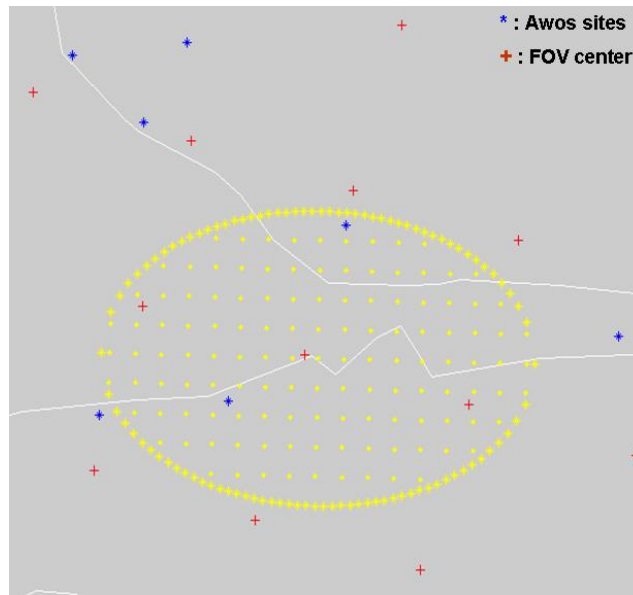


Figure 42 Meshed structure of the sample H01 and H02 products footprint

Determination of the $W(r_{i,m})$ weighting function in Equation 1 is crucial. In open literature, various approaches are proposed for determining this function. For instance, Thiebaux and Pedder (1987) suggested weightings in general as,

$$W(r_{i,m}) = \begin{cases} \left(\frac{R^2 - r_{i,m}^2}{R^2 + r_{i,m}^2} \right)^\alpha & \text{for } r_{i,m} \leq R \\ 0 & \text{for } r_{i,m} \geq R \end{cases} \quad (4.13.2)$$

where R is the radius of influence, $r_{i,m}$ is the distance from point i to point m to the point and α is a power parameter that reflects the curvature of the weighting function. Another form of geometrical weighting function was proposed by Barnes (1964) as,

$$W(r_{i,m}) = \exp \left[-4 \left(\frac{r_{i,m}}{R} \right)^\alpha \right] \quad (4.13.3)$$

Unfortunately, none of these functions are observation dependent but suggested on the basis of the logical and geometrical conceptualizations only. They are based only on the configuration, i.e. geometry of the measurement stations and do not take into consideration the natural variability of the

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meteorological phenomenon concerned. In addition, the weighting functions are always the same from site to site and time to time. However, in reality, it is expected that the weights should reflect to a certain extent the regional and temporal dependence behavior of the phenomenon concerned.

For the validation activities, the point cumulative semi-variogram technique proposed by Şen and Habib (1998) is used to determine the spatially varying weighting functions. In this approach, the weightings not only vary from site to site, but also from time to time since the observed data is used. In this way, the spatial and temporal variability of the parameter is introduced more realistically to the validation activity.

Matching approach

The temporal and spatial matching approaches are applied separately in the validation of the satellite products. As for the temporal matching, the product time is taken into account and 5 minute window($t-2$ to $t+3$) is considered for estimation of the average rainrate for each site.

For the spatial matching, the mesh grid size of 3kmX3km is constructed for each IFOV area. For each grid point, the rainrate is estimated by taking the 5 minute averaged rainrate amounts observed at the nearby AWOS sites within the radius distance of 45 km(for convective type) or 125 km(for stratiform type) considering the weighting of each site with respect to the grid point(Equation 1). The weighting amounts are derived from the spatially varying weighting functions obtained by using the semi-variogram approach(Şen and Habib,1998). Finally, the Gaussian filter is applied to the estimations at the mesh grid of the IFOV area to get the average rainrate. Then, this amount is compared with the satellite precipitation product amount for the validation purposes.

4.13 Conclusions

After these inventories some conclusions can be drawn.

The rain gauge in PPVG is composed by 3500 instruments across the 6 Countries: Belgium, Bulgaria, Germany, Italy, Poland, and Turkey. These data are, as usual, irregularly distributed over ground and are generally deduced by tipping bucket type instruments. Moreover most of the measurements are hourly cumulated. So probably the raingauge networks used in this validation activities are surely appropriated for the validation of cumulated products (1 hour and higher), while for the validation of instantaneous estimates the use of hourly cumulated ground measurements could introduce a large error. Moreover the revisiting time (3,4 hours) of H02 makes impossible or not reasonable to validate the product for 1-24 hours cumulated interval. The first object of PPVG (*Rain Gauge- WG*) in the next future it will be to quantitatively estimate the errors introduced in the validation procedure comparing the instantaneous satellite precipitation estimation with the rain gauge precipitation cumulated on different intervals (the Polish and Turkish data will be used for this purpose).

The rain gauge inventory has also pointed out that different approaches for the estimates matching are considered in the PPVG. The second steps in the next future will be to define the rain gauge spatial interpolation technique and to develop the related software.

The radar data in the PPVG is composed by 54 C-band radars across the 7 countries: Belgium, Germany, Hungary, Italy, Slovakia, Poland, Turkey. The rain gauge network responsible declared that the systems are kept in a relatively good status. The rain gauge inventory pointed out that different correction factors are applied. This means that the corresponding rainfall estimates are diverse, and

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the estimation of their errors cannot be homogenized. The first step in PPVG (*Radar –WG*) will be to define a quality index on the base of the study performed by the Slovakian team (Annex 4) and the scheme published by J. Szturc *et al* 2008. The main difficulty consists on the definition of a quality index computable for every radar networks of PPVG. The evaluation of this quality index will allow to evaluate the rain gauge error in the same way and to select the more reliable radar data in the PPVG.

In this chapter the first example of precipitation fields integration has been provided (Section 4.4.3): INCA and RADOLAN products. The INCA system, a tool for the precipitation products validation, is available in Slovakia and Poland, in both countries being run in pre-operational mode. In Germany similar precipitation analysis system called RADOLAN is being run operationally. This tool is already used for validation of the H-SAF precipitation products in Germany. The study performed in the PPVG (*INCA-WG*) showed that the accuracy and reliability of the raingauge stations significantly affect final precipitation analysis of the INCA or INCA-like systems. In order to solve this problem an automated blacklisting technique is going to be developed at SHMÚ (currently blacklisting is used in manual mode). The next step will be to develop the software for up-scaling the INCA precipitation field into the satellite product grid. The grids of INCA and RADOLAN have similar horizontal resolution to the common radar grid. The up-scaling software will allow to provide case study analysis and statistical score evaluation for future considerations on the opportunity to use these precipitation integration products in the H-saf validation programme.

5 Validation results: case study analysis

5.1 Introduction

As reported in the Chapter 3 the common validation methodology is composed of large statistic (multi-categorical and continuous), and case study analysis. Both components (large statistic and case study analysis) are considered complementary in assessing the accuracy of the implemented algorithms. Large statistics helps in identifying existence of pathological behaviour, selected case studies are useful in identifying the roots of such behaviour, when present.

This Chapter collects the case study analysis performed by PPVG on H02 for the year 2010. The Chapter is structured by Country / Team, one section each. The analysis has been conducted to provide information to the User of the product on the variability of the performances with climatological and morphological conditions, as well as with seasonal effects.

Each section presents the case studies analysed giving the following information:

- description of the meteorological event;
- comparison of ground data and satellite products;
- visualization of ancillary data deduced by nowcasting products or lightning network;
- discussion of the satellite product performances;
- indications to satellite product developers;
- indication on the ground data (if requested) availability into the H-SAF project.

In the future the PPVG will test the possibility to present case study analysis in the test sites, indicated by the hydrological validation team, in order to provide a complete product accuracy and hydrological validation analysis to the users.

5.2 Case study analysis in Belgium (IRM)

5.2.1 Case study: August 14th -17th, 2010

Description

This event has been select because convective precipitation occurred during 14 – 17 August and covering large parts of the study area during 15 and 16 August. A low was moving from Germany to The Netherlands (next figure). Warm air from Central Europe was lifted over oceanic cold air over the study area.

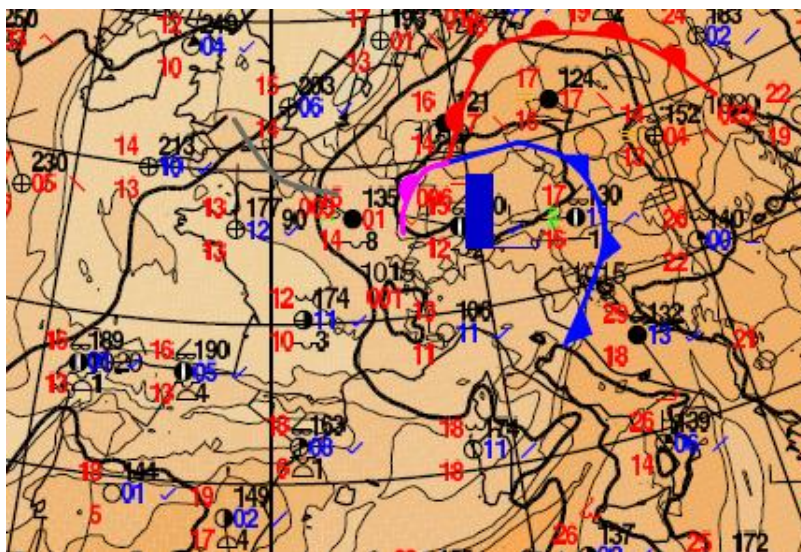


Figure 43 Synoptic situation on 15 August 2010 at 6 UTC (zoom in the surface map)

Data used

Products (H02) from August 14th at 6.00 UTC to August 17th at 18.00 UTC have been considered in this study. The total is 32 satellite passages, distributed as follows:

- 4 in the afternoon of August 14th;
- 4 in the morning of August 15th;
- 7 in the afternoon of August 15th;
- 8 in the morning of August 16th;
- 3 in the afternoon of August 16th;
- 6 in the morning of August 17th;

The ground data used for validation are the Wideumont radar instantaneous measurements, without rain-gauge adjustment. Radar data are available within 5 minutes around the satellite passage.

Comparison

Here are three examples of H02 files, compared with radar data upscaled to the same grid. The first two examples are observing the same scene from different satellites at noon of August 15th, while the third one refers to the early morning of August 16th.

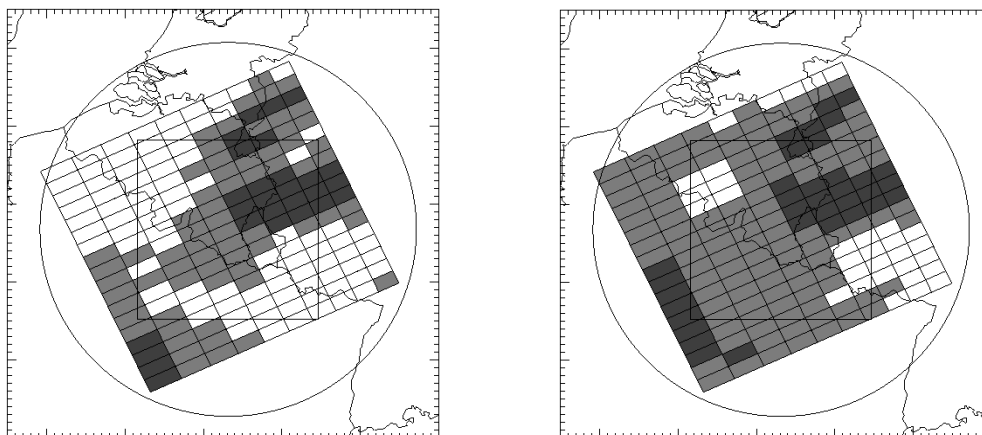


Figure 44 H02 image of August 15, 2010 at 12.08 (left) compared with upscaled radar at 12.10 (right). The scale corresponds to thresholds of 0.1, 1., and 10. mm h⁻¹

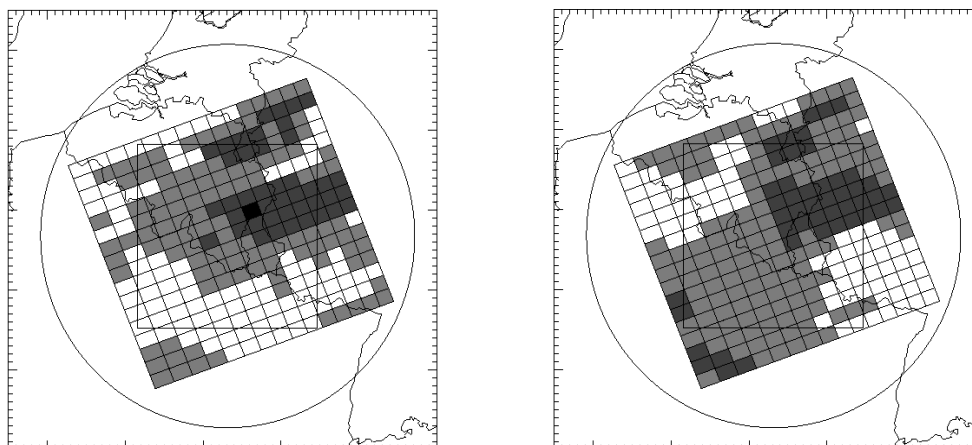


Figure 45 H02 image of August 15th, 2010 at 12.09 (left) compared with upscaled radar at 12.10 (right – the same radar image as above, but upscaled on a different grid). The scale corresponds to thresholds of 0.1, 1., and 10. mm h⁻¹

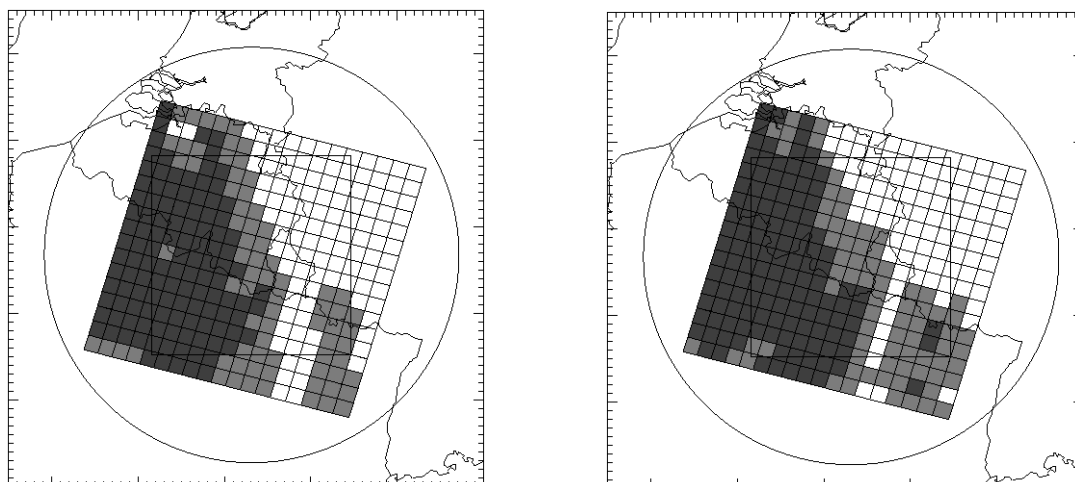


Figure 46 H02 image of August 16th, 2010 at 2.07 (left) compared with upscaled radar at 2.05 (right). The scale corresponds to thresholds of 0.1, 1., and 10. mm h⁻¹

We can see that in the noon case the matching is rather good and the images from two satellites are consistent in particular in detecting the precipitation cells in the North of the validation area. There is just a slight underestimation. In the morning case it is quite good.

Scores evaluation

The score evaluation results (Table 21) are quite good if compared to long period statistics, especially for what concerns correlation, POD and FAR. A slight underestimation is reported over all the case study (consistently with the long period statistics).

Sample	32
Mean error*	-0.43
Standard deviation*	1.37
Mean absolute error*	0.98
Multiplicative bias	0.72
Correlation coefficient	0.49
Root mean square error*	1.45
URD-RMSE	1.56
POD	0.62
FAR	0.22
CSI	0.52

Table 21 Scores obtained with the comparison with radar data (* in mm h⁻¹)

The time evolution of the fraction area with rain, the average rain rate over this area, the Equitable Threat Score (ETS), and the root mean square error (RMSE) is reported in the following figure:

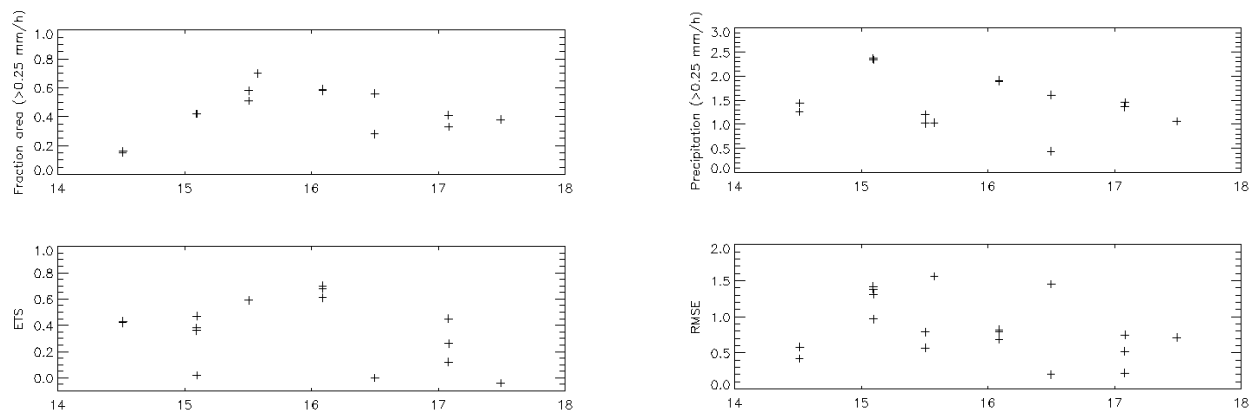


Figure 47 Time evolution of fraction area with rain, average rain rate over this area (threshold 0.25 mm/h), RMSE and ETS during the present case study

Conclusions

From qualitative and statistics comparison, it appears that for this case study (summer storm characterized by convective rainfall) the h02 product could reproduce the rainfall patterns with quite good confidence, slightly underestimating rainfall amounts.

5.2.2 Case study: August 22th -24th, 2010

Description

This event has been chosen because thunderstorms with intense precipitation resulted in local flooding in Belgium. The country was at the edge of a large anti-cyclone which was moving away towards South-East (next figure). Warm but humid and unstable air was brought from South-West whereas a cold front was moving from West.

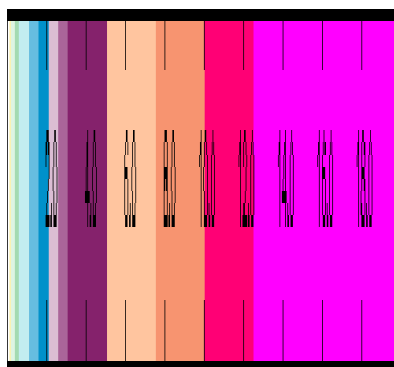


Figure 48 Surface map on 22 August 2010 at 06 UTC (MSLP and synoptic observations)

Data used

Products (H02) from August 22th at 6.00 UTC to August 24th at 12.00 UTC have been considered in this study. The total is 12 satellite passages, distributed as follows:

- 4 in the early afternoon of August 22th;
- 2 in the early morning of August 23th;
- 3 in the early afternoon of August 23th;
- 3 in the early morning of August 24th.

The ground data used for validation are the Wideumont radar instantaneous measurements, without rain-gauge adjustment. Radar data are available within 5 minutes around the satellite passage.

Comparison

Here are three examples of H02 files, compared with radar data upscaled to the same grid. The first is in the morning of August 23th, the second around noon, and the third one refers to the early morning of August 24th.

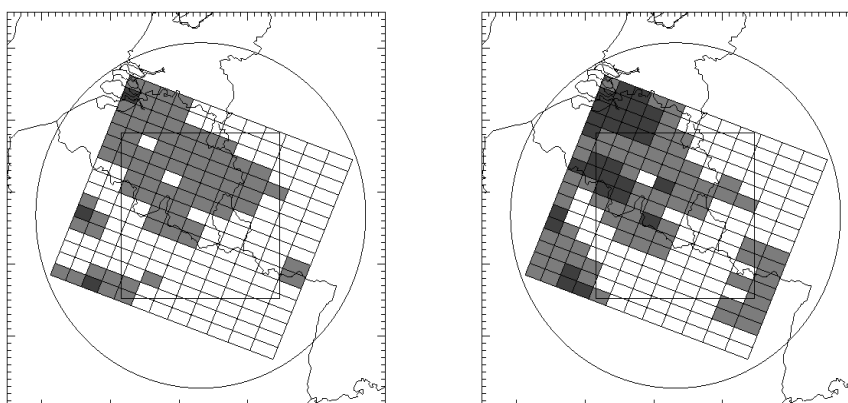


Figure 49 H02 image of August 23th, 2010 at 2.35 (left) compared with upscaled radar at the same time (right). The scale corresponds to thresholds of 0.1, 1., and 10. mm h-1

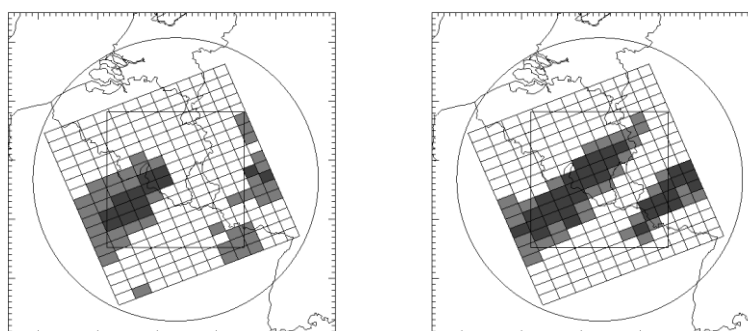


Figure 50 H02 image of August 23th, 2010 at 12.23 (left) compared with upscaled radar at 12.25 (right). The scale corresponds to thresholds of 0.1, 1., and 10. mm h-1

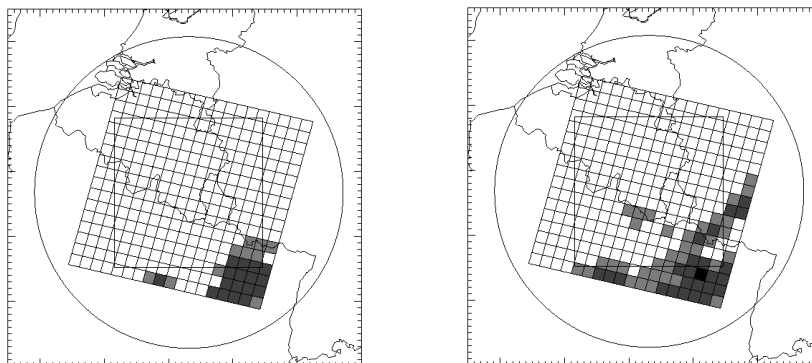


Figure 51 H02 image of August 23th, 2010 at 12.23 (left) compared with upscaled radar at 12.25 (right). The scale corresponds to thresholds of 0.1, 1., and 10. mm h⁻¹

We can see that in all the shown cases the satellite is able to detect the presence of rainfall in the area, but it tends to underestimate the extension and the amount of it.

Scores evaluation

The score evaluation results (Table 1) are not as good as the other summer case. They appear more aligned to the ones obtained in the long period analysis, with noticeable underestimation. This might be connected with the fact that in this case, the fraction of area interested by the rainfall is smaller (see Figure 52 and, for comparison, Figure 47).

Sample	12
Mean error*	-0.72
Standard deviation*	1.66
Mean absolute error*	1.06
Multiplicative bias	0.52
Correlation coefficient	0.41
Root mean square error*	1.73
URD-RMSE	0.95
POD	0.59
FAR	0.36
CSI	0.44

Table 22 Scores obtained with the comparison with radar data (* in mm h⁻¹)

The time evolution of the fraction area with rain, the average rain rate over this area, the Equitable Threat Score (ETS), and the root mean square error (RMSE) is reported in the following figure.

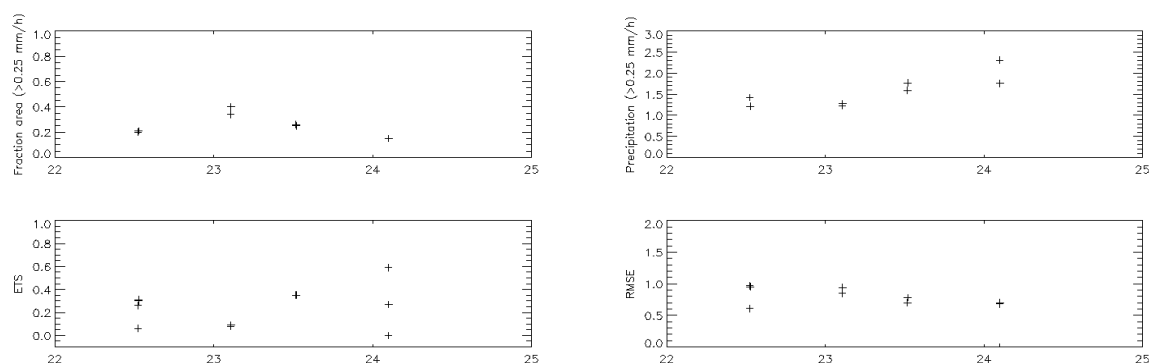


Figure 52 Time evolution of fraction area with rain, average rain rate over this area (threshold 0.25 mm/h), RMSE and ETS during the present case study

Conclusions

From qualitative and statistics comparison, it appears that for this case study the h02 product could reproduce the rainfall patterns, but regularly underestimating rainfall amounts and areas. The results, aligned with the ones of long period statistics, are sensibly worse than the ones obtained for the other summer case study, occurred just one week before.

5.2.3 Case study: November 12th - 15th, 2010

Description of the event

A wide area with low pressure extended from Scandinavia to Great Britain and made a very active precipitating perturbation stay over the country during several days (next figure) and result in high

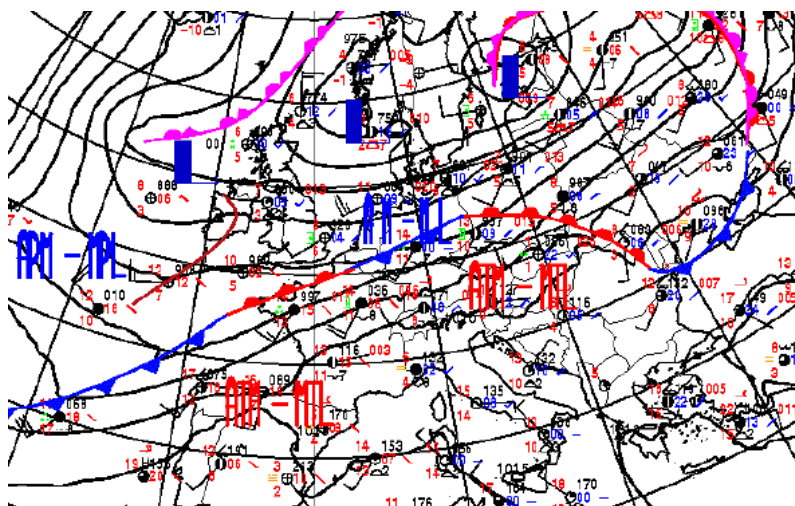


Figure 53 Surface map on 13 November 2010 at 06 UTC (MSLP and synoptic observations)

Data used

Products (H02) from November 12th at 0.00 UTC to November 15th at 18.00 UTC have been considered in this study. The total is 58 satellite passages, distributed as follows:

- 14 in the morning of November 12th;
- 2 in the early afternoon of November 12th;
- 9 in the morning of November 13th;
- 6 in the early afternoon of November 13th;
- 9 in the morning of November 14th;
- 6 in the early afternoon of November 14th;
- 7 in the early morning of November 15th;
- 5 in the early afternoon of November 15th;

The ground data used for validation are the Wideumont radar instantaneous measurements, without rain-gauge adjustment. Radar data are available within t5 minutes around the satellite passage.

Comparison

Two representative examples of the comparison between H02 and upscaled radar are given.

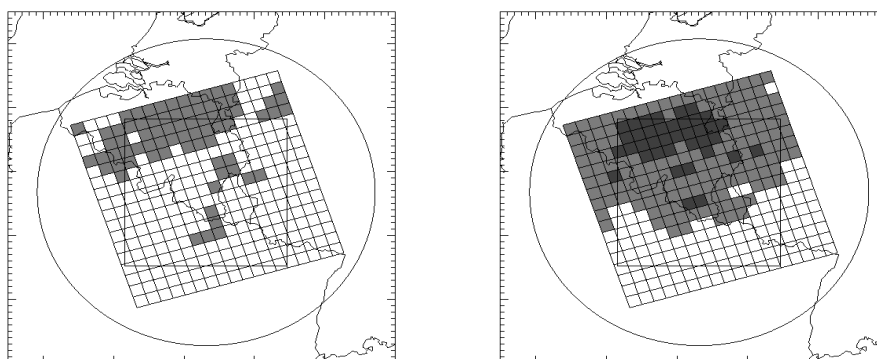


Figure 54 H02 image of November 13th, 2010 at 12.53 (left) compared with upscaled radar at 12.55 (right). The scale corresponds to thresholds of 0.1, 1., and 10. mm h-1

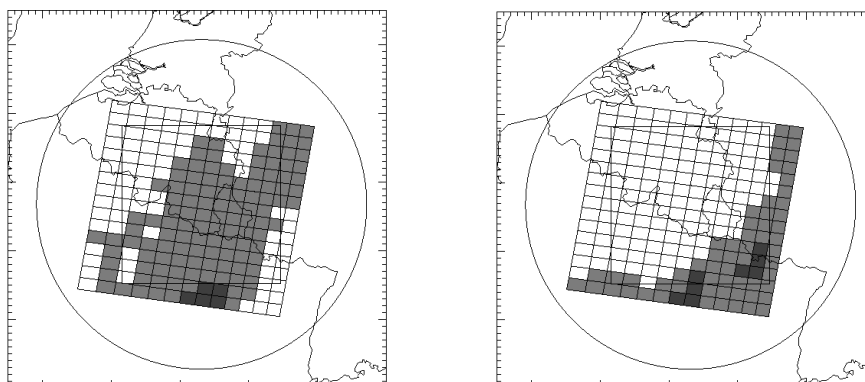


Figure 55 H02 image of November 15th, 2010 at 1.29 (left) compared with upscaled radar at 1.30 (right). The scale corresponds to thresholds of 0.1, 1., and 10. mm h-1

The matching of the precipitation area is very weak, and only in one case a cell with rain rate greater than 1 mm h⁻¹ is detected.

Scores evaluation

The statistical scores of the comparison between H02 and upscaled radar data are given on the following table.

Sample	58
Mean error*	-0.60
Standard deviation*	0.49
Mean absolute error*	0.64
Multiplicative bias	0.20
Correlation coefficient	0.13
Root mean square error*	0.80
URD-RMSE	0.88
POD	0.19
FAR	0.37
CSI	0.17

Table 23 Scores obtained with the comparison with radar data (* in mm h⁻¹)

These results, unlike the summer case, show performances lower than the ones of the long-period analysis, with low probability of detection, high false alarm ratio and large underestimation. It can be added that the radar data cumulated over 24h revealed to be underestimated compared with interpolated rain-gauge data. This of course only worsens the conclusion about the product.

The time evolution of the fraction area with rain, the average rain rate over this area, the Equitable Threat Score (ETS), and the root mean square error (RMSE) is reported in next figure.

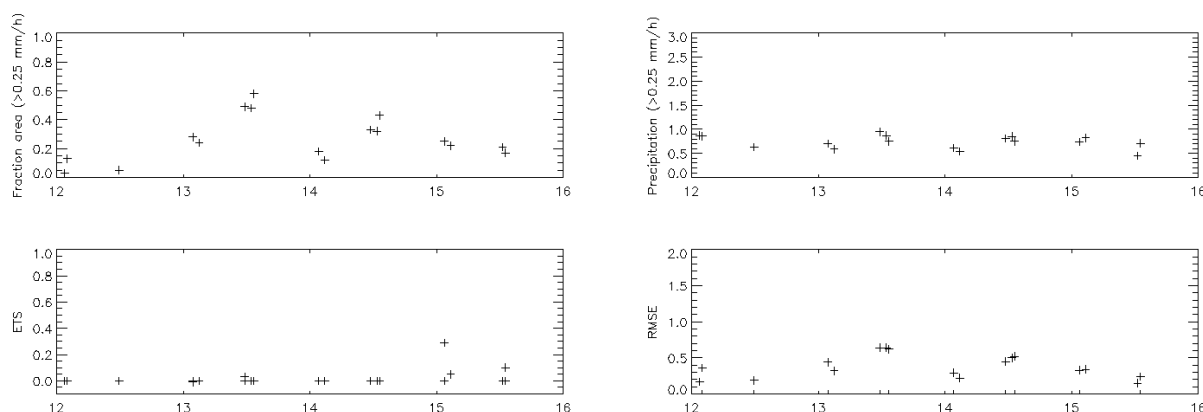


Figure 56 Time evolution of fraction area with rain, average rain rate over this area (threshold 0.25 mm/h), RMSE and ETS during the present case study

Conclusions

From the visual and statistical comparison with radar data, it appears that the H02 product fails to reproduce the rainfall patterns and amount in this winter situation.

5.3 Case study analysis in Germany (BfG)

5.3.1 Case study: August 7th, 2010 (River Neiße, Oder, Spree and Elbe catchments)

Description

At 7th August 2010 there was a baroclinic zone reaching from the Baltic sea across Poland and Czechia until Austria, where sub-tropical air was advected from south to north at the eastern flank of the associated low pressure. During the 7/8th August 2010 the precipitation reached about 35 mmh^{-1} (150 mm in 48 hours) in parts of Germany, especially in Saxony, causing floods in the upper parts of the rivers Neiße, Spree and Elbe with catastrophic damages.⁵

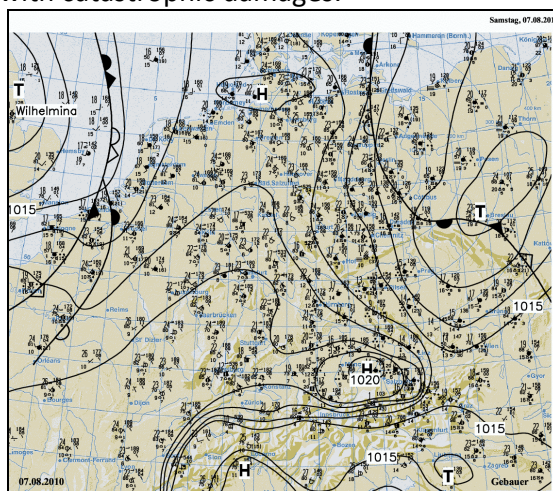


Figure 57 Synopsis for Central Europe for 07th August 2010 (FU Berlin, <http://wkserv.met.fu-berlin.de>)

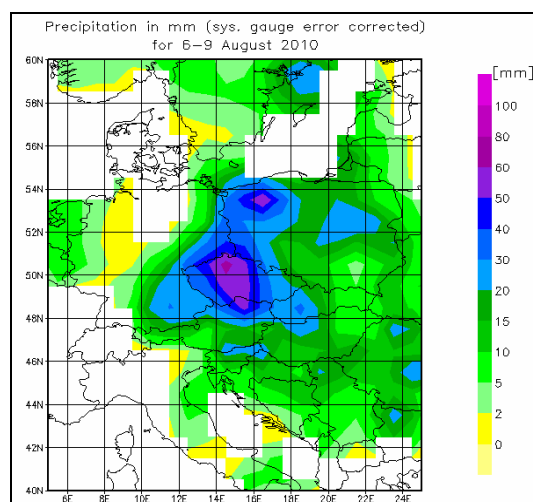


Figure 58 two-day totals (ending at 9th August, 0 UTC) interpolated on a $1^\circ \times 1^\circ$ evaluation grid as derived from SYNOP messages (Global Precipitation Climatology Centre, GPCC operated by DWD)

⁵ Zur Rolle des Starkniederschlages am 7.-9. August 2010 im Dreiländereck Polen, Tschechien, Deutschland bei der Entstehung der Hochwasser von Neiße, Spree und Elbe, Bissolli et al, Rapp, Friedrich, Ziese, Weigl, Nitsche, Gabriele Malitz, Andreas Becker (Floods in Eastern Central Europe in May 2010, FU Berlin 2010).

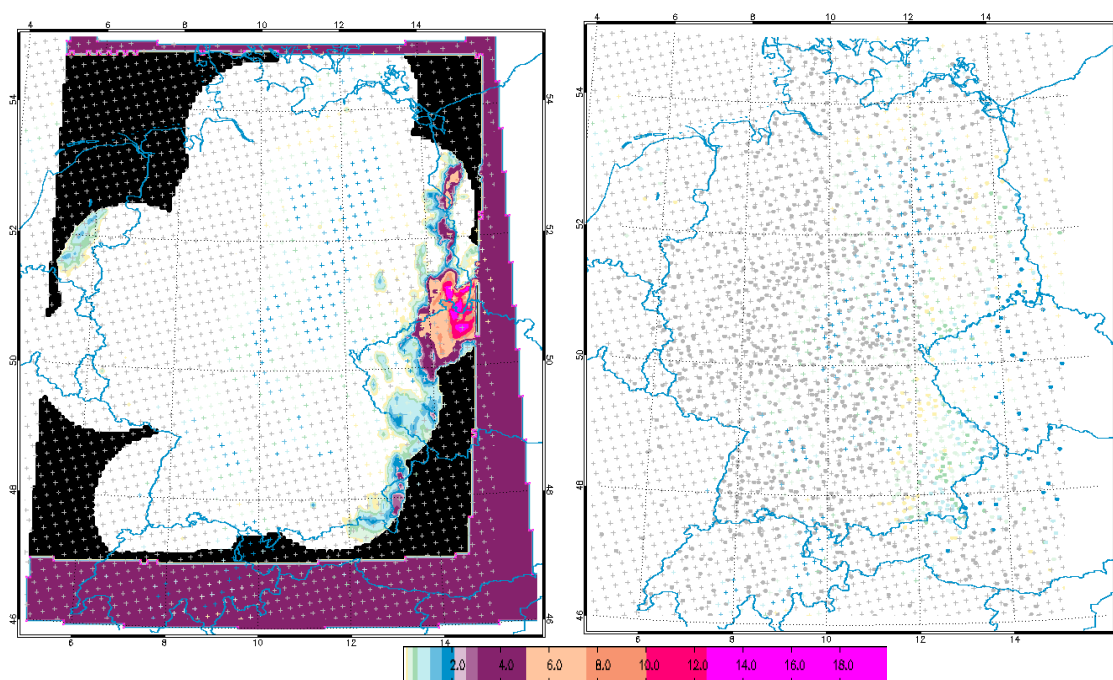


Figure 59 Hourly precipitation sum [mm] for H02 satellite data (crosses, time stamp 2010-08-07 11:58 UTC, station Rome) and for RADOLAN-RW (left, filled raster, 2010-08-07 12:50 UTC) and station data (right, dots, 2010-08-07 13:00 UTC)

Data used

H02 data for eastern part of Germany in the given period were available for 2:01 UTC (station Athens), 2:02 UTC (station Lannion), 11:51 UTC (station Athens), 11:52 UTC (station Lannion) and 11:58 UTC (station Rome). Only these data are analysed in this case study.

Comparison

A first look to the results (Figure 59) shows, that rain rates detected by satellite product are in the same area of Germany as those indicated by the ground data.

Statistical score

In the following two tables the result of the categorical statistic of the validation with both RADOLAN and rain gauge data are listed. The Probability Of Detection (POD) of precipitation $\geq 0.25 \text{ mmh}^{-1}$ gain for validation with RADOLAN 0.66, with rain gauge 0.54. The different results are due to the fact that RADOLAN data produce more valid pairs of satellite/ground points. A valid pair is given if for a satellite observation point (fixed date/time) at least one ground observation point can be found within an surrounding area formed by a search ellipse of $\sim 2.5 \text{ km} \times \sim 2.5 \text{ km}$. Also the False Alarm Rate (FAR) is different: for RADOLAN it was 0.49, for rain gauge 0.44 (worse than for whole August 2010). For both kinds of ground data there were no valid pairs in the class $\text{RR} \geq 10 \text{ mmh}^{-1}$, so that for this class we have no statement on validation.

7 th August 2010	H02 vs. radar			H02 vs. rain gauge		
[mm/h]	RR>=0.25	RR>=1.0	RR>=10	RR>=0.25	RR>=1.0	RR>=10
Samples	1133	405	1	288	104	0
POD	0.66	0.37	0.00	0.54	0.35	0.00
FAR	0.49	0.51	1.00	0.44	0.50	#DIV/0!
CSI	0.41	0.27	0.00	0.38	0.26	0.00

Table 24 Results of the categorical statistic of the validation for 7th August 2010

August 2010	H02 vs. radar			H02 vs. rain gauge		
[mm/h]	RR>=0.25	RR>=1.0	RR>=10	RR>=0.25	RR>=1.0	RR>=10
Samples	15896	7672	97	3173	1019	4
POD	0.68	0.65	0.09	0.38	0.27	0.03
FAR	0.47	0.63	0.98	0.35	0.51	0.75
CSI	0.43	0.31	0.02	0.32	0.21	0.03

Table 25 Results of the categorical statistic of the validation for whole August 2010

In comparison with categorical statistic of the whole August 2010 we can see, that in case of the 7th August we got worse results for POD in all classes for validation with radar data, for validation with gauge data it is the converse. Better results generally were received by validation with radar data. For 7th August the validation with both kind of ground data provide a POD in the second class (0.37 radar, 0.35 rain gauge) less than the FAR (0.51 radar, 0.5 rain gauge). The Critical Success Index (CSI) is more stable and differs only by 1-3 percent between the different validation methods. A CSI of 0.41 (0.38) means that 41% resp. 38 % of the predictions (H02) of precipitation ($\geq 0.25 \text{ mmh}^{-1}$) of all predicted/observed rain events are correct.

Next two figures. show the contingency table of four classes. In opposite to results of H01 on validation only for the first class over 50% of the H02 data are in the same class. In higher classes most of H02 data belong to lower classes. That means we have a strong underestimation of all precipitation amounts higher than 1 mmh^{-1} .

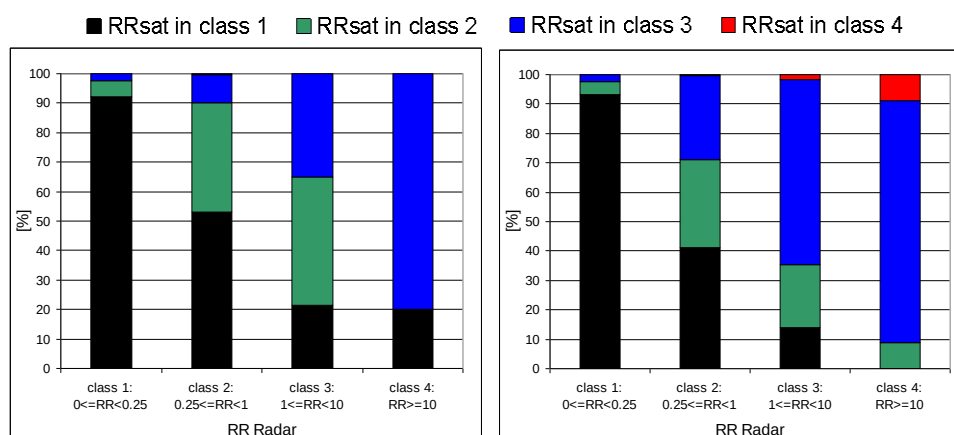


Figure 60 Contingency table statistic of rain rate [mmh^{-1}] for H02 vs. radar data. Left: for 7th August 2010, Right: for whole August 2010

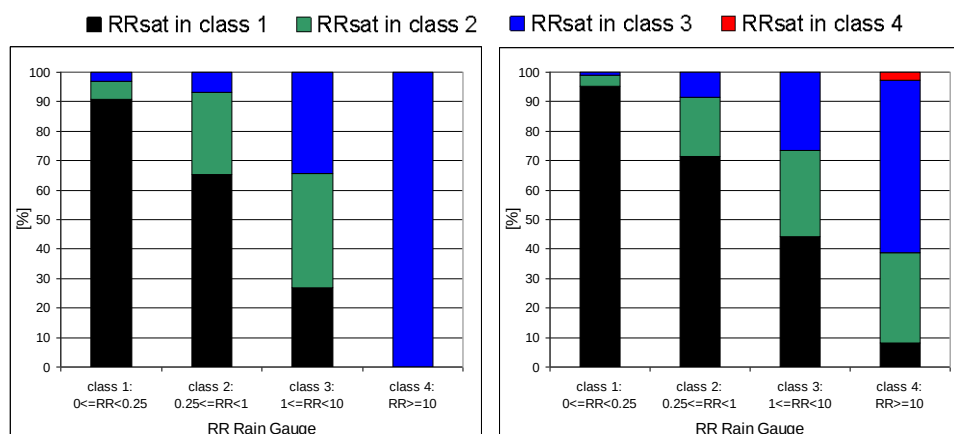


Figure 61 Contingency table statistic of rain Rate [mmh^{-1}] for H02 vs. rain gauge data. Left: for 7th August 2010, Right: for whole August 2010

Results of the continuous statistic (next table) show negative mean error (ME) for detection of precipitation ($\text{RR} \geq 0.25 \text{ mmh}^{-1}$), which means, that H-SAF product underestimates the fact of precipitation generally. Standard deviation (SD) with 0.5 mmh^{-1} for this class is less than for validation of H01. The correlation coefficient (CC) with 0.61/0.49 is better than that for H01 (0.24/0.46). These facts are due to less samples for H02. Results for whole August are not so clearly better: ME -0.64/0.19 for H02 against -0.25/-0.59 for H01, CC 0.35/0.38 for H02 against 0.32/0.38 for H01.

RR[mmh^{-1}]	7 th August 2010		August 2010		7 th August 2010		August 2010	
	rain gauge	radar	rain gauge	radar	rain gauge	radar	rain gauge	radar
	0.25 <= RR < 1				RR >= 0.25			
ME	-0.29	-0.18	-0.21	0.41	-0.84	-1.55	-0.64	0.19
SD	0.50	0.81	0.76	1.32	1.44	2.31	1.53	1.90
MAE	0.47	0.50	0.54	0.75	1.06	1.74	0.97	1.12
MB	0.46	0.69	0.59	1.86	0.44	0.36	0.44	1.16

CC	0.01	0.02	0.09	0.22	0.61	0.49	0.35	0.38
RMSE	0.58	0.83	0.79	1.38	1.66	2.78	1.66	1.91
	1 <= RR < 10				RR >= 10			
ME	-1.26	-2.07	-1.28	-0.19	-11.22	-9.75	-11.69	-8.08
SD	1.41	1.92	1.58	2.53	0.00	1.96	2.81	5.17
MAE	1.52	2.18	1.61	1.75	11.22	9.75	11.69	8.88
MB	0.45	0.35	0.40	0.92	0.24	0.20	0.17	0.40
CC	0.52	0.42	0.28	0.22	-	-0.04	0.58	0.14
RMSE	1.89	2.83	2.03	2.53	11.22	9.94	12.02	9.59

Table 26 Continuous statistic

Conclusions

The results for H02 were worse than for H01. For rain rates greater than 1 mmh⁻¹ the probability of detection is equal/less than the false alarm rate. All the quantitative precipitation amounts were underestimated.

5.3.2 Case study: June 3rd , 2010 (River Danube catchment)

Description

On the beginning of June 2010 the weather was determined by a low pressure area over eastern part of Central Europe. Wet hot air out from Mediterranean Sea was directed around the low-pressure vortex “Bergthora” contraclockwise out from north to Bavaria and arrived overhead the near-ground cold area. By this air advection on 3rd of June fell long lasting rain in the catchments of the rivers Regen and Danube and caused a Danube river flood. Precipitation amounts over 24 hours reached between 80 mm and 155 mm and⁶.

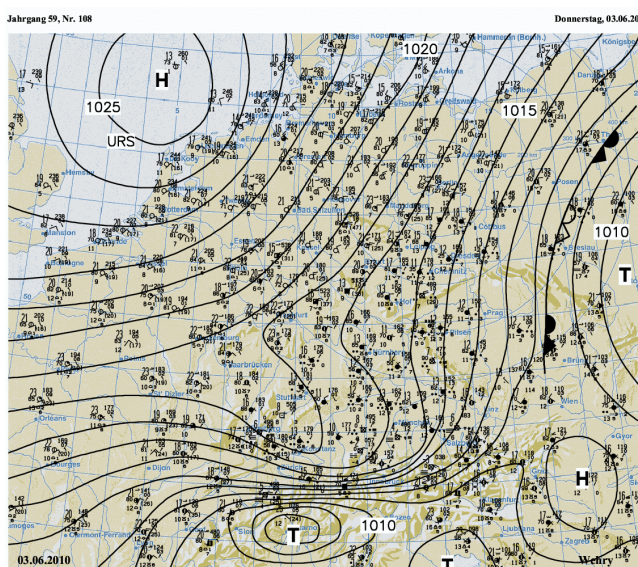


Figure 62 Synopsis for Central Europe for 03rd June 2010 (FU Berlin, <http://wkserv.met.fu-berlin.de>)

⁶ Gewässerkundlicher Monatsbericht Juni 2010, Bayerisches Landesamt für Umwelt

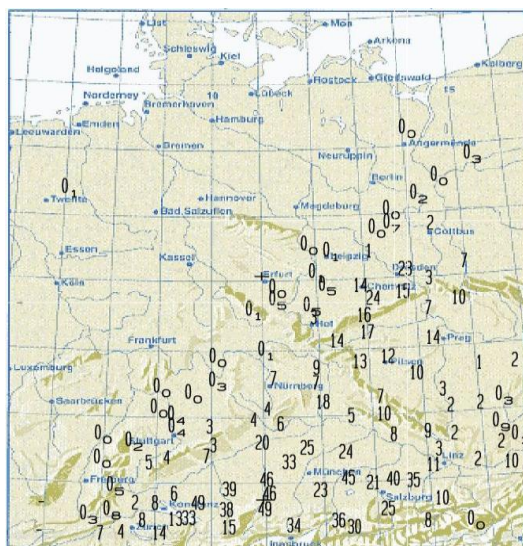


Figure 63 12h totals of precipitation(ending (FU at 3rd June 2010, 7 UTC)

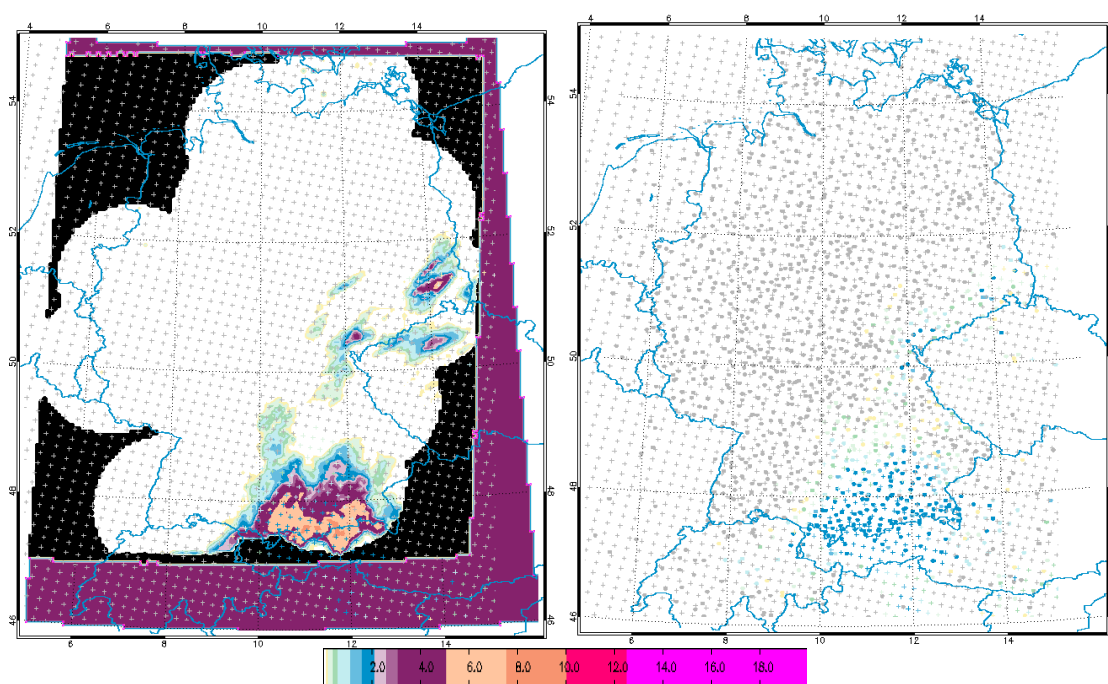


Figure 64 Hourly precipitation sum [mm] for H02 satellite data (crosses, time stamp 2010-06-03 01:50 UTC, station Athens) and for RADOLAN-RW (left, filled raster, 2010-06-03 01:50 UTC) and station data (right, dots 2010-06-03 02:00 UTC)

Data used

H02 data for Bavaria in the given period were available for 1:30 UTC (Rome), 1:49 UTC (Mos), 1:50 UTC (Athens), 11:42 UTC (Rome), 13:18 UTC (Rome) and 13:22 UTC (Lannion). Only these data are analysed for this case study.

Comparison

A first look to the results shows, that rain rates detected by satellite product are in the same area of Germany as those indicated by the ground data.

Statistical score

In the next two tables the result of the categorical statistic of the validation with both RADOLAN and rain gauge data are listed. The results for validation with radar data for 3rd June are worse than for the whole month June: Probability Of Detection of precipitation ($RR \geq 0.25 \text{ mmh}^{-1}$) was 0.30 with less False Alarm Rate of 0.13 and Critical Success Index is 0.29. Compared with results of H01 validation the results are much worse for 3rd June. Results for H02, 3rd June were better than for the whole June. The matter may be the fact, that the rain events were particularly in small point areas, which were not scanned by satellite.

3 rd June 2010	H02 vs. radar			H02 vs. rain gauge		
[mmh ⁻¹]	$RR \geq 0.25$	$RR \geq 1.0$	$RR \geq 10$	$RR \geq 0.25$	$RR \geq 1.0$	$RR \geq 10$
Samples	206	96	0	88	39	3
POD	0.30	0.29	-	0.28	0.24	-
FAR	0.13	0.10	-	0.14	0.18	1.00
CSI	0.29	0.28	-	0.26	0.23	0.00

Table 27 Results of the categorical statistic of the validation for 3rd June 2010

June 2010	H02 vs. radar			H02 vs. rain gauge		
[mmh ⁻¹]	$RR \geq 0.25$	$RR \geq 1.0$	$RR \geq 10$	$RR \geq 0.25$	$RR \geq 1.0$	$RR \geq 10$
Samples	6958	2919	29	1736	594	26
POD	0.60	0.61	0.22	0.39	0.31	0.29
FAR	0.45	0.56	0.62	0.43	0.54	0.85
CSI	0.40	0.34	0.16	0.30	0.23	0.11

Table 28 Results of the categorical statistic of the validation for whole June 2010

The contingency tables (next two figures) for both kinds of validation data show that only in the lowest class (except for validation with radar data for whole June) more than 50% of H02 data fall in the same class. The results are worse than for H01.

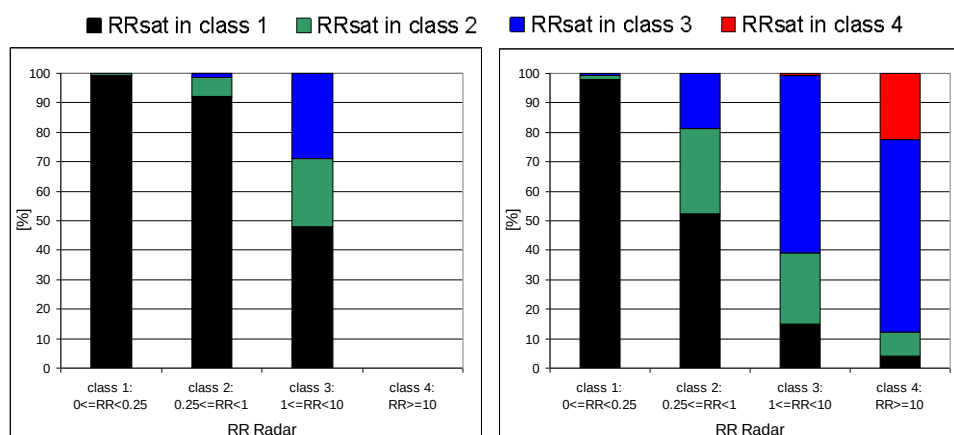


Figure 65 Contingency table statistic of Rain Rate [mm h^{-1}] for H02 vs. radar data Left: for 3rd June 2010, Right: for whole June 2010

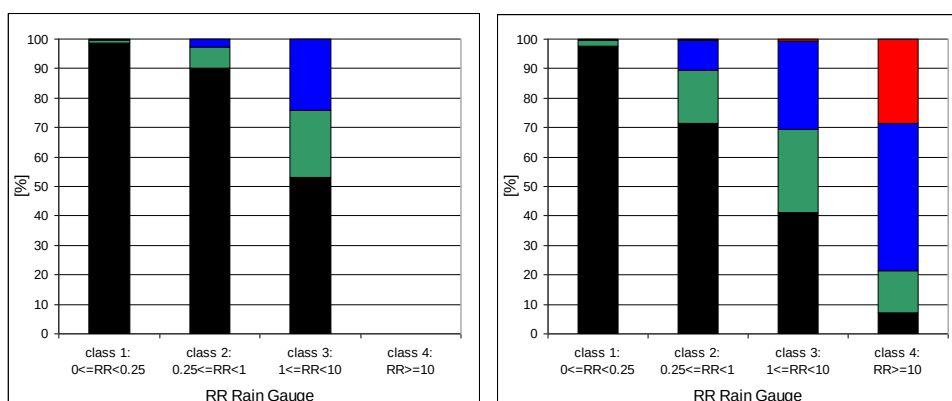


Figure 66 Contingency table statistic of rain rate [mm h^{-1}] for H02 vs. rain gauge data. Left: for 3rd June 2010; Right: for whole June 2010

Results of the continuous statistic (next table) show negative Mean Error (ME) in both periods with both kind of ground data in the first class, which means, that H-SAF product underestimates all kind of precipitation amounts. For SD of 0.48 for radar data is the best, analogue to the results for POD (see above). For detection of precipitation $\text{RR} \geq 0.25 \text{ mmh}^{-1}$ there are nearly the same results for both kind of ground data and for both periods, which means the chosen period is representative for June 2010. Standard deviation (SD) with 1.51 mmh^{-1} for this class is the highest for validation with RADOLAN for 3rd June, nevertheless the correlation coefficient (CC) with 0.62 is the best, analogue to the results for POD (see above).

The better results for CC and RMSE in comparison with that for H01 validation are due to smaller number of samples.

RR[mmh^{-1}]	3 rd June 2010		June 2010		3 rd June 2010		June 2010	
	rain gauge	radar	rain gauge	radar	rain gauge	radar	rain gauge	radar
	0.25 <= RR < 1				RR >= 0.25			
ME	-0.45	-0.45	-0.15	0.13	-1.26	-1.38	-0.55	-0.11
SD	0.54	0.48	1.05	0.96	1.36	1.51	1.84	1.66
MAE	0.57	0.53	0.58	0.55	1.38	1.46	1.02	0.94
MB	0.19	0.15	0.71	1.28	0.27	0.28	0.52	0.91
CC	0.11	-0.11	0.14	0.29	0.61	0.62	0.32	0.50
RMSE	0.70	0.65	1.06	0.97	1.85	2.05	1.92	1.66
	1 <= RR < 10				RR >= 10			
ME	-2.13	-2.33	-1.19	-0.47	-	-	-10.20	-6.43
SD	1.44	1.60	1.96	2.24	-	-	10.48	4.53
MAE	2.26	2.41	1.71	1.63	-	-	11.66	7.11
MB	0.29	0.30	0.46	0.81	-	-	0.35	0.49
CC	0.59	0.56	0.22	0.25	-	-	-0.21	0.34
RMSE	2.57	2.83	2.30	2.29	-	-	14.62	7.87

Table 29 Continuous statistic

Conclusions

The results for H02 were worse than for H01. Compared with the case study for August the results were worse. All the quantitative precipitation amounts were underestimated.

5.3.3 Case study: December 5th /6th, 2010 (River Rhine catchment)

Description

Intense rains on 5th / 6th December 2010 lasting over 72 hours fell along an air mass boundary, lying across France and Germany. It was a result of subtropical air from south west and polar cold air over Central Europe, moving forward to south. First precipitation as snow and rain were observed on 5th in relation to the cyclone “Liane” in northern parts of Germany. On the evening the precipitation deflected to the south of Germany. In higher regions of the river Rhine they fell as snow. In the night to 6th December in south of river Danube the snow changed to rain.⁷

Over a period of 4 days precipitation sum reached 100 mm. See next figures.

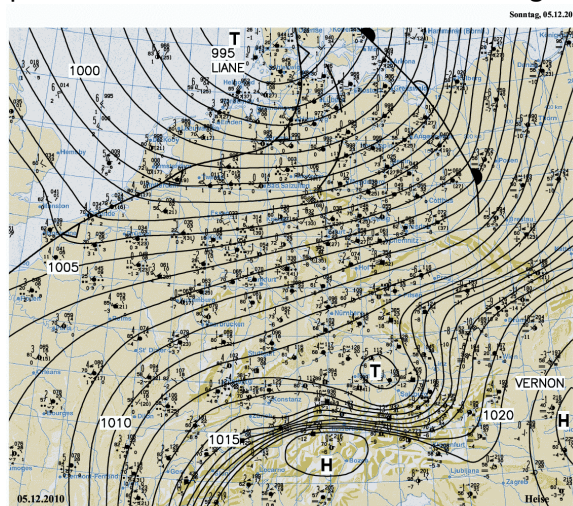
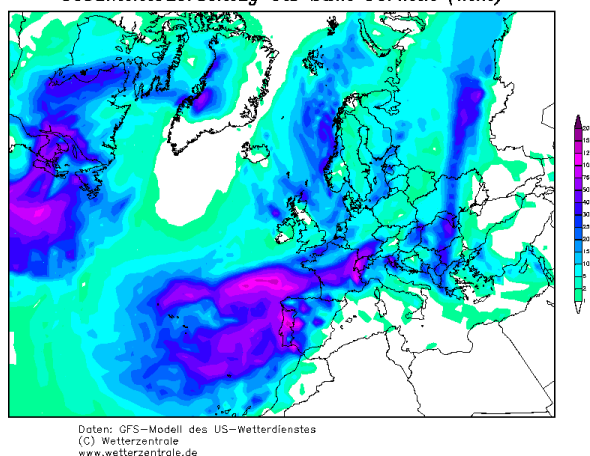


Figure 67 Synopsis for Central Europe for 05th December 2010 (FU Berlin, <http://wkserv.met.fu-berlin.de>)

Init : Sat,04DEC2010 06Z Valid: Wed,08DEC2010 00Z
Gesamtniederschlag bis zum Termin (mm)



Daten: GFS-Modell des US-Wetterdienstes
(C) Wetterzentrale
www.wetterzentrale.de

Figure 68 96h totals of precipitation

⁷ Der Wetterservice für NRW und Deutschland, Rückblick Starkniederschläge - Hochwasser - West-, Mitteleuropa 05.12. - 09.12.2010

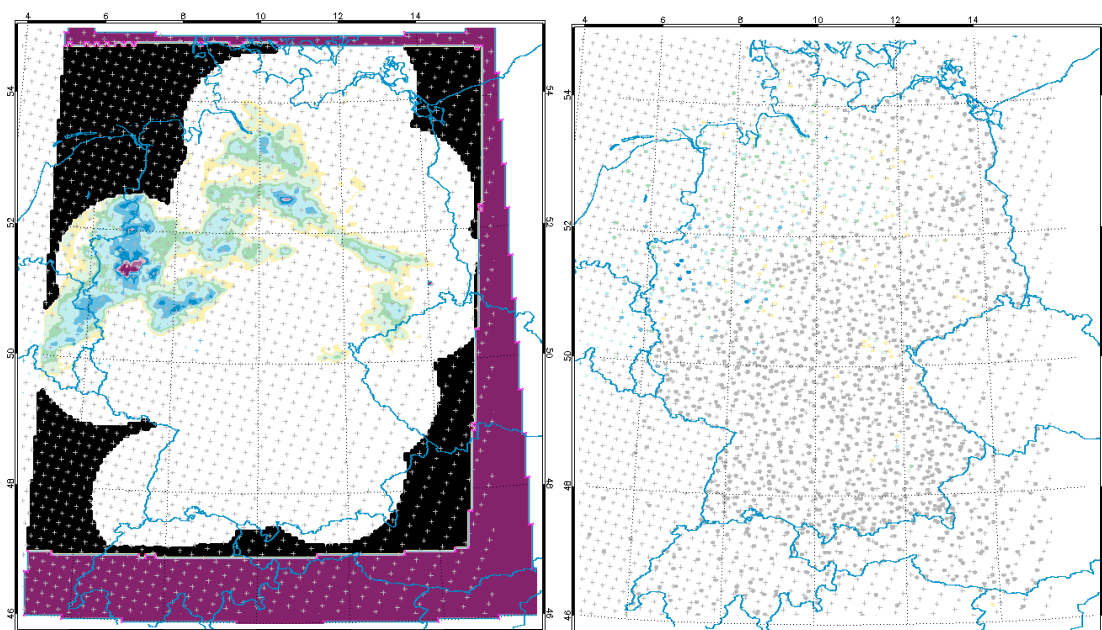


Figure 69 Hourly precipitation sum [mm] for H02 satellite data (crosses, time stamp 2010-12-05 02:29 UTC) and for RADOLAN-RW (left, filled raster, 2010-12-05 02:50 UTC) and station data (right, dots 2010-12-05 03:00 UTC)

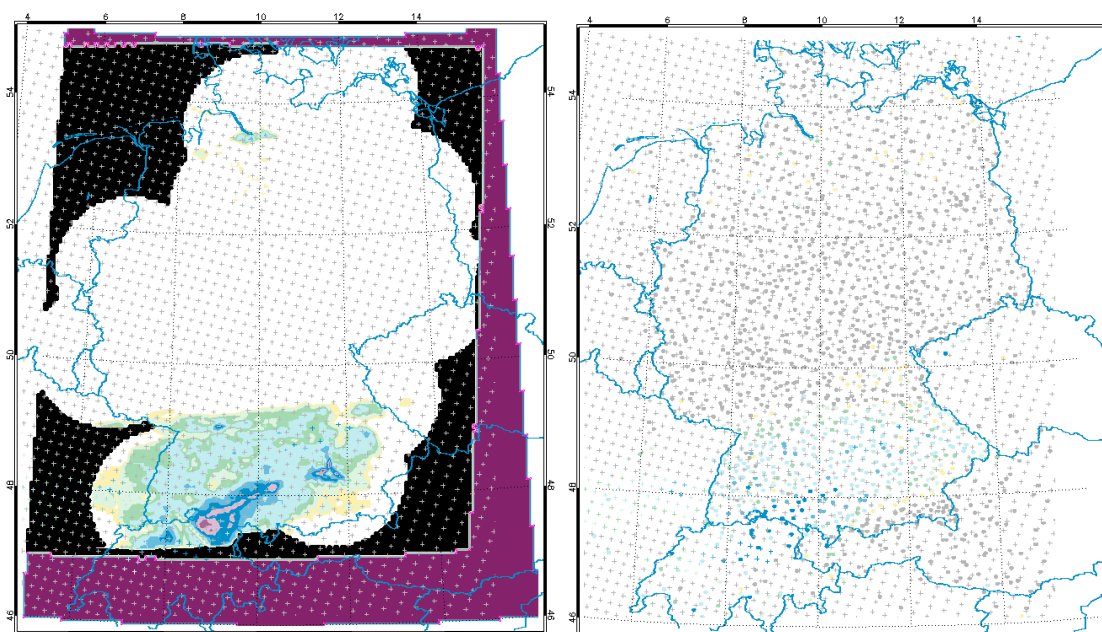


Figure 70 Hourly precipitation sum [mm] for H02 satellite data (crosses, time stamp 2010-12-06 02:18 UTC) and for RADOLAN-RW (left, filled raster, 2010-12-06 02:50 UTC) and station data (right, dots 2010-12-06 03:00 UTC)

Data used

H02 data for Bavaria in the given period were available for 5th December, 1:23, 2:29, 11:51, 12:20 and 12:56 UTC and for 6th December, 2:18, 12:09 and 13:50 UTC. Only these data are analysed in this case study.

Comparison

A first look to the results (previous figures) shows, that rain rates detected by satellite product are in the same two areas of Germany as those indicated by the ground data.

Statistical score

In the next two tables the results of the categorical statistic of the validation with both radar and rain gauge data are listed. The results for validation with radar data for 5/6th December are worse than for the whole month December: Probability Of Detection of precipitation ($RR \geq 0.25 \text{ mmh}^{-1}$) was 0.16 with higher False Alarm Rate of 0.71 and Critical Success Index is 0.11, more worse than summer results.

5/6 December 2010	H02 vs. radar			H02 vs. rain gauge		
[mmh ⁻¹]	$RR \geq 0.25$	$RR \geq 1.0$	$RR \geq 10$	$RR \geq 0.25$	$RR \geq 1.0$	$RR \geq 10$
Samples	792	504	0	168	108	0
POD	0.16	0.07	-	0.11	0.04	-
FAR	0.71	0.96	-	0.79	0.96	-
CSI	0.11	0.03	-	0.08	0.02	-

Table 30 Results of the categorical statistic of the validation for 5/6th December 2010

December 2010	H02 vs. radar			H02 vs. rain gauge		
[mmh ⁻¹]	$RR \geq 0.25$	$RR \geq 1.0$	$RR \geq 10$	$RR \geq 0.25$	$RR \geq 1.0$	$RR \geq 10$
Samples	13082	3125	4	610	311	1
POD	0.49	0.23	-	0.08	0.09	0.00
FAR	0.88	0.86	1.00	0.46	0.71	1.00
CSI	0.11	0.09	0.00	0.08	0.07	0.00

Table 31 Results of the categorical statistic of the validation for whole December 2010

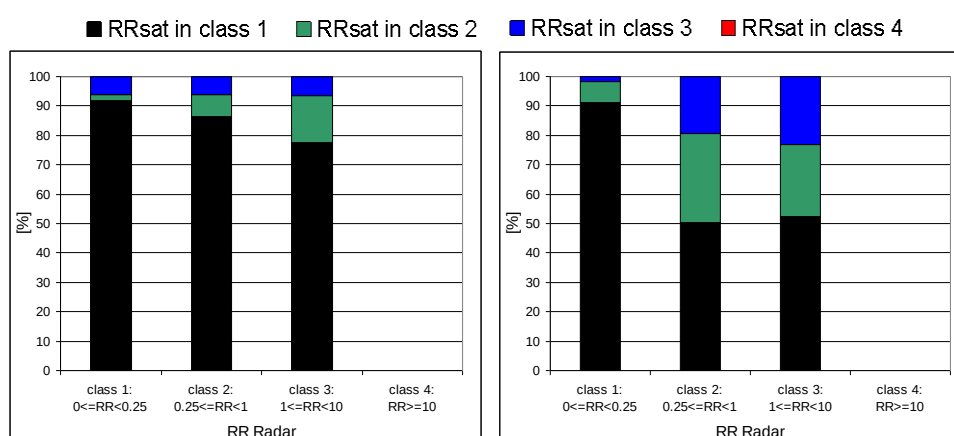


Figure 71 Contingency table statistic of Rain Rate [mm h^{-1}] for H02 vs. radar data. Left: for 5/6th December, Right: for whole December 2010

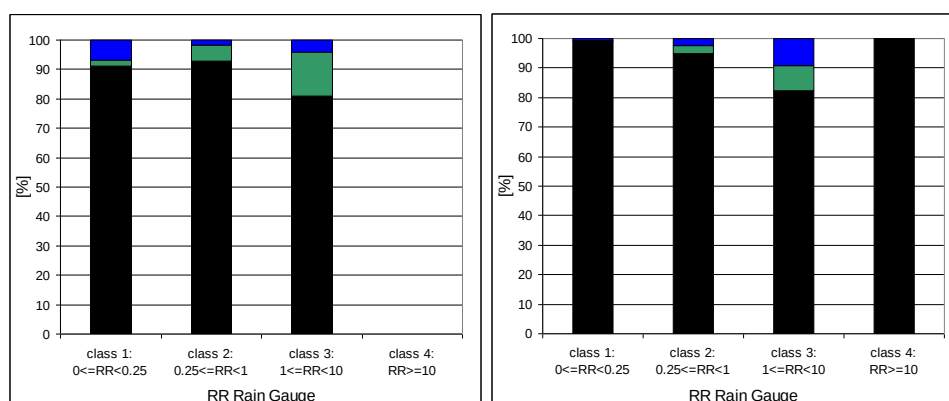


Figure 72 Contingency table statistic of rain rate [mm h^{-1}] for H02 vs. rain gauge data. Left: for 5/6th December; Right: for whole December 2010

Results of the continuous statistic (next table) show negative Mean Error (ME) in the period 5/6th December with both kind of ground data in all classes, which means, that H-SAF product underestimated precipitation amounts. Standard deviation (SD) with 0.64 mmh^{-1} for the class $\text{RR} \geq 0.25 \text{ mmh}^{-1}$ is the highest for validation with radar data for 5/6th December, the correlation coefficient (CC) with mostly less than 0.2 is more worse than for results in summer, analogue to the results for POD (see above).

RR[mmh^{-1}]	5/6 December 2010		December 2010		5/6 December 2010		December 2010	
	rain gauge	radar	rain gauge	radar	rain gauge	radar	rain gauge	radar
	0.25 ≤ RR < 1				RR ≥ 0.25			
ME	-0.49	-0.40	-0.46	-0.09	-0.70	-0.58	-0.70	-0.77
SD	0.28	0.49	0.33	0.67	0.49	0.64	0.89	1.12
MAE	0.53	0.56	0.52	0.53	0.73	0.71	0.77	1.07
MB	0.10	0.27	0.11	0.86	0.11	0.21	0.12	0.42
CC	0.19	-0.03	0.12	0.04	0.22	0.03	0.14	0.16
RMSE	0.57	0.63	0.57	0.67	0.85	0.86	1.14	1.36
	1 ≤ RR < 10				RR ≥ 10			
ME	-1.19	-1.26	-1.39	-1.33	-	-	-26.25	-
SD	0.54	0.68	0.97	1.10	-	-	1.55	-
MAE	1.21	1.30	1.47	1.50	-	-	26.25	-
MB	0.11	0.14	0.14	0.31	-	-	0.00	-
CC	0.16	0.03	0.08	0.19	-	-	-	-
RMSE	1.31	1.43	1.69	1.73	-	-	26.30	-

Table 32 Continuous statistic

Conclusions

The results for H02 were worse than for H01: the probability of detection was less, the false alarm rate nearly same (higher than POD). All the quantitative precipitation amounts were underestimated.

5.4 Case study analysis in Hungary (OMSZ)

5.4.1 Case study: July 18th, 2010

Description

At Iceland a cyclone multiple center derives the weather of Europe. Along the front lot of clouds with rain develop, thunderstorms are also observed.

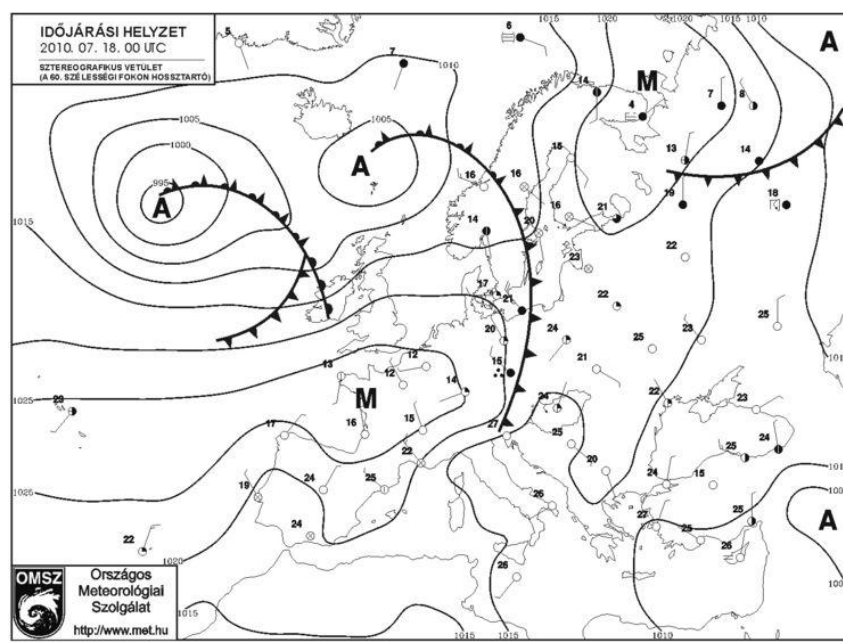
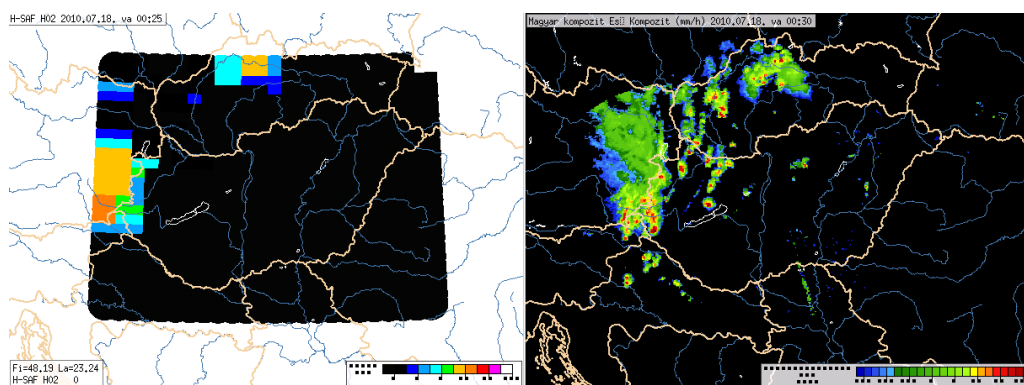


Figure 73 Synoptic chart at 00 UTC on 18 July 2010

Data used



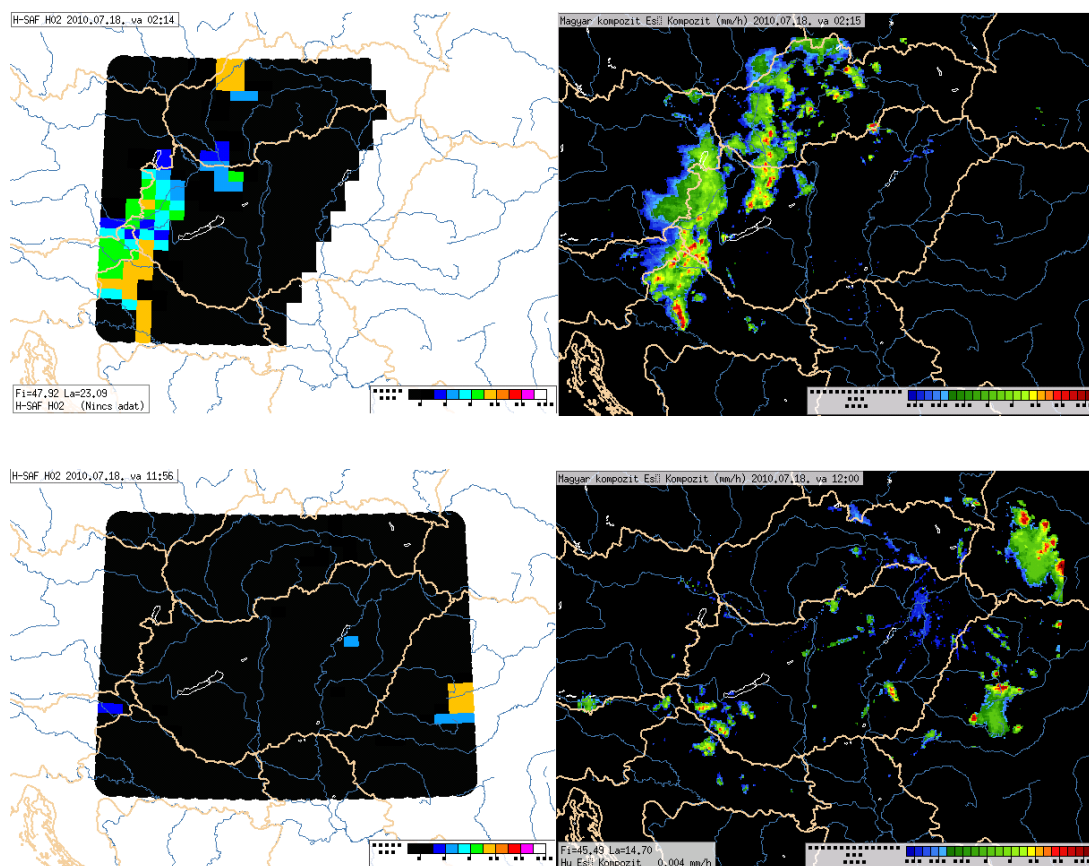


Figure 74 H02 product (left panel), Precipitation rate from the Hungarian radar network at its original resolution (right panel) at 00:30 UTC, at 2:15 UTC and at 12 UTC

Comparison

In this cold front weather situation during the whole day H02 did not detect the middle size thunderstorms.

Conclusions

The H02 in most cases well detects the precipitation area, but the middle size thunderstorms were not detected. Improvement of the H02 spatial resolution would help the detection.

5.4.2 Case study: September 2010

Description

A cyclone over Mediterranean causes precipitation in Central and South Europe. Lot of precipitation was measured mainly in the central part in Hungary.

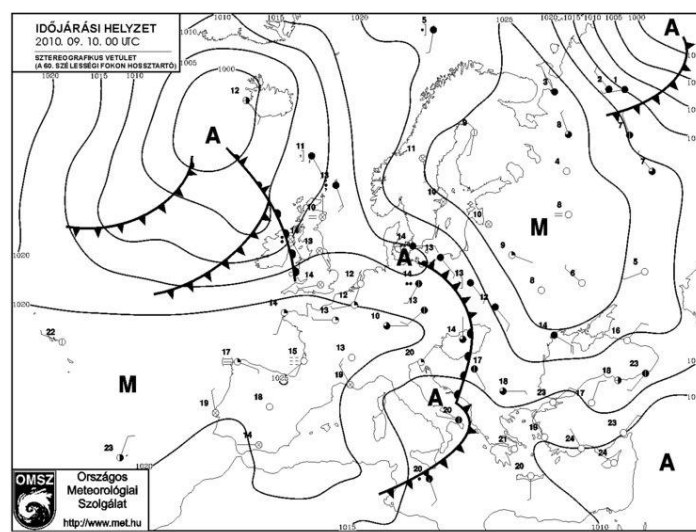


Figure 75 Synoptic chart at 00 UTC on 10 September 2010

Data used

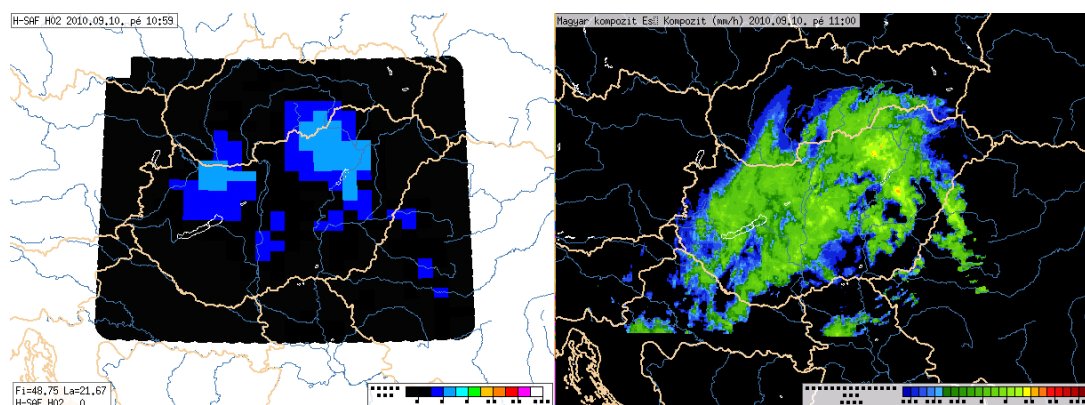


Figure 76 Precipitation rate from the Hungarian radar network at its original resolution at 11 UTC (right panel), H02 product at 11 UTC (left panel)

Comparison

H02 well detected the precipitation area over the country. H02 derives lower values than the radar measured.

Conclusions

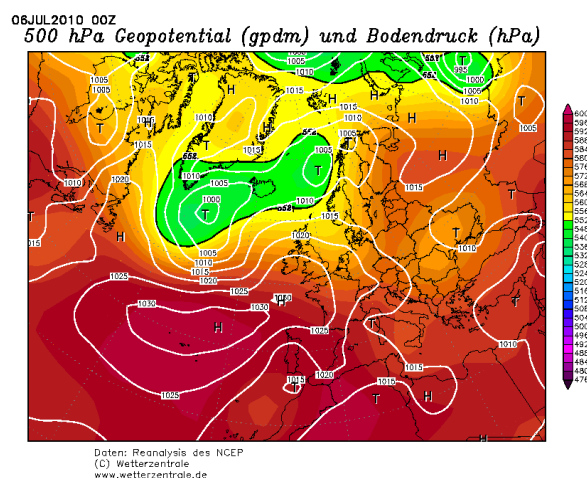
The H02 well detects the precipitation area, but it underestimates the precipitation values.

5.5 Case study analysis in Italy (Uni Fe)

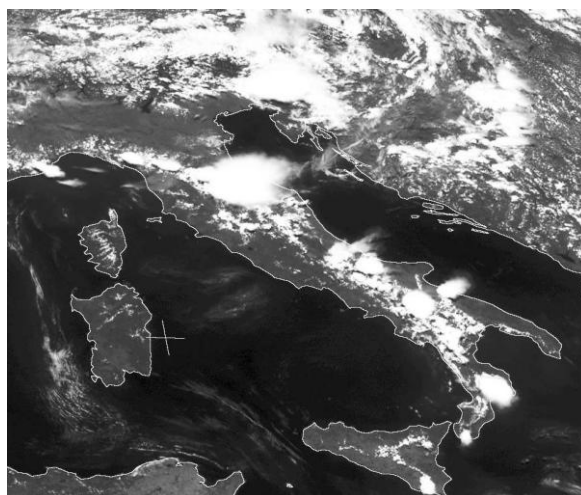
5.5.1 Case study: July 06th, 2010

Description

On July 06 the Azores anticyclone advected very warm and moist air on the Tyrrhenian coasts, where a weak trough induced cyclonic circulation and instability in the early morning. After 10:00 UTC deep convections initiated in the Po Valley and in central Italy, along the Apennines chain, causing waterspouts along the northern Adriatic coasts, hail falls and supercells storms in Central Italy.



SEVIRI HR-VIS image at 12:00 on July 06 shows a well developed convective cluster over central Italy, while small-scale, scattered convection is present along the Apennines chain. Some of these small systems are expected to grow in the following hours.



Data used

Reference data: Italian hourly raingauges network (provided by DPC)

Ancillary data (used for case analysis):

SEVIRI images (courtesy of University of Dundee – NEODAAS)

Weather charts (courtesy of Wetterzentrale, NCEP and METOFFICE).

Comparison

This deep convective case has been observed by two different AMSU sensors on board NOAA NP and NOAA NN with a time lag of only 10 minutes. In the figure below the two estimates are presented (top panel) with the hourly cumulated rain gauge map at 13:00 UTC (please note: zero rain rate gauges are not shown).

The rain rate patterns in the two estimates are rather similar, but some significant variations in the shape of rain areas and in the rain rate values can be due to the time lag between the images (10 minutes), and to a different viewing angle of the two sensors. The NOAA NP estimate shows higher precipitation rates (close to the end of the scale: 20 mm h^{-1}), while the rain gauge cumulated maximum value is 34 mm h^{-1} . The considered statistical parameters indicate a best matching for the NOAA-NN

estimate, with the following values: ETS=31 (27), FAR=43 (44), POD=49 (42), HSS=37 (29), where values within brackets refer to the NOAA-NP overpass. Overestimation occurs, for both estimates, around the large convective cells, while underestimation takes place mainly in case of very small structure, not detected by h02 because the rather large IFOV.

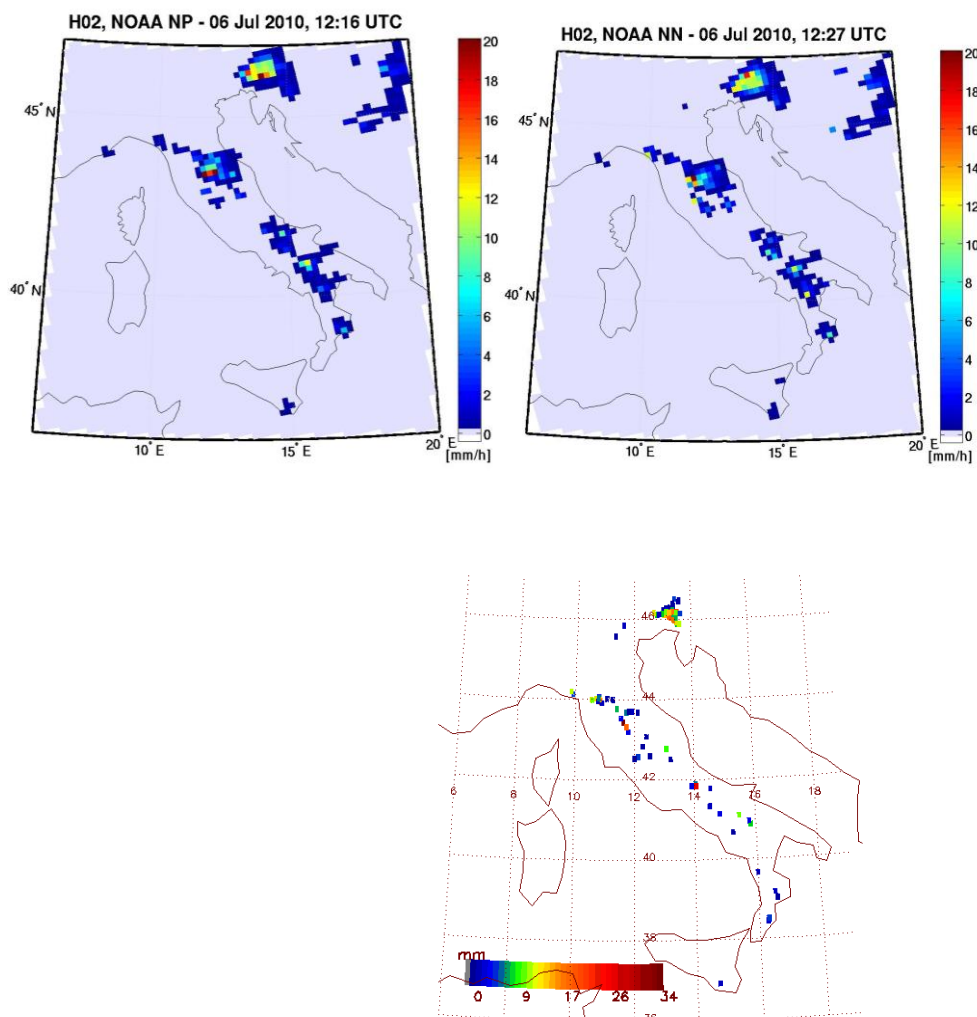


Figure 77 H02 precipitation map at 12:16 UTC (top-left), at 12:27 (top-right) and raingauges hourly precipitation cumulated at 13:00 UTC (bottom panel) of 06 July 2010

Please note different colour scales; zero rainrate gauges are not shown.

Conclusions

For this convective case the performances of h02 are satisfactory, pointing out that no parallax correction is applied and this could be particularly effective in case of small convective structures. This case is also useful to understand the inadequacy of hourly gauge measurements in validating instantaneous satellite snapshots, as in case of h02. As a matter of fact, the variability of the precipitation field, well described by the two overpasses shown above, cannot be caught by hourly integrals provided by the raingauges, especially in case of convective precipitation. The skill score

values reported above indicate rather different performances between the two satellite overpasses: HSS increases from 29 to 37 in 10 minutes.

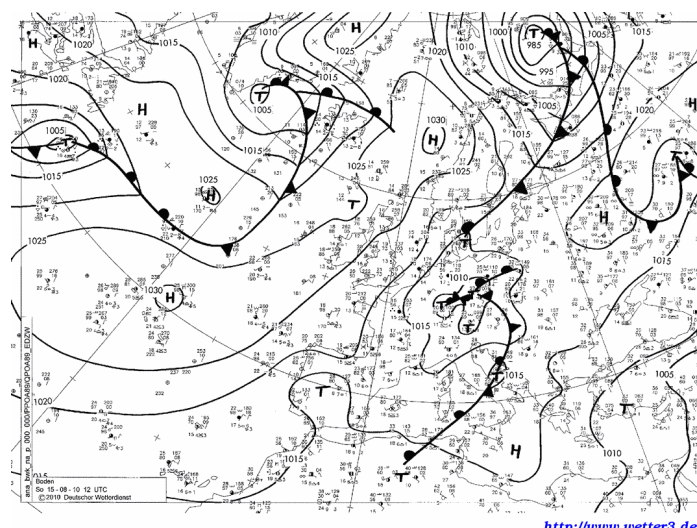
It seems the main problem of this technique for convective precipitation is related to the relatively large IFOV of the AMSU data, that prevent the correct retrieval of small (sub-IFOV) precipitation structures. It has also to be mentioned that this case study does not show differences between land and sea algorithms, as it was remarked in the 2009 case study.

5.6 Case study analysis in Poland (IMWM)

5.6.1 Case study: August 15th, 2010

Description

Significant cloud layer reaching over Lower Silesia region with its upper constituent belongs to developing low pressure centre. That structure is a part of bigger low pressure centre over France and tends to move over Germany to Poland. Stripe of clouds extending from Tunis, through central Italy, Adriatic Sea to Austria is a cold front of Atlantic air which is going to reach Poland on Monday 16th of August when bay of low pressure over Germany moves over Poland. Mentioned above bay of low pressure extends further over Balkans with significant wind convergence stimulating convection updrafts with large-scale moves. Moreover the forecast dated on 0000 UTC shows very turbulent night because of development of low pressure centre over Poland.



<http://www.wetter3.de>

Figure 78 Synoptic chart at 1200 UTC on 15th of August 2010

Convective storms were observed over the country on that day. The precipitation was accompanied by lightning activity. On the next figure, the lightning activity map for half an hour time span (1145 UTC - 1215 UTC) is presented. The map was constructed on the base of data from Polish Lightning Detection System, PERUN.

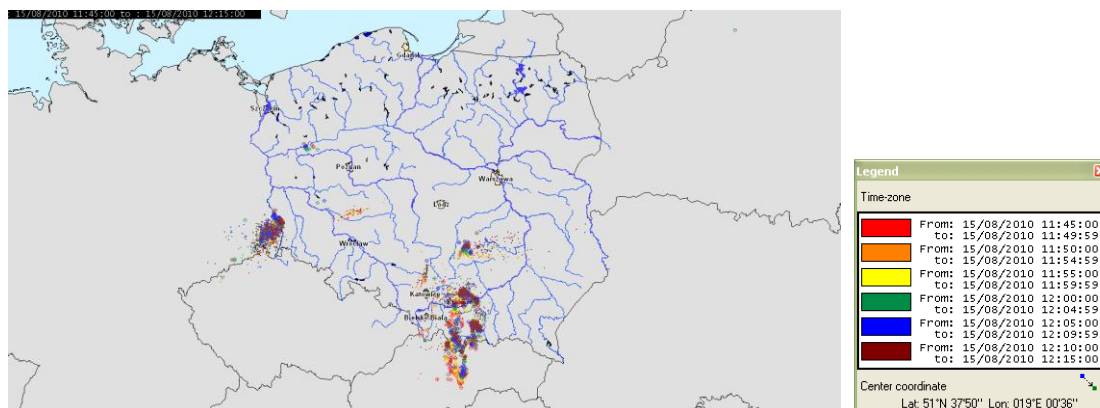


Figure 79 Total lighting map of Poland showing electrical activity between 1145 and 1215 UTC on 15th of August 2010

Comparison

On the Figure 80 the H02 product is visualized for the noon overpass. For comparison, the distribution of 10 minute precipitation obtained from RG data measured at closest to the given time slot is presented. The RG derived precipitation map was prepared using Near Neighbor method.

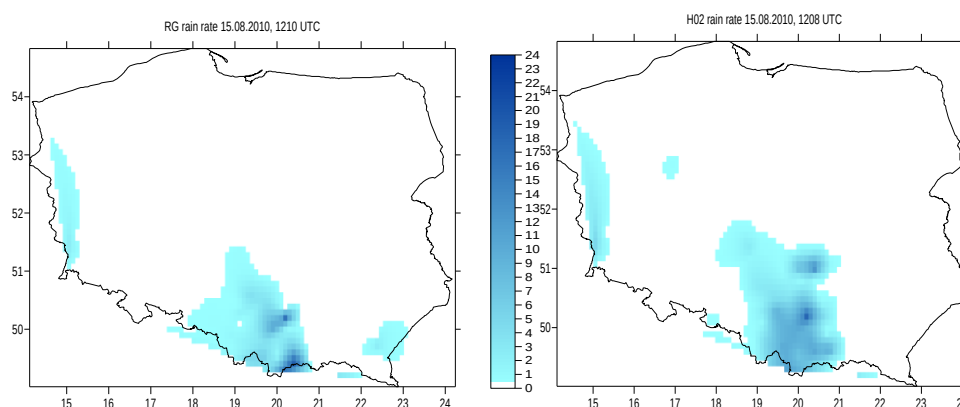


Figure 80 H02 at 1208 UTC on the 15th of August 2010 (right panel) and 10 minute precipitation interpolated from RG data from 1210 UTC (left panel)

On both maps, the precipitating areas reveal the lightning activity seen on the Figure 79, however, the H02 overestimated the precipitation area. This tendency is clearly seen in the Central Poland when H02 reports rainfall, while the ground data doesn't (Figure 80). On the other hand, this precipitating area seen on the satellite derived rainfall map in the Central Poland (Figure 80, right panel) corresponds to lightning activity observed in this region (Figure 79). Fact that this rainfall is not present on the RG map may be explained by the ground network density.

One maximum out of two was properly recognized by satellite product while instead of the second one, the fuzzy area of increased rainfall was obtained (Figure 80).

Statistical score

Further analysis was performed for all overpasses available for the 15th of August 2010. The ability of H02 product to recognize the precipitation was analyzed using dichotomous statistics parameters. The 0.25mm/h threshold was used to discriminate rain and no-rain cases. In the next table the values of Probability of Detection (POD), False Alarm Rate (FAR) and Critical Success Ratio (CSI) are presented.

Parameter	Scores
POD	0.83
FAR	0.52
CSI	0.44

Table 33 Results of the categorical statistics obtained for PR-OBS-1 on the base of all data available on the 15th August 2010

Higher value of POD than the value of FAR indicate that the product ability to recognize the convective precipitation is quite good.

The quality of H02 in estimating the convective precipitation is presented on the next figure. The points on the scatter plot are mostly arranged above and along the diagonal, what indicates that H02 tends to overestimate the precipitation except for the very heavy ones.

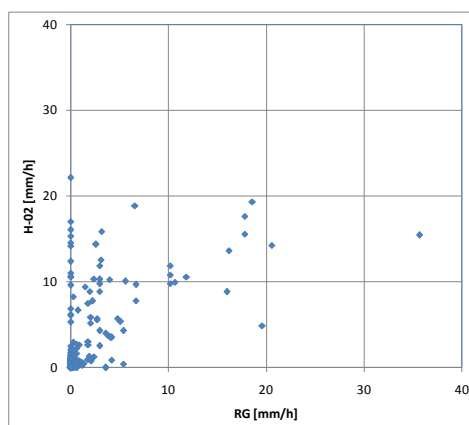


Figure 81 Scatter plot for measured (RG) and satellite derived (H-02) rain rate obtained for all H02 data on the 15th of August 2010

Finally, the analysis of rain classes was performed. The categories were selected in accordance with the common validation method. Next figure shows the percentage distribution of satellite derived precipitation categories within each precipitation class defined using ground measurements.

One can easily notice very good ability of H02 to recognize both, no-rain and heavy precipitation situations – respectively, more than 90% and 60% of ground cases was properly allocated by satellite product. The light precipitation is not properly recognized in most cases: it is either overestimated (26% of cases) or missed (36% of cases). When moderate is considered, the H02 quality is better: almost 60% of the observed precipitation in this class is properly recognized.

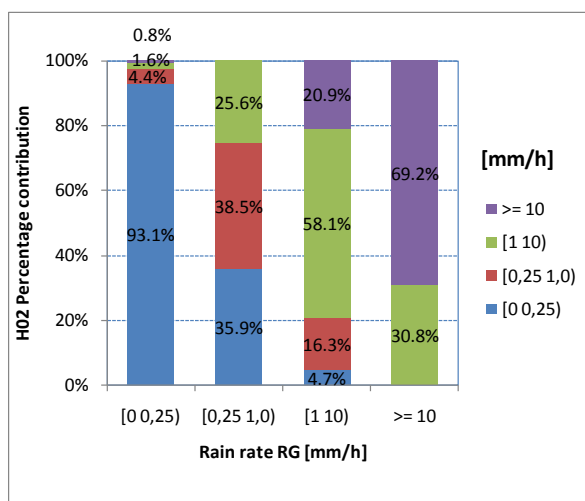


Figure 82 Percentage distribution of H02 precipitation classes in the rain classes defined using rain gauges (RG) data on the 15th of August 2010

Conclusions

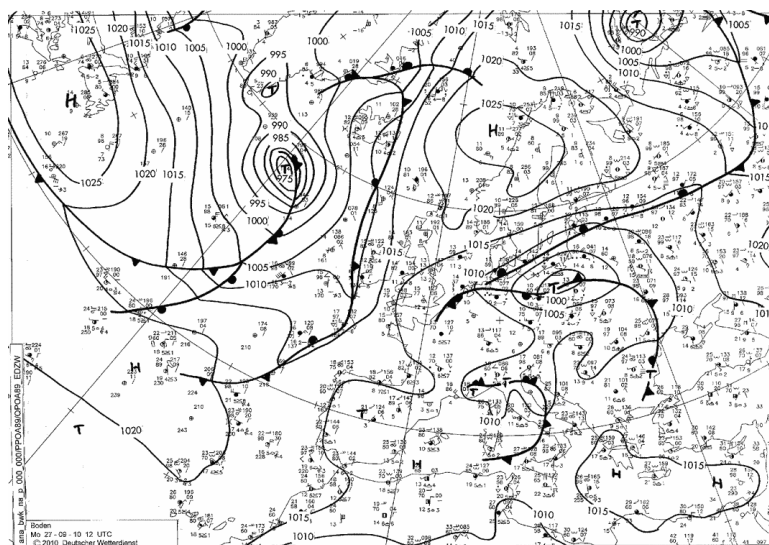
The analysis performed for situation with convective precipitation showed very good ability of H02 product in recognition of precipitation, especially moderate and heavy ones (rain rate > 10mm/h) while the light precipitation is either overestimated or missed.

The product tends to overestimate the precipitation areas and has some difficulties with proper recognition of rainfall maximum.

5.6.2 Case study: September 27th, 2010

Description

Low pressure centre left Hungary and heading through Slovak Republic entered Poland territory from South and is building up in the centre of the country. However the most rain productive clouds of that low will remain in the SW Poland even when the centre of the low pressure leave NE Poland. According to synoptic charts this low pressure centre will tend to deepen and build up due to feeding with cold air masses from over Barents Sea flowing between low over Scandinavia and above mentioned low pressure centre. This cold air will force up warm air masses. Condensing water vapor will stimulate clouds development and also emitting condensation energy supporting vorticity of the low pressure centre.



<http://www.wetter3.de>

Figure 83 Synoptic chart at 1200 UTC on 27th of September 2010

Comparison

On the next figure the H02 product is visualized for the noon overpass. For comparison, the distributions of 10 minute precipitation obtained from RG data measured at closest to the given time slots are presented. The RG derived precipitation maps were prepared using Near Neighbor method.

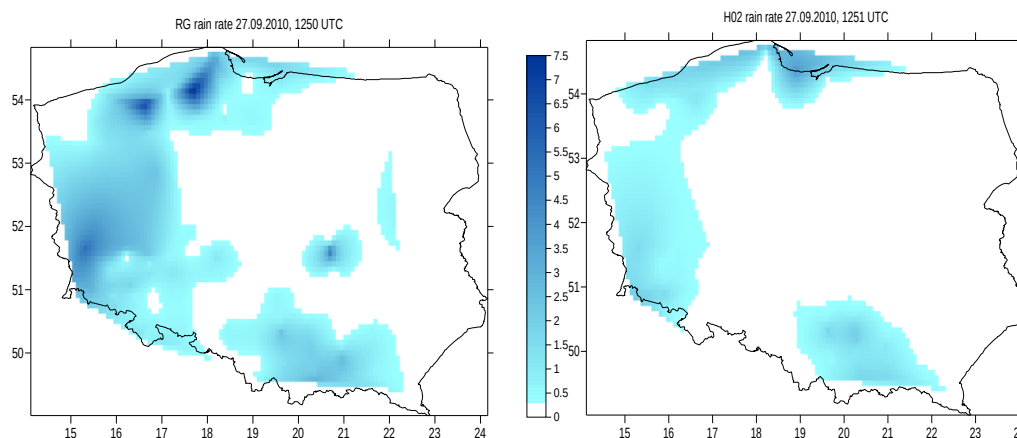


Figure 84 PR-OBS-1 at 1251 UTC on the 27th of September 2010 (right panel) and 10 minute precipitation interpolated from RG data from 1250 UTC (left panel)

On the both maps the precipitating area is located along with South, West and North Polish borderlines, however the its spatial distribution is underestimated by H02 product. Moreover, some rainfall observed in the Central Poland was not recognized by satellite product at all. The rainfall maxima measured by ground stations in western and northern Poland were missed by H02, what resulted in more homogenous precipitation distribution obtained for satellite product.

Statistical score

Further analysis was performed for all overpasses available for the 27th of September 2010. The ability of PR-OBS-01 product to recognize the precipitation was analyzed using dichotomous statistics parameters. The 0.25mm/h threshold was used to discriminate rain and no-rain cases. In the next

table the values of Probability of Detection (POD), False Alarm Rate (FAR) and Critical Success Ratio (CSI) are presented.

Parameter	Scores
POD	0.52
FAR	0.18
CSI	0.47

Table 34 Results of the categorical statistics obtained for H02 on the base of all data available on the 27th September 2010

Reasonably high value of POD and low value of FAR indicate that the product ability to recognize the stratiform precipitation is rather good.

The quality of H02 in estimating the convective precipitation is presented on the next figure Most of the points on the scatter plot are located under and along with the diagonal what indicates that that H02 tends to underestimate the rain rate rarely exceeding the 4 mm/h value.

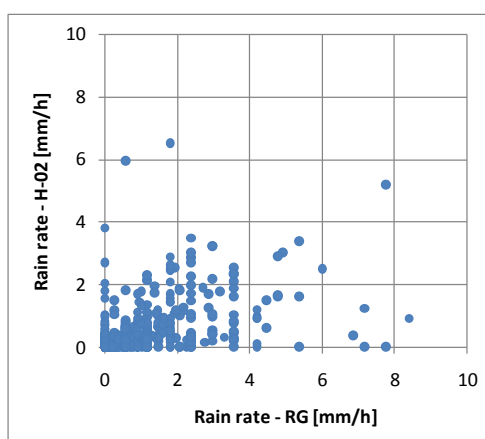


Figure 85 Scatter plot for measured (RG) and satellite derived (H-02) rain rate obtained for all H02 data on the 27th of September 2010

Finally, the analysis of rain classes was performed. The categories were selected in accordance with the common validation method. Next figure shows the percentage distribution of satellite derived precipitation categories within each precipitation class defined using ground measurements.

One can easily notice very good ability of H02 to recognize no-rain situations – more than 90% of ground cases was properly allocated by satellite product. The light precipitation is strongly underestimated – 68% of cases is allocated in the no-rain class. Better results were obtained for moderate precipitation: 40% of pixels in this class was properly recognized by H02, however, 34% of cases was overestimated and 27% was underestimated.

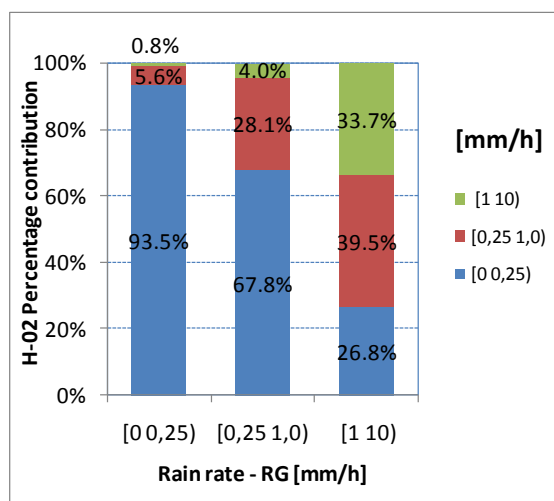


Figure 86 Percentage distribution of PR-OBS-1 precipitation classes in the rain classes defined using rain gauges (RG) data on the 27th of September 2010

Conclusions

The analysis performed for situation with stratiform precipitation showed reasonably good ability of H02 product in recognition of precipitation, however the product tends to underestimate the precipitation areas and has some difficulties with proper recognition of rainfall maximum.

The stratiform rain rate is underestimated, especially for light precipitation. For the moderate rainfall, the underestimation is not so strong.

5.7 Case study analysis in Slovakia

5.7.1 Case study: August 15th, 2010

Description

During the day, a cold front was moving over Slovakia territory towards North-East (next figure). The cold front was accompanied by thunderstorms and occasional torrential rainfall causing severe floods in some river catchments in the western half of Slovakia.

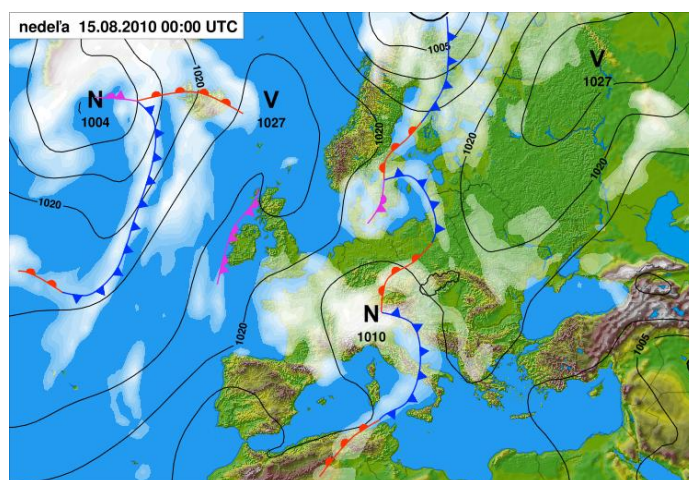


Figure 87 Synoptic situation on 15 August 2010 at 0:00 UTC

Data used

The EUMETSAT Network of Satellite Application Facilities  Support to Operational Hydrology and Water Management	Product Validation Report - PVR-02 (Product H02 – PR-OBS-2)	Doc.No: SAF/HSAF/PVR-02/1.1 Issue/Revision Index: 1.1 Date: 30/09/2011 Page: 110/177
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The H02 v2.2 data from two temporally close satellite passages over the SHMU validation area on 15 August 2010 have been selected: the NOAA18 observation at 12:07 UTC (average observation time of the SHMU validation area) and the NOAA19 observation at 12:08 UTC.

As ground data the instantaneous precipitation field derived by the SHMU radar network is used. The closest coincident fields (5 min time frequency) to the satellite passages have been selected: from 12:05 UTC and 12:10 UTC.

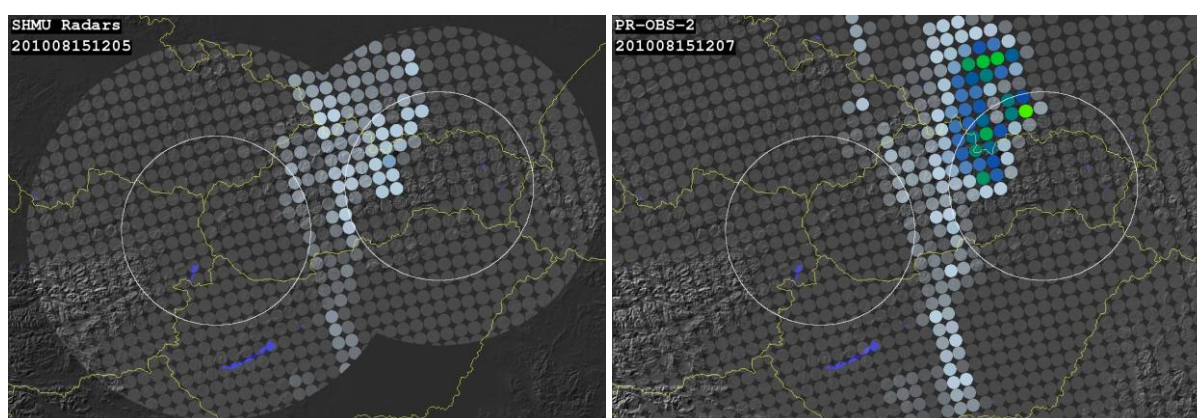
The radar composites used consist of data from two radars: one is situated at Maly Javornik and the second at Kojsovska hola. The rule of maximum value selection is applied in the composition. The original spatial resolution of the radar field is about 1 km but values upscaled into the satellite grid using the IFOV Gaussian filter are presented. For statistical scores computation only the data lying inside the 120 km rain effective range of both radars are considered.

Comparison

The H02 and upscaled radar precipitation fields for both satellite passages are presented in next figure. In both cases an overestimation of the precipitation by H02 compared to radars can be seen. This is obvious especially in case of higher precipitation intensities. It should be noted that lower radar intensities, especially near the Slovakia-Poland border, could be also caused by the radar beam blockage and/or attenuation in the precipitation.

For the passage of NOAA18 at 12:07 UTC (top row in the figure) the maximum value observed by radars is 7 mm/h while by H02 it is 22 mm/h. For the passage of NOAA19 at 12:08 UTC (second row in the figure) the corresponding maximum value is 3 mm/h and 20 mm/h, respectively. Spatial shift between the maxima in H02 and coincident radar field is about 65 km for the 12:07 UTC passage but only 16 km (1 satellite along-track sampling distance) in case of the 12:08 UTC passage.

Generally, there are slightly smaller differences between higher precipitation rates observed by H02 and radars for the 12:08 UTC passage. This could be a result of larger, closer to the swath edge, IFOVs that smooth more the extremes in precipitation fields. However, observation by different satellites and time lag between the compared fields could also be the reason.



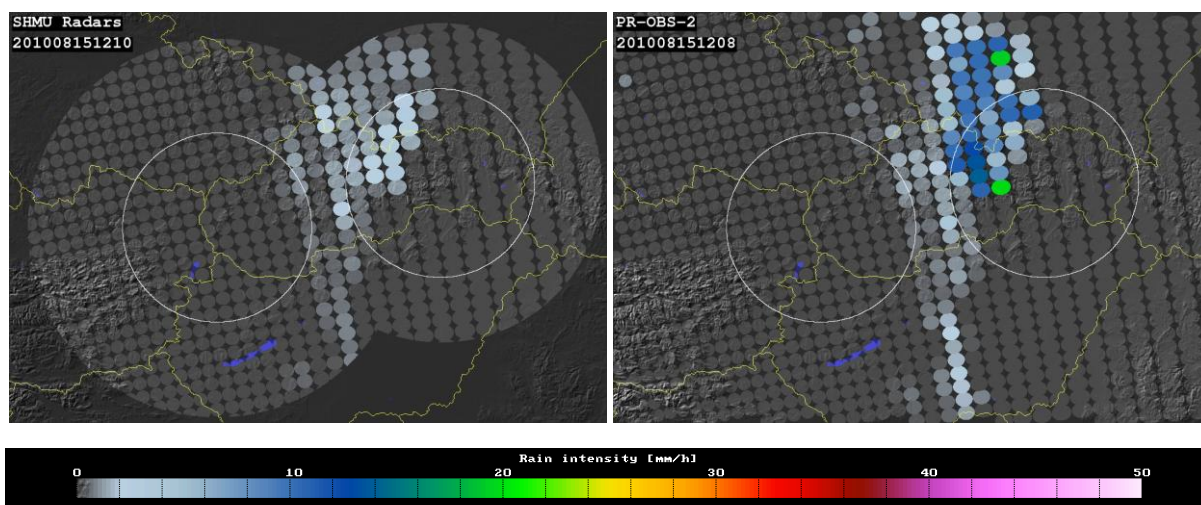


Figure 88 Instantaneous precipitation fields from 15 August 2010 observed by H02 product (left column) and SHMU radar network (right column) corresponding to NOAA18 passage at 12:07 UTC (top row) and NOAA19 passage at 12:08 UTC (second row)

The precipitation values are shown as satellite IFOVs projected over the radar composite domain. White contoured circles represent 120 km rain effective range of the radars inside which data are included in the statistical scores computation.

Despite the H02 overestimation a good spatial consistency between the H02 and radar precipitation fields can be observed. Even the patterns of light precipitation were localized by H02 quite well.

Scores evaluation

Statistical scores have been computed separately for each of the two satellite passages but also for common dataset from both passages. Totally 249 radar-satellite pairs from the 12:07 UTC passage and 190 pairs from the 12:08 UTC passage have been included in the computation. Results of the scores for continuous and dichotomous statistics for precipitation threshold of 0,25 mm/h are presented in the next two tables, respectively.

Satellite passage	12:07 UTC NOAA18	12:08 UTC NOAA19	Common
Number of satellite values	34	25	59
Number of radar values	28	22	50
Mean error (mm/h)	5.50	5.46	5.46
Standard deviation (mm/h)	5.67	4.93	5.34
Mean absolute error (mm/h)	5.64	5.48	5.57
Multiplicative bias	3.52	4.41	3.84
Correlation coefficient	0.63	0.39	0.56
Root mead square error (mm/h)	7.87	7.36	7.65
RMSE%	4.01	5.60	4.77

Table 35 Scores for continuous statistics for precipitation threshold of 0,25 mm/h

In agreement with visual comparison of precipitation fields, the scores of continuous statistics (Table 1) as Mean Error and Multiplicative bias exhibit overestimation of the H02 product in this case. The Multiplicative bias and URD-RMSE obtained for the 12:07 UTC passage are better than for the 12:08

UTC passage. This is in agreement with the observed better consistency of precipitation intensities in the first passage. However other scores such as Mean error do not confirm this observation. The values of correlation coefficient are relatively high and reflect good spatial consistency of the compared fields. Better values were obtained again for the 12:07 UTC passage.

Satellite passage	12:07 UTC NOAA18	12:08 UTC NOAA19	Common
POD	0.93	0.96	0.94
FAR	0.24	0.16	0.20
CSI	0.72	0.81	0.76

Table 36 Scores for dichotomous statistics for precipitation threshold of 0,25 mm/h

The POD (see Table 2) reaches values very close to 1 and the FAR values are on the other hand quite low. This also supports the observed good spatial match between the radar and H02 fields.

Conclusions

In this event of intense convective precipitation, the H02 product overestimated the precipitation as compared to radars, especially in case of higher precipitation rates. This is not in agreement with results of long-term statistics for August 2010 showing slight underestimation of H02.

The H02 overestimation was slightly lower in case of NOAA19 passage at 12:07 where the IFOVs were larger due to the longer distance from the satellite track compared to NOAA18 passage 1 min later. Thus heavy precipitation in horizontally small convective cells could have been more smoothed by the Gauss filter in the radar field. However, observation by different satellites or time lag between the compared fields could also be the reason of this discrepancy.

Despite the observed H02 overestimation the overall spatial consistency of the H02 and radar fields is satisfactory as confirmed by relatively good results of the correlation coefficient and very good scores of dichotomous statistics (see above).

5.8 Case study analysis in Turkey (ITU)

5.8.1 Case study: October 20th, 2010

Description

As it can be seen from next two figures, Turkey is in low pressure area and there are respectively warm and stationary fronts rain bands and precipitation in western part of Turkey on October 20 at 06:00 GMT and 12:00 GMT.

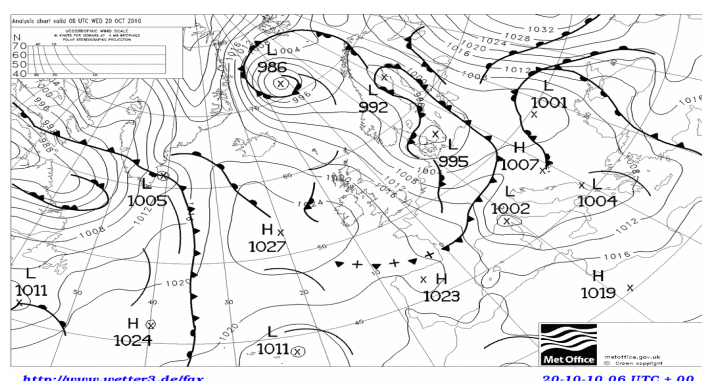


Figure 89 Atmospheric condition (20.10.2010; 06:00 GMT)

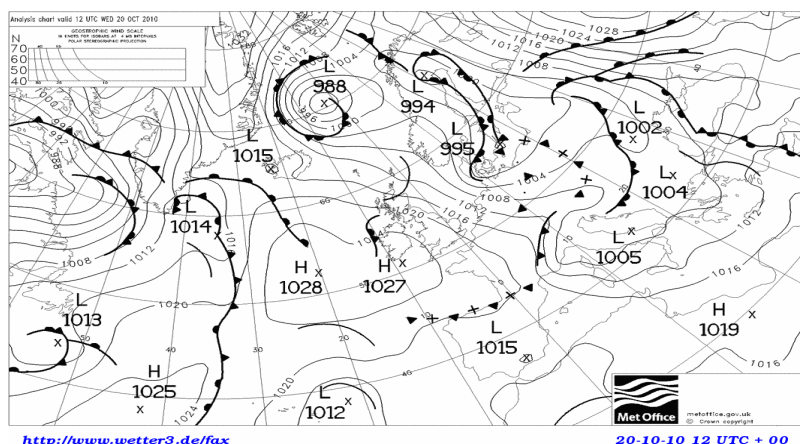


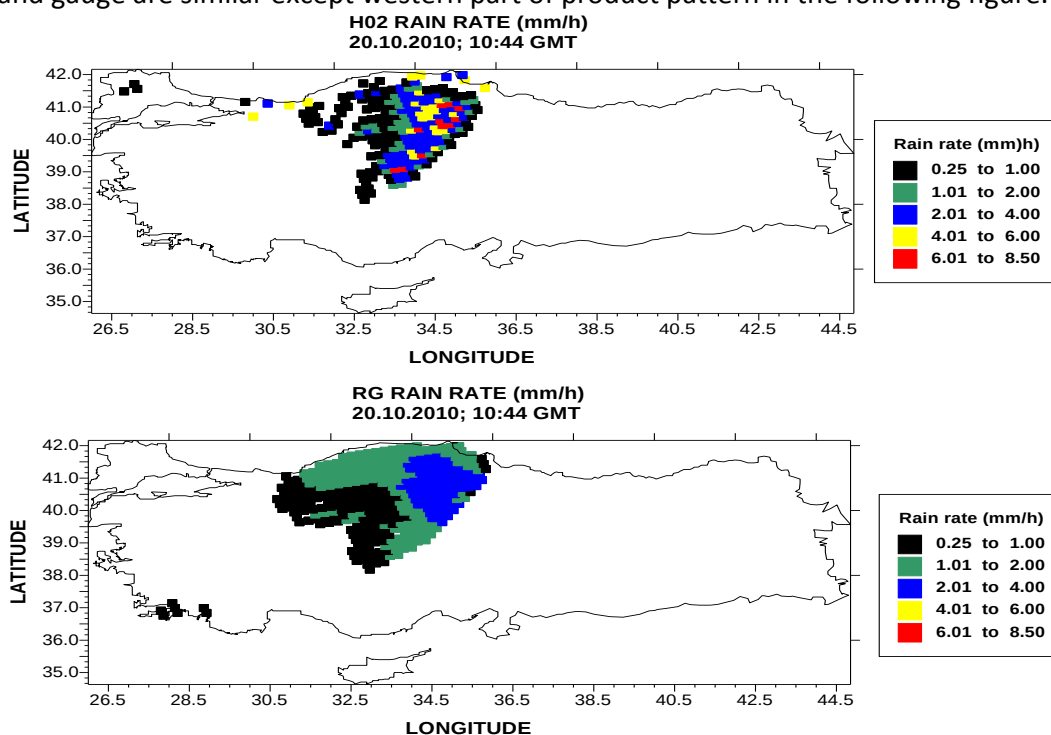
Figure 90 Atmospheric condition (20.10.2010; 12:00 GMT)

Data used

In this case study, 193 rain gauges, which have specifications as explained in section 4.12, in western part of Turkey has been used. H02 product on October 20 at 10:44 GMT has been compared with gauge observations. Moreover, synoptic cards from UK MetOffice have been taken for understanding the meteorological situation.

Comparison

Comparison of H02 product and rain gauge can be seen in next two figures. Values of H02 product are between 0.25 to 8.50 mm/h, but they vary from 0.25 to 4.00 mm/h for gauge. Main patterns of product and gauge are similar except western part of product pattern in the following figure.



According to ME (mean error) score in Table 37, there is no any underestimation or overestimation, but H02 product has higher rain rate values than rain gauge values in next figure.

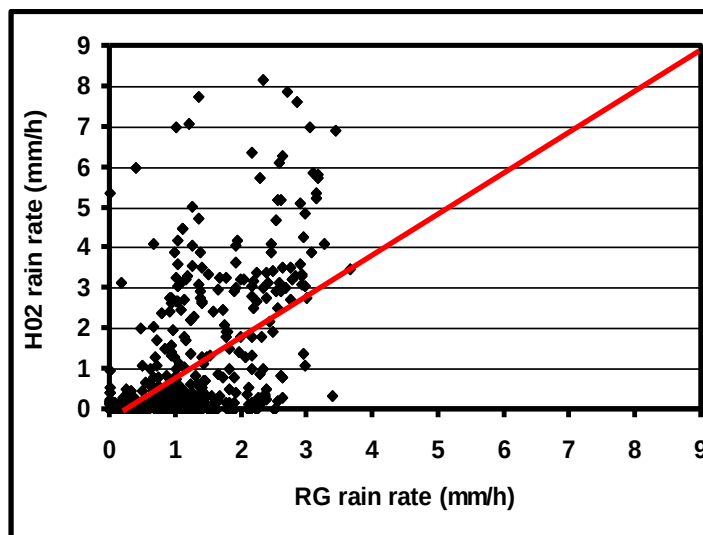


Figure 92 Scatter diagram of rain gauge and H02 product (Red line is 45 degree line)

Statistical scores

Statistics scores can be seen from Table 37. Correlation coefficient is 0.54 for H02 product. POD, FAR and CSI are respectively 0.64, 0.04 and 0.62 for this case study.

NS	NR	ME	SD	MAE	MB	CC	RMSE	URD	POD	FAR	CSI
494	752	-0.01	1.51	1.12	0.99	0.54	1.51	132%	0.64	0.04	0.62

Table 37 Statistic scores for H02

Conclusions

H02 product is not well enough to catch rainy area. In other words, frontal system is not well described generally by this product algorithm in terms of areal matching and quantitative estimate.

5.9 Conclusions

Eleven case study analysis of H02 have been here reported for 2010. Stratiform and convective precipitations during summer and winter periods have been analysed in different countries. Rain gauges with 10 minutes refresh time, radar data and nowcasting tools have been used to highlight different characteristics of the satellite product.

The case studies here proposed have pointed out that different statistical score values are obtained during summer and winter period.

In summer, when more convective events occur, all the countries have observed that H02 reproduces the rainfall patterns and amounts with quite good confidence. It has some difficulties with proper recognition of rainfall maximum. About the convective systems it has been observed that H02 did not well detect the small-medium size thunderstorms. This effect is due to a typical size of these convective cells which does not exceed the H02 (AMSU-B and HMS) IFOV. Capturing of convective

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cores by satellite IFOV or in upscaled radar image is strongly dependent on the mutual position of convective core and satellite IFOV centres. Other cases of medium-large size convective cells have showed a general correct qualitative location and estimation of the precipitation by H02, especially moderate and heavy ones (rain rate > 10mm/h) while the light precipitation is either overestimated or missed.

The dichotomous statistical scores evaluated for the summer cases have quite different values, mean values: POD 0.60, FAR 0.40 and CSI 0.40, but there are case studies with POD ranges between 0.8-0.9.

During winter period, when more stratiform events occur, the H02 product well detects the precipitation area, but it underestimates the precipitation (apart from few cases see Turkish and Polish cases). The satellite product misses or strongly underestimates the rainfall. In general for these events the FAR has an higher value than POD, and the CSI is average 0.15.

Some general satellite product characteristics have been highlighted by the case studies here proposed as that parallax shift is particularly effective in case of small convective structures and that ground data hourly cumulated use is incorrect for H02 validation (see Italian case study). This is due to the variability of the precipitation field, which cannot be caught by hourly integrals provided by the raingauges, especially in case of convective precipitation. It has also to be mentioned that differences between land and sea algorithms have not been observed.

It has been showed a case study (Poland) where the ground data have been unable to catch the precipitation system while the satellite product reproduced more correctly the precipitation area.

It is also interesting to stress the German case study where ground data of different sources (rain gauge and radar) have been used for validation exercise over the same region. The statistical scores obtained by rain gauge and radar data validation have very similar values.

6 Validation results: long statistic analysis

6.1 Introduction

In this Chapter the validation results of the H02 long statistic analysis are reported for the period (1.12.2009 – 31.11.2010). The validation has been performed on the product release currently in force at the time of writing.

Each Country/Team contributes to this Chapter by providing the monthly contingency tables and the statistical scores. The results are showed for radar and rain gauge, land and coast area in the three precipitation classes defined in table 7. The rain rates lower than 0.25 mm/h have been considered as no rain. The precipitation ground networks, instruments and data used for the validation of H02 have been described in Chapter 4.

To assess the degree of compliance of the product with user requirements all the PPVG members provided the long statistic results following the validation methodology reported in Chapter 3.

For product H02 the User requirements are recorded in Table 38.

Precipitation range	threshold	target	optimal
> 10 mm/h	90	80	25
1-10 mm/h	120	105	50
< 1 mm/h	240	145	90

Table 38 Accuracy requirements for product PR-OBS-1 [RMSE (%)]

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This implies that the main score to be evaluated has been the RMSE%. However, in order to give a more complete idea of the product error structure, several statistical scores have been evaluated as reported: Mean Error, Standard Deviation (SD) and Correlation Coefficient (CC), Probability Of Detection (POD), False Alarm Rate (FAR) and Critical Success Index (CSI). These scores have been defined in Section 3.7.

The long statistic results obtained in Belgium, Hungary, Germany, Italy, Poland, Slovakia and Turkey will be shown in the next sections. The country validation results are here reported in order to respond not only to the question whether the product meets the requirements or not, but also where meets or approaches or fails the requirements.

The average performance of H02 for all sites is presented in a compact, synoptic way in this chapter. The contents of the monthly statistical scores have been provided by the individual Countries/Teams and verified by the Validation Cluster Leader, step by step, as described in the Chapter 3. As stressed in Chapter 4, the average scores reported in the following tables have been obtained on measurements collected in heterogeneous geographical, orographical and climatological conditions.

6.2 The continuous statistic

There are three sets of columns:

- one set for Countries/Teams that has compared satellite data with meteorological radar in inner land areas: Belgium/BE, Germany/DE, Hungary/HU and Slovakia/SL; and their average weighed by the number of comparisons;
- one set for three Countries/Teams that has compared satellite data with rain gauges in inner land areas: Italy/IT, Germany/DE, Poland/PO and Turkey/TU; and their average weighed by the number of comparisons;
- one column for Turkey/TU that has compared satellite data with rain gauges in coastal areas.

In order to highlight the seasonal performances of H02 the statistical scores have been presented not only for yearly average but also for seasons averages. The seasons are reported in table 39.

Winter: Dec. 2009, Jan. and Feb. 2010	Spring: March, April and May 2010	Summer: June, July and August 2010	Autumn: Sept., Oct. and Nov. 2010
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Table 39 split in four sections, one for each season, reports the Country/Team results side to side

6.2.1 The winter period:

H02		BE	DE	HU	SL	TOTAL	IT	PO	TU	DE	TOTAL	TU coast
winter 2010												
Version 2.2		radar	radar	radar	radar	radar	gauge	gauge	gauge	gauge	gauge	gauge
NS	<1mm/h	1118	17006	7783	1441	27348	11895	378	10262	449	22984	663
NR	<1mm/h	10828	16267	25648	3279	56022	131498	5850	55783	6210	199341	6793
ME	<1mm/h	-0,43	-0,45	-0,31	-0,22	-0,37	-0,44	-0,46	-0,38	-0,44	-0,43	-0,28
SD	<1mm/h	0,19	0,39	0,59	0,46	0,45	0,54	0,29	1,05	0,31	0,67	0,97
MAE	<1mm/h	0,46	0,53	0,50	0,40	0,49	0,57	0,50	0,53	0,49	0,55	0,67
MB	<1mm/h	0,09	0,17	0,36	0,43	0,25	0,17	0,10	0,23	0,08	0,18	0,47
CC	<1mm/h	0,10	0,06	0,08	0,05	0,07	0,06	0,07	0,08	0,08	0,07	0,10
RMSE	<1mm/h	0,52	0,61	0,68	0,51	0,62	0,70	0,55	1,15	0,54	0,81	1,01
RMSE%	<1mm/h	105%	111%	152%	141%	131%	132%	102%	180%	107%	144%	215%
NS	1-10mm/h	411	3932	4583	557	9483	19171	136	5759	607	25673	1753
NR	1-10mm/h	1502	8537	5633	155	15827	83347	1306	20361	1391	106405	3483
ME	1-10mm/h	-1,31	-1,58	-1,08	-0,79	-1,37	-1,88	-1,36	-1,17	-1,32	-1,73	-1,00
SD	1-10mm/h	0,62	1,03	0,97	0,59	0,97	1,80	0,73	2,10	0,98	1,83	2,88
MAE	1-10mm/h	1,37	1,67	1,30	0,89	1,50	2,12	1,41	1,70	1,44	2,02	2,32
MB	1-10mm/h	0,16	0,15	0,36	0,41	0,23	0,17	0,09	0,36	0,15	0,21	0,53
CC	1-10mm/h	0,32	0,21	0,40	0,28	0,29	0,21	-0,01	0,21	0,11	0,20	0,17
RMSE	1-10mm/h	1,48	1,89	1,50	1,04	1,70	2,60	1,55	2,43	1,65	2,55	3,08
RMSE%	1-10mm/h	92%	94%	88%	74%	92%	102%	97%	145%	97%	110%	150%
NS	≥10mm/h	0	3	0	0	3	481	0	118	2	601	89
NR	≥10mm/h	0	3	0	0	3	805	0	17	1	823	25
ME	≥10mm/h	-	-11,5	-	-	-11,50	-16,03	- ,00	-9,83	-13,80	-15,90	-12,45
SD	≥10mm/h	-	3,841	-	-	3,84	15,20	- ,00	3,04	0,00	14,93	3,15
MAE	≥10mm/h	-	11,5	-	-	11,50	16,12	- ,00	9,83	13,80	15,99	12,45
MB	≥10mm/h	-	0,076	-	-	0,08	0,09	- ,00	0,16	0,00	0,09	0,00
CC	≥10mm/h	-	-0,846	-	-	-0,85	-0,12	- ,00	0,09	- ,00	-0,12	-0,34
RMSE	≥10mm/h	-	12,125	-	-	12,13	22,44	- ,00	10,21	13,80	22,17	12,83
RMSE%	≥10mm/h	-	91%	-	-	91%	91%	0%	87%	100%	91%	99%

Table 40 The main statistical scores evaluated by PPVG for H02 during the winter period. The rain rates lower than 0.25 mm/h have been considered as no rain

In Table 40 it can be seen that the scores obtained by radar data are very similar to the scores obtained by rain gauge data for all the precipitation classes. The RMSE % evaluated for light precipitation rain, rate lower than 1mm/h, has the highest value. The difficulty to estimate small precipitation intensities is not only of the satellite product, but also of rain gauge and radar instruments. This aspect has been highlighted also in Section 4.2 and 4.3 on ground data description.

Germany is the only country which has performed the validation using both radar and rain gauge data. The results reported in tab. 40 appear quite similar in particular for precipitation with rain rate lower than 10 mm/h. The difference for the heavy precipitation, rain rate greater than 10 mm/h, is probably due to the small number of samples of this class.

A general precipitation underestimation by H02 is reported in table 40 using both rain gauge and radar data for all the precipitation classes.

The winter average RMSE % evaluated using radar data have been (RMSE% CI1: 131%, CI2:92%, CI3:91%) and using rain gauge (RMSE% CI1: 144%, CI2:110%, CI3:91%).

A small Mean Error and Mean Absolute errors have been obtained for medium precipitation (rain rate between 1-10 mm/h) with radar (ME: -1,37 mm/h; MAE: 1,5 mm/h) and rain gauge (ME: -1,73 mm/h, MAE: 2,02) with a standard deviation respectively of 0.97 mm/h and 1.83 mm/h.

6.2.2 The Spring period

H02		BE	DE	HU	SL	TOT	IT	PO	TU	DE	TOT	TU coast
		spring 2010										
Version 2.2		radar	radar	radar	radar	radar	gauge	gauge	gauge	gauge	gauge	gauge
NS	<1mm/h	3343	19496	25315	9561	57715	12246	2334	17105	2578	34263	898
NR	<1mm/h	9850	9061	40753	11495	71159	57309	8886	35590	7380	109165	4177
ME	<1mm/h	-0,39	0,33	-0,04	0,20	0,00	-0,36	-0,36	-0,25	-0,31	-0,32	0,02
SD	<1mm/h	0,20	1,12	1,73	1,09	1,34	0,80	0,66	1,09	0,65	0,88	1,41
MAE	<1mm/h	0,47	0,67	0,60	0,55	0,58	0,59	0,52	0,58	0,50	0,57	0,85
MB	<1mm/h	0,22	1,69	0,90	1,41	0,99	0,32	0,32	0,50	0,35	0,38	1,06
CC	<1mm/h	0,11	0,27	0,12	0,23	0,15	0,07	0,06	0,05	0,10	0,06	0,16
RMSE	<1mm/h	0,56	1,17	1,78	1,12	1,43	0,90	0,81	1,17	0,75	0,97	1,45
RMSE%	<1mm/h	116%	267%	444%	266%	347%	164%	146%	284%	155%	201%	303%
NS	1-10mm/h	1151	10450	12970	3836	28441	14105	1370	6974	1167	23616	2039
NR	1-10mm/h	3021	3502	13741	1241	21505	35710	4781	11387	2296	54174	2109
ME	1-10mm/h	-1,34	-0,18	-0,35	1,03	-0,38	-1,73	-1,59	-1,36	-1,09	-1,61	-0,61
SD	1-10mm/h	1,37	2,11	2,34	3,11	2,21	1,90	1,56	1,38	1,72	1,75	3,12
MAE	1-10mm/h	1,65	1,50	1,46	1,60	1,50	2,04	1,75	1,60	1,53	1,90	2,50
MB	1-10mm/h	0,36	0,92	0,80	1,72	0,81	0,25	0,25	0,25	0,40	0,26	0,75
CC	1-10mm/h	0,39	0,27	0,27	0,40	0,29	0,23	0,17	0,11	0,28	0,20	0,13
RMSE	1-10mm/h	2,03	2,12	2,43	3,29	2,37	2,60	2,24	1,94	2,07	2,41	3,19
RMSE%	1-10mm/h	96%	105%	165%	166%	146%	113%	94%	97%	117%	108%	152%
NS	≥10mm/h	13	50	354	0	417	418	6	115	22	561	57
NR	≥10mm/h	35	64	40	0	139	533	94	44	9	680	16
ME	≥10mm/h	-8,61	-16,89	-1,27	-	-10,31	-13,82	-24,96	-13,38	-11,06	-15,30	-15,14
SD	≥10mm/h	2,21	14,08	11,82	-	10,44	7,06	20,24	6,05	4,69	8,78	5,17
MAE	≥10mm/h	8,73	17,15	7,45	-	12,24	13,89	24,96	13,38	11,06	15,35	15,14
MB	≥10mm/h	0,33	0,17	0,91	-	0,42	0,10	0,05	0,07	0,21	0,10	0,08
CC	≥10mm/h	0,56	-0,35	0,07	-	0,00	-0,04	0,09	0,21	-0,02	-0,01	-
RMSE	≥10mm/h	9,12	22,00	11,89	-	15,85	15,56	32,17	14,82	12,01	17,76	16,08
RMSE%	≥10mm/h	71%	81%	92%	-	82%	91%	93%	93%	81%	91%	92%

Table 41 The main statistical scores evaluated by PPVG for H02 during the spring period. The rain rates lower than 0.25 mm/h have been considered as no rain

In Table 41 it can be seen that the scores obtained by radar data are quite different from the scores obtained by rain gauge data for light precipitation (rain rate < 1 mm/h). Besides, the RMSE % of this precipitation class has the highest value. This is due to the RMSE% evaluated by Hungary. An investigation on this result is in progress.

The statistical scores evaluated for precipitation classes 2 and 3, using both rain gauge and radar data, are quite similar.

A general precipitation underestimation by H02 is reported in table 42 using both rain gauge and radar data for all precipitation classes.

The spring average RMSE % evaluated using radar data have been (RMSE% CI1: 347%, CI2:145%, CI3:81%) and using rain gauge (RMSE% CI1: 201%, CI2:108%, CI3:91%).

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A small Mean Error and Mean Absolute errors have been obtained for medium precipitation (rain rate between 1-10 mm/h) with radar (ME: -0,38 mm/h; MAE: 1,5 mm/h) and rain gauge (ME: -1,61 mm/h, MAE: 1,9) with a standard deviation respectively of 2.21 mm/h and 1.75 mm/h.

6.2.3 The summer period

H02		BE	DE	HU	SL	TOT	IT	PO	TU	DE	TOT	TU coast
		summer 2010										
Version 2.2		radar	radar	radar	radar	radar	gauge	gauge	gauge	gauge	gauge	gauge
NS	<1mm/h	8105	16863	24289	12951	62208	7216	2785	7395	4879	22275	346
NR	<1mm/h	9995	18786	28570	12962	70313	11803	5590	13508	7290	38191	2051
ME	<1mm/h	-0,19	0,27	0,01	0,54	0,15	-0,18	-0,11	-0,11	-0,15	-0,14	0,27
SD	<1mm/h	0,21	1,26	1,00	1,21	0,99	1,19	0,96	1,17	0,95	1,10	2,05
MAE	<1mm/h	0,51	0,68	0,51	0,73	0,60	0,66	0,57	0,64	0,57	0,62	1,06
MB	<1mm/h	0,63	1,56	1,02	2,07	1,30	0,66	0,80	0,77	0,70	0,73	1,56
CC	<1mm/h	0,12	0,23	0,23	0,33	0,23	0,07	0,14	0,11	0,09	0,10	0,08
RMSE	<1mm/h	0,87	1,29	1,01	1,33	1,12	1,21	0,97	1,18	0,97	1,12	2,10
RMSE%	<1mm/h	189%	289%	181%	265%	226%	251%	195%	254%	206%	235%	521%
NS	1-10mm/h	3879	15235	14556	7575	41245	5986	2733	4457	2470	15646	941
NR	1-10mm/h	5938	10177	16757	2869	35741	12356	4777	5136	3820	26089	553
ME	1-10mm/h	-1,35	-0,28	-0,10	1,79	-0,21	-1,70	-1,30	-1,31	-1,16	-1,47	-1,24
SD	1-10mm/h	1,53	2,58	2,92	3,22	2,62	2,63	2,67	2,12	1,96	2,44	1,96
MAE	1-10mm/h	1,75	1,79	1,86	2,28	1,86	2,43	2,02	1,98	1,70	2,16	2,03
MB	1-10mm/h	0,45	0,89	0,94	2,02	0,93	0,40	0,52	0,40	0,46	0,43	0,40
CC	1-10mm/h	0,25	0,22	0,40	0,46	0,33	0,24	0,18	0,11	0,25	0,21	0,15
RMSE	1-10mm/h	2,29	2,60	2,96	3,70	2,80	3,17	2,97	2,50	2,30	2,87	2,42
RMSE%	1-10mm/h	87%	120%	133%	209%	128%	108%	110%	121%	101%	110%	116%
NS	≥10mm/h	68	268	1024	0	1360	431	97	108	62	698	0
NR	≥10mm/h	77	202	359	0	638	584	309	21	80	994	0
ME	≥10mm/h	-13,68	-7,29	-5,13	-	-6,85	-12,22	-15,53	-7,59	-9,92	-12,97	-
SD	≥10mm/h	8,27	6,65	7,31	-	7,22	9,31	9,88	6,70	5,83	9,15	-
MAE	≥10mm/h	14,28	8,89	7,61	-	8,82	13,12	15,57	8,63	10,75	13,60	-
MB	≥10mm/h	0,20	0,48	0,66	-	0,55	0,23	0,18	0,41	0,30	0,23	-
CC	≥10mm/h	0,17	0,28	0,28	-	0,26	0,00	0,42	-0,76	0,26	0,13	-
RMSE	≥10mm/h	16,64	9,91	9,36	-	10,42	15,37	18,42	10,02	11,94	15,93	-
RMSE%	≥10mm/h	83%	71%	59%	-	66%	85%	84%	71%	79%	84%	-

Table 42 The main statistical scores evaluated by PPVG for H02 during the summer period. The rain rates lower than 0.25 mm/h have been considered as no rain

In Table 42 it can be seen that the scores obtained by radar data are quite similar to the scores obtained by rain gauge data for all precipitation classes. The RMSE % for the light precipitation has the highest value as during the other seasons.

A general precipitation underestimation by H02 is reported in table 42 using both rain gauge and radar data for rain rate greater than 1 mm/h. Besides a precipitation overestimation by H02 has been found for light precipitation (rain rate < 1mm/h) using radar data.

The spring average RMSE % evaluated using radar data have been (RMSE% CI1: 226%, CI2:127%, CI3:66%) and using rain gauge (RMSE% CI1: 235%, CI2:109%, CI3:84%).

The worst statistical scores during this season have been obtained over coastal areas by Turkey.

6.2.4 The autumn period

H02		BE	DE	HU	SL	TOT	IT	PO	TU	DE	TOT	TU coast
		autumn 2010										
Version 2.2		radar	radar	radar	radar	radar	gauge	gauge	gauge	gauge	gauge	gauge
NS	<1mm/h	5978	20251	22648	8224	57101	10554	1506	12677	2857	27594	578
NR	<1mm/h	11845	11886	25609	9720	59060	32554	4177	33369	6469	76569	4514
ME	<1mm/h	-0,32	0,27	-0,15	0,25	-0,03	-0,25	-0,38	-0,32	-0,35	-0,30	0,07
SD	<1mm/h	0,21	0,86	0,57	0,85	0,60	1,12	0,44	0,61	0,48	0,81	1,43
MAE	<1mm/h	0,45	0,58	0,43	0,56	0,48	0,68	0,49	0,51	0,48	0,58	0,91
MB	<1mm/h	0,38	1,59	0,70	1,52	0,95	0,54	0,30	0,37	0,32	0,44	1,12
CC	<1mm/h	0,21	0,23	0,24	0,36	0,25	0,06	0,11	0,09	0,12	0,08	0,11
RMSE	<1mm/h	0,56	0,91	0,59	0,89	0,70	1,17	0,58	0,70	0,59	0,88	1,44
RMSE%	<1mm/h	107%	222%	125%	202%	153%	245%	106%	140%	118%	181%	326%
NS	1-10mm/h	1569	11033	9541	3146	25289	13241	774	6808	1039	21862	2645
NR	1-10mm/h	3614	3780	10123	819	18336	31768	2611	15989	2810	53178	2815
ME	1-10mm/h	-1,13	-0,52	-0,55	0,45	-0,61	-1,90	-1,42	-1,36	-1,28	-1,68	-0,32
SD	1-10mm/h	0,72	1,51	1,18	1,42	1,17	2,44	1,33	1,93	1,20	2,17	3,27
MAE	1-10mm/h	1,25	1,21	1,02	1,15	1,11	2,43	1,57	1,85	1,47	2,16	2,49
MB	1-10mm/h	0,34	0,73	0,70	1,34	0,66	0,32	0,31	0,39	0,29	0,34	0,86
CC	1-10mm/h	0,20	0,11	0,37	0,15	0,27	0,26	0,22	0,23	0,23	0,25	0,25
RMSE	1-10mm/h	1,45	1,62	1,31	1,53	1,41	3,11	1,95	2,37	1,76	2,76	3,29
RMSE%	1-10mm/h	79%	83%	70%	117%	77%	103%	82%	98%	90%	100%	162%
NS	≥10mm/h	0	3	0	0	3	935	0	193	33	1161	114
NR	≥10mm/h	0	7	0	0	7	1191	14	256	7	1468	60
ME	≥10mm/h	-	-12,96	-	-	-12,96	-12,84	-13,10	-10,19	-13,02	72,69	-8,60
SD	≥10mm/h	-	1,28	-	-	1,28	9,97	6,04	6,63	4,58	9,33	9,26
MAE	≥10mm/h	-	12,96	-	-	12,96	13,87	13,10	11,57	13,02	13,46	11,74
MB	≥10mm/h	-	0,04	-	-	0,04	0,25	0,04	0,26	0,11	0,25	0,43
CC	≥10mm/h	-	0,97	-	-	0,97	0,16	-0,10	0,06	-0,85	0,14	0,23
RMSE	≥10mm/h	-	13,02	-	-	13,02	16,40	14,43	12,54	13,97	15,69	12,59
RMSE%	≥10mm/h	- %	97%	- %	- %	97%	84%	95%	88%	90%	85%	83%

Table 43 The main statistical scores evaluated by PPVG for H02 during the autumn period. The rain rates lower than 0.25 mm/h have been considered as no rain

A general precipitation underestimation by H02 is reported in table 43 using both rain gauge and radar data for all the precipitation classes. The statistical scores obtained during this season with both radar data (RMSE% CI1: 153%, CI2:77%, CI3:97%) and rain gauge (RMSE% CI1: 181%, CI2:100%, CI3:85%) are the best ones of all the year.

6.2.5 The annual average

PR-OBS-2		BE	DE	HU	SL	TOT	IT	PO	TU	DE	TOT	TU coast
		DIC.09-NOV.10										
Version 2.2		radar	radar	radar	radar	radar	gauge	gauge	gauge	gauge	gauge	gauge
NS	<1mm/h	18544	73616	80035	32177	204372	41911	7003	47439	10763	107116	2485
NR	<1mm/h	42518	56000	120580	37456	256554	233164	24503	138250	27349	423266	17535
ME	<1mm/h	-0,33	0,07	-0,11	0,29	-0,05	-0,38	-0,33	-0,31	-0,31	-0,35	-0,05
SD	<1mm/h	0,20	0,90	1,07	1,01	0,88	0,72	0,60	0,97	0,61	0,79	1,32
MAE	<1mm/h	0,47	0,61	0,52	0,60	0,54	0,59	0,52	0,55	0,51	0,57	0,82
MB	<1mm/h	0,33	1,18	0,77	1,58	0,91	0,28	0,37	0,39	0,38	0,33	0,91
CC	<1mm/h	0,14	0,19	0,16	0,29	0,18	0,06	0,09	0,08	0,10	0,07	0,12
RMSE	<1mm/h	0,62	0,99	1,11	1,08	1,00	0,84	0,75	1,05	0,72	0,89	1,35
URD	<1mm/h	128%	220%	252%	238%	222%	162%	140%	205%	149%	174%	300%
NS	1-10mm/h	7010	40650	41650	15114	104458	52503	5013	23998	5283	86797	7378
NR	1-10mm/h	14075	25996	46254	5084	91409	163181	13475	52873	10317	239846	8960
ME	1-10mm/h	-1,29	-0,73	-0,39	1,31	-0,53	-1,83	-1,43	-1,28	-1,20	-1,66	-0,71
SD	1-10mm/h	1,19	1,85	2,13	2,83	1,95	2,01	1,83	1,90	1,57	1,95	3,00
MAE	1-10mm/h	1,56	1,63	1,49	1,89	1,56	2,19	1,78	1,75	1,57	2,04	2,40
MB	1-10mm/h	0,37	0,63	0,78	1,79	0,73	0,24	0,34	0,35	0,36	0,27	0,68
CC	1-10mm/h	0,28	0,21	0,35	0,39	0,30	0,23	0,17	0,18	0,23	0,21	0,18
RMSE	1-10mm/h	1,93	2,16	2,26	3,17	2,23	2,74	2,37	2,31	2,02	2,60	3,13
URD	1-10mm/h	87%	104%	123%	180%	115%	105%	98%	118%	101%	107%	152%
NS	≥10mm/h	90	324	1397	0	1811	2265	103	534	119	3021	260
NR	≥10mm/h	112	276	399	0	787	3113	417	338	97	3965	101
ME	≥10mm/h	-12,09	-9,71	-4,75	- ,00	-7,53	-13,72	-17,58	-10,43	-10,29	17,74	-10,59
SD	≥10mm/h	6,38	8,21	7,76	- ,00	7,72	10,70	12,08	6,38	5,58	10,35	7,10
MAE	≥10mm/h	12,55	10,94	7,60	- ,00	9,47	14,32	17,60	11,53	10,98	14,34	12,45
MB	≥10mm/h	0,24	0,39	0,68	- ,00	0,52	0,18	0,15	0,24	0,28	0,18	0,27
CC	≥10mm/h	0,30	0,14	0,26	- ,00	0,22	0,02	0,33	0,03	0,15	0,06	0,07
RMSE	≥10mm/h	14,29	12,82	9,62	- ,00	11,40	17,62	21,39	12,56	12,11	17,45	13,20
URD	≥10mm/h	79%	74%	63%	- %	69%	87%	87%	88%	80%	87%	88%

Table 44 The main statistical scores evaluated by PPVG for H02 during one year of data 1st December 2009- 30th November 2010 . The rain rates lower than 0.25 mm/h have been considered as no rain

The yearly averages obtained by all the countries using both radar and rain gauge data are similar. The worst RMSE% has been evaluated for light precipitation comparing H02 precipitation estimations with radar data. In this case there is a precipitation overestimation by the satellite product but in general a clear precipitation underestimation by H02 is reported in tab 44.

The yearly averages of RMSE% obtained with radar data (RMSE% CI1: 222%, CI2:115%, CI3:69%) and with rain gauge (RMSE% CI1: 174%, CI2:107%, CI3:87%).

A small Mean Error and Mean Absolute errors have been obtained for medium precipitation (rain rate between 1-10 mm/h) with radar (ME: -0,53 mm/h; MAE: 1,56 mm/h) and rain gauge (ME: -1,66 mm/h, MAE: 2,04) with a standard deviation respectively of 1.95 mm/h and 1.95 mm/h.

6.3 The multi-categorical statistic

Two sets of validation have been performed:

- one set for Countries/Teams that has compared satellite data with meteorological radar in inner land areas: Belgium/BE, Germany/DE, Hungary/HU and Slovakia/SL;
- one set for Countries/Teams that has compared satellite data with rain gauges in inner land areas: Italy/IT, Germany/DE, Poland/PO and Turkey/TU.

Each Country/Team contributes to this Chapter by providing the monthly contingency table and the statistical scores. The Validation Cluster Leader has collected all the validation files, has verified the consistency of the results and evaluated the monthly and yearly contingency tables and the statistical scores.

6.3.1 radar validation

	Dec-09	Jan-10	Feb.-10	Mar.-10	Apr.-10	May.-10	Jun.-10	Jul.-10	Aug-10	Sep-10	Oct-10	Nov-10	tot
POD with RR ≥ 0.25 mm/h	0,25	0,18	0,17	0,27	0,27	0,61	0,61	0,63	0,65	0,65	0,38	0,37	0,47
FAR with RR ≥ 0.25 mm/h	0,63	0,82	0,77	0,70	0,63	0,41	0,34	0,35	0,39	0,38	0,61	0,39	0,47
CSI with RR ≥ 0.25 mm/h	0,18	0,10	0,11	0,17	0,18	0,43	0,47	0,47	0,46	0,47	0,24	0,30	0,33
POD with RR ≥ 1 mm/h	0,17	0,21	0,16	0,31	0,27	0,53	0,52	0,57	0,58	0,53	0,33	0,26	0,43
FAR with RR ≥ 1 mm/h	0,83	0,82	0,85	0,76	0,81	0,60	0,53	0,52	0,54	0,59	0,74	0,61	0,62
CSI with RR ≥ 1 mm/h	0,09	0,11	0,08	0,15	0,13	0,29	0,33	0,35	0,35	0,30	0,17	0,19	0,25

Table 45 The averages POD, FAR and CSI deduced comparing H02 with radar data

	mm/h	Radar data			
		PR<0.25	0.25≤PR<1.00	1.00≤PR<10.00	10.00≤PR
Satellite data	PR<0.25	98%	61%	31%	5%
	0.25≤PR<1.00	2%	26%	26%	11%
	1.00≤PR<10.00	1%	14%	42%	50%
	10.00≤PR	0%	0%	1%	34%

Table 46 The contingency table for the three precipitation classes defined in table 7 evaluated by comparing H02 with radar data

The averages of POD : 0.47, FAR: 0.47 and CSI:0.33 have been obtained using radar data on one year of data 1st December 2009- 30th November 2010.

In table 46 it is possible to see that 98% of no rain is correctly classified by H02. There is a general precipitation underestimation by H02.

6.3.2 rain gauge validation

	Dec-09	Jan-10	Feb.-10	Mar.-10	Apr.-10	May.-10	Jun.-10	Jul.-10	Aug-10	Sep-10	Oct-10	Nov-10	TOT
POD with RR $\geq$ 0.25 mm/h	0,11	0,09	0,11	0,13	0,18	0,33	0,34	0,39	0,42	0,32	0,30	0,19	0,18
FAR with RR $\geq$ 0.25 mm/h	0,31	0,33	0,34	0,45	0,49	0,47	0,46	0,47	0,36	0,36	0,30	0,32	0,40
CSI with RR $\geq$ 0.25 mm/h	0,10	0,08	0,11	0,12	0,15	0,26	0,26	0,29	0,34	0,27	0,27	0,17	0,16
POD with RR $\geq$ 1 mm/h	0,12	0,12	0,13	0,15	0,14	0,25	0,26	0,36	0,36	0,25	0,27	0,18	0,18
FAR with RR $\geq$ 1 mm/h	0,50	0,50	0,46	0,57	0,66	0,59	0,57	0,53	0,43	0,48	0,44	0,43	0,52
CSI with RR $\geq$ 1 mm/h	0,11	0,10	0,12	0,13	0,11	0,18	0,19	0,26	0,28	0,20	0,22	0,16	0,15

Table 47 The averages POD, FAR and CSI deduced comparing H02 with rain gauge data

		Radar data			
	mm/h	PR<0.25	0.25≤PR<1.00	1.00≤PR<10.00	10.00≤PR
Satellite data	PR<0.25	98%	88%	70%	43%
	0.25≤PR<1.00	1%	7%	12%	13%
	1.00≤PR<10.00	1%	5%	17%	35%
	10.00≤PR	0%	0%	1%	9%

Table 48 The contingency table for the three precipitation classes defined in table 7 evaluated by comparing H02 with rain gauge data

The averages of POD : 0.18, FAR: 0.40 and CSI:0.16 have been obtained using rain gauge data on one year of data 1st December 2009- 30th November 2010.

In table 48 it is possible to see that 98% of no rain is correctly classified by H02. There is a general precipitation underestimation by the satellite product H02.

6.4 User requirement compliance

In table 49 In table 6.9 the statistical scores obtained by the yearly validation of H02 with radar and rain gauge data are reported. **The statistical scores reach the thresholds stated in the User Requirements for land areas in all cases using both rain gauge and satellite data as ground reference. Only for precipitation lower than 10 mm/h using rain gauge in coast areas the threshold is not completely reached.** This result might be explained by considering the difficulty of rain gauge to evaluate the precipitation in a coastal IFOV with a large part covered by sea.

Between target and optimal	Between threshold and target	Threshold exceeded by < 50 %	Threshold exceeded by ≥ 50 %
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PR-OBS-1 v2.2				Annual average of RMSE%		
Precipitation class	Requirement (RMSE %)			radar land	gauge land	gauge coast
	thresh	target	optimal			
> 10 mm/h	90	80	25	69%	87%	88%
1-10 mm/h	120	105	50	115%	107%	152%
< 1 mm/h	240	145	90	222%	173%	300%

Table 49 User requirement and compliance analysis for product H02

As reported in Annex 8 the results obtained by the current validation procedure represent the convolution of at least three factors: the satellite product accuracy, the accuracy of the ground data used and the limitations of the comparison methodology (e.g., errors of space and time co-location, representativeness changing with scale, etc.). Therefore, the results currently found are by far pessimistic in respect of what is the real product performance.

7 Conclusions

7.1 Summary conclusions on the status of product validation

The H02 product has been validated by the PPVG on one year of data 1st of December 2009 – 30th of November 2010. Each Country/Team have provided case study and long statistic analysis using radar and rain gauge following the validation methodology reported in Chapter 3.

The results of the Precipitation Validation Programme are reported in this Product Validation Report (PVR). A precipitation product validation section of the H-SAF web page is under development. This validation web section will be continuously updated with the last validation results and studies coming from the Precipitation Product Validation Group (SPVG).

It is well know that radar and rain gauge rainfall estimation is influenced by several error sources that should be carefully handled and characterized before using these data as reference for ground validation of any satellite-based precipitation products. A complete inventory of the precipitation ground networks, instruments and data available inside the PPVG has been provided in Chapter 4 in order to highlight the main error sources and to present possible methodology for selecting the

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ground data more reliable (Annex 1-7). In the last months the first example of precipitation fields integration has been also provided (Section 4.4.3): INCA and RADOLAN products. The INCA system, a tool for the precipitation products validation, is available in Slovakia and Poland, in both countries being run in pre-operational mode. In Germany similar precipitation analysis system called RADOLAN is being run operationally. The study performed in the PPVG (*Annex 5*) showed that the accuracy and reliability of the raingauge stations significantly affect final precipitation analysis of the INCA or INCA-like systems. In order to solve this problem an automated blacklisting technique is going to be developed at SHMÚ (currently blacklisting is used in manual mode).

Eleven case study analysis of H02 have been here reported in Chapter 5. Stratiform and convective precipitations during summer and winter periods have been analysed in different countries. Rain gauges with 10 minutes refresh time, radar data and nowcasting tools have been used to highlight different characteristics of the satellite product. The case studies proposed have pointed out that different statistical score values are obtained during summer and winter period, problems on coast line and parallax shift. It has been also showed a case study (Poland) where the ground data have been unable to catch the precipitation system while the satellite product reproduced more correctly the precipitation area.

In Chapter 6 the validation results of the H02 long statistic analysis obtained for the period (1.12.2009 – 31.11.2010), have been presented. To assess the degree of compliance of the product with user requirements Each Country/Team has provided the monthly contingency tables and the statistical scores. The results have been showed for radar and rain gauge, land and coast area in the three precipitation classes defined in table 7. The rain rates lower than 0.25 mm/h have been considered as no rain.

The statistical scores evaluated by the PPVG reach the thresholds stated in the User Requirements in all cases using both rain gauge and radar data as ground reference. Only for precipitation lower than 1 mm/h using rain gauge in coast areas the threshold is not completely reached. This result might be explained by considering the difficulty of rain gauge to evaluate the precipitation in a coastal IFOV with a large part covered by sea. As reported in Annex 8 the results obtained by the current validation procedure represent the convolution of at least three factors: the satellite product accuracy, the accuracy of the ground data used and the limitations of the comparison methodology (e.g., errors of space and time co-location, representativeness changing with scale, etc.). Therefore, the results currently found are by far pessimistic in respect of what is the real product performance.

7.2 Next steps

On the base of the development phase it is possible to say that the ground data error characterization is necessary and that a validation of a common protocol is not enough. Only the use of the same software can guarantee that the results obtained by several institutes are obtained in the same way. To improve the validation methodology and to develop software used by all members of the validation cluster several working groups have been composed during the last Validation Workshop held in Bratislava, 20-22 October 2010 (see annex 1,2,3,4,5,6,7).

On the base of published papers and the characteristics of the ground data available inside the PPVG the main next steps are foreseen in order to improve the validation methodology:

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- quantitative estimation of the errors introduced in the validation procedure comparing the instantaneous satellite precipitation estimation with the rain gauge precipitation cumulated on different intervals;
- definition of a rain gauge and radar data quality check;
- application of the data quality check to all radar and rain gauge data used in the PPVG;
- definition of the optimal and minimal spatial density of rain gauge stations to be representative of the ground precipitation in the view of satellite product comparison;
- development of the three software for raingauges, radar and INCA products up-scaling vs AMSU and MHS grids;
- definition and code implementation of the technique for the temporal matching of satellite rain rate with rain gauge and radar data;
- selection of the appropriate methodology for spatial distribution of precipitation products errors taking into consideration spatial and temporal characteristics of each product for selected areas as test catchments.

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8 Annex 1: Status of working group

Working Group 1: “Rain gauge data”

Coordinator: Federico Porcù (University of Ferrara) supported by Silvia Puca (DPC), Italy.

Proposal completed, first report available.

Participants: Emmanuel Roulin and Angelo Rinollo (Belgium), Gergana Kozinarova (Bulgaria), Claudia Rachimow and Peter Krahe (Germany), Emanuela Campione (Italy), Rafal Iwanski and Bozena Lapeta (Poland), Ibrahim Sonmez and Ahmet Oztopal (Turkey).

Working Group 2: “Radar data”

Coordinators: Gianfranco Vulpiani (DPC), Italy and Eszter Labo (HMS) Hungary

Proposal completed, first report available.

Participants: Rafal Iwanski (Poland), Emmanuel Roulin and Angelo Rinollo (Belgium) Marian Jurasek, Luboslav Okon, Jan Kanak, Ladislav Meri (Slovakia), Firat Bestepe and Ahmet Oztopal (Turkey)

Working Group 3: “INCA products”

Coordinator: Jan Kanak (SHMU) Slovakia

Proposal completed, first report available.

Participants: Claudia Rachimow and Peter Krahe (Germany), Rafal Iwanski and Bozena Lapeta (Poland), Silvia Puca (Italy)

Working Group 4: “COSMO grid”

Coordinators: Angelo Rinollo (RMI,) Belgium supported by Federico Porcù (University of Ferrara) and Lucio Torrisi (CNMCA) Italy

Proposal completed, First report available in:

ftp://ftp.meteoam.it/hsaf/WP6000/WP6100/precipitation/WG_groups/
software developed, WG CLOSED.

Participants: Emmanuel Roulin, Eszter Labo and Judit Kerenyi

Testing over Belgium successful; procedure already generalized in a way that can be tested and used by all groups and delivered. Testing by other members in progress

Working Group 5: “Geographical error map”

Coordinator: Bozena Lapeta (IMGW) Poland

Proposal completed

Participants: Silvia Puca (Italy), Ibrahim Sonmez and Ahmet Oztopal (Turkey)

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9 Annex 2: Working Group 1 “Rain gauge data”

PROPOSAL

The “ground reference” does not exist. The common validation methodology inside the H-SAF project has been based on the “hydrologist reference” (end-users) constituted mainly by rain gauge and then by radar data.

During the Precipitation Product and Hydrological Validation workshop held in Bratislava the 20-22 of October 2010 the Precipitation Product Validation Group (PPVG) has decided to set up a working group for the definition of the correct verification of satellite precipitation product performances using the rain gauges data available inside the PPVG.

The main aims of this working group are:

- to identify the more suitable techniques to compare rain gauge data with satellite precipitation products;
- to analyse the application of these techniques to the rain gauge available inside the PPV;
- to produce a well referenced documentation on the methodology defined;
- to develop the code to be used in the PPVG for a correct verification of satellite precipitation product performances.

Activities:

First step - collect:

- characteristics (telemetric/..., spatial distribution, temporal resolution, quality check applied, instrument sensitivity and saturation value ... and accuracy) of the rain gauge networks which composes the PPVG (Belgium, Bulgaria, Germany, Poland, Italy, Turkey).

Start Time - End time : December 2010 - January 2011

First Report: 31st of January 2011

Second step- define on the base of published papers and the characteristics of the rain gauge data available inside the PPVG:

- ground data quality check to be applied to all rain gauge data;
- optimal spatial density of rain gauge stations to be representative of the ground precipitation in the view of satellite product comparison;
- optimal time resolution of rain gauge network (15 min, 30 min, 1 h) for a correct comparison with rain rate and cumulated precipitation satellite products;
- raingauges up-scaling techniques vs AMSU-B, SSMI, SEVIRI grids;
- technique for the temporal matching of rain rate and cumulated precipitation satellite products with rain gauge data;

Start Time-End time: January 2011 – July 2011

Second Report: 31st of March 2011

Final Report: 31st of July 2011

Third step- code (possible Matlab) realization for:

- ground data quality check;
- comparison between rain gauge and satellite products.

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Start Time-End time: June 2011- November 2011

Codes delivery and related documentation: 30th of November 2011

Composition of the working group:

Coordinator: Federico Porcù (University of Ferrara) supported by Silvia Puca (DPC), Italy

Participants from Belgium, Bulgaria, Germany, Poland, Italy, Turkey.

FIRST REPORT

Coordinator: Federico Porcù (University of Ferrara) supported by Silvia Puca (DPC), Italy

Participants: Emmanuel Roulin and Angelo Rinollo (Belgium), Gergana Kozinarova (Bulgaria), Claudia Rachimow and Peter Krahe (Germany), Rafal Iwanski and Bozena Lapeta (Poland), Ibrahim Sonmez and Ahmet Oztopal (Turkey), Emanuela Campione (Italy).

Introduction

This document reports on the outcomes of the inventory completed about the raingauges used as “ground reference” within the validation groups. Moreover, some general conclusion is drawn, based on the raingauges validation activities carried on in the last years by the Validation Group of H-SAF. The inventory was structured in three sections, dealing with the instruments used, the operational network and the approach to match gauge data with the satellite estimates. The results are summarized in the next pages.

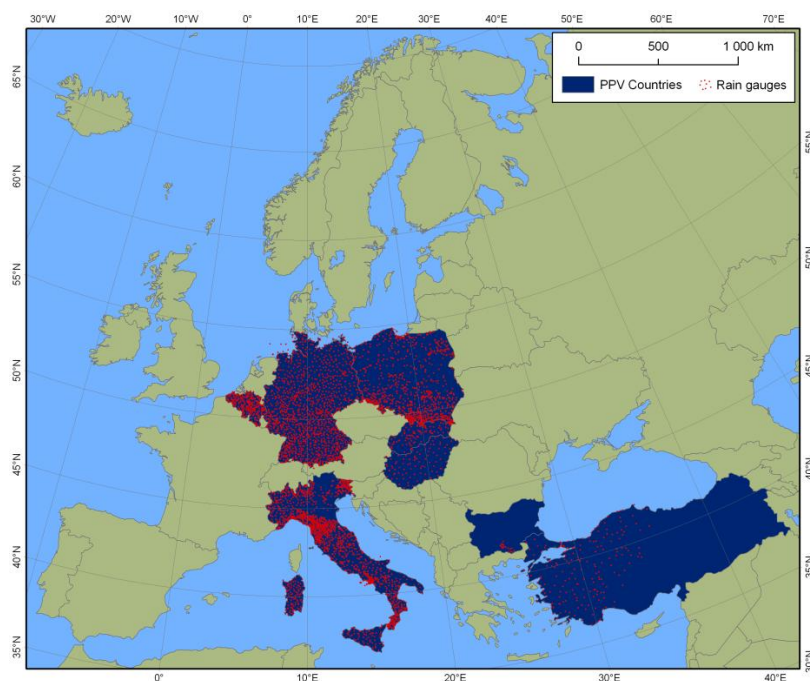


Figure 93 Rain gauge networks in PPVG

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The Instruments

Most of the gauges used in the National networks by the Precipitation Product Validation Group (PPVG) Partners are of the tipping bucket type, which is the most common device used worldwide to have continuous, point-like rainrate measurement. Nevertheless, several source of uncertainty in the measurements are well known but difficult to mitigate. First, very light rainrates (1 mm h^{-1} and less) can be incorrectly estimated due to the long time it takes the rain to fill the bucket (Tokay et al., 2003). On the other side, high rainrates (above 50 mm h^{-1}) are usually underestimated due to the loss of water during the tips of the buckets (Duchon and Biddle, 2010). Drifting wind can also greatly reduce the size of the effective catching area, if rain does not fall vertically, resulting in a rainrate underestimation quantitatively assessed in about 15% for an average event (Duchon and Essenberg, 2001).

Further errors occur in case of solid precipitation (snow or hail), when frozen particles are collected by the funnel but not measured by the buckets, resulting in a temporal shift of the measurements since the melting (and the measure) can take place several hours (or days, depending on the environmental conditions) after the precipitation event (Leitinger et al, 2010, Sugiura et al, 2003). This error can be mitigated by an heating system that melts the particles as soon as are collected by the funnel. All these errors can be mitigated and reduced, but in general not eliminated, by a careful maintenance of the instrument.

A number of *a posteriori* correction strategies have been developed in order to correct precipitation data measured by raingauges, but mainly apply at longer accumulation intervals, daily to monthly (Wagner, 2009)

Country	Minimum detectable rainrate	Maximum detectable rainrate (mm h^{-1})	Heating system (Y/N)	cumulation interval (min)
Belgium	0.1 mm	N/A**	N	60
Bulgaria	0.1 mm	2000	Y	120, 1440
Germany	0.05 mm h^{-1}	3000	Y	60
Italy	0.2 mm	N/A**	Y/N*	60
Poland	0.1 mm	N/A**	Y	10
Turkey	0.2 mm	720	Y	1

Table 50 Summary of the raingauge characteristics

* only 300 out of 1800 gauges are heated

** information not available at the moment: a value about 300 mmh^{-1} can be assumed for tipping bucket raingauges.

Most of these shortcomings could be avoided by using instruments based on different principle or mechanisms. The German network, and a part of the Bulgarian network, as an example, are equipped by precipitation weighting gauges, that allow continuous precipitation (both solid and liquid) measurements with higher accuracy. Other option could be the use of disdrometers, that give more information about the precipitation structure and a more accurate rainrate measure.

In table 53 relevant characteristics of the raingauges used in the different countries are reported.

The networks

The validation work carried on with raingauges uses about 3000 instruments across the 6 Countries, as usual, irregularly distributed over the ground. A key characteristic of such networks is the distance between each raingauge and the closest one, averaged over all the instruments considered in the network and it is a measure of the raingauge density. Instruments number and density are summarized in table 55.

The gauges density ranges between 7 (for Bulgaria, where only 3 river basins are considered) to 27 km (for Turkey). These numbers should be compared with the decorrelation distance for precipitation patterns at mid-latitude. Usually the decorrelation distance is defined as the minimum distance between two measures to get the correlation coefficient (Pearson Coefficient) reduced to e^{-1} . A recent study on the H-SAF hourly data for Italy, shows this decorrelation distance varies from about 10 km in warm months (where small scale convection dominates) to 50 km in cold months, when stratified and long lasting precipitation mostly occur. In figure 97 the value of the linear correlation coefficient is computed between each raingauge pair in the Italian hourly 2009 dataset, as function of the distance between the two gauges.

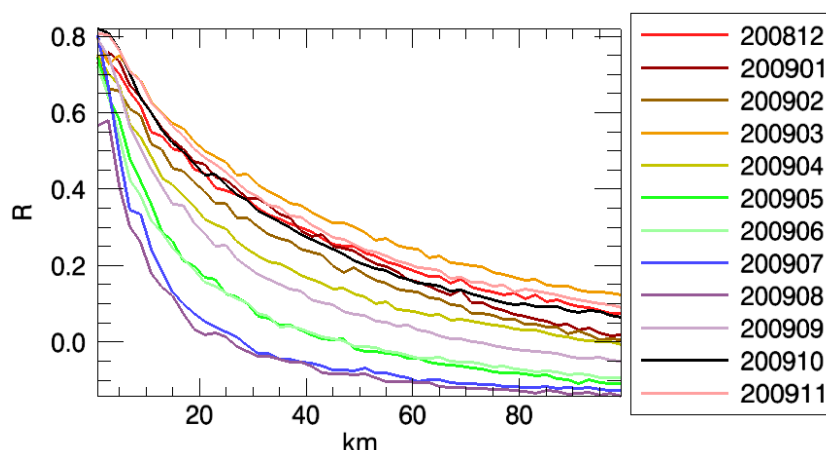


Figure 94 Correlation coefficient between raingauge pairs as function of the distances between the gauges. Colours refer to the months of the year 2009

Assuming these values significant for the other Countries involved in this study, we can conclude the distribution of gauges is capable to resolve the spatial structure of rain patterns only for stratified systems but it is inadequate for small scale convective events.

Country	Total number of gauges *	Average minimum distance (km)
Belgium	89**	11.2
Bulgaria	37***	7
Germany	1300	17
Italy	1800	9.5
Poland	330-475	13.3
Turkey	193****	27

Table 51 Number and density of raingauges within H-SAF validation Group

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* the number of raingauges could vary from day to day due to operational efficiency within a maximum range of 10-15%.

** only in the Wallonia Region

*** only in 3 river basins

**** only covering the western part of Anatolia

Data processing

The partners of the Validation Group have been using a variety of different strategies to treat gauge data and to compare them with satellite estimates. Some are using interpolation algorithms to get spatially continuous rainfall maps, while others process directly the measurements of individual gauges. All the data in the network (except for cold months in Poland) are quality controlled: there is no information about the techniques used, but usually quality control rejects data larger than a given threshold and in case of too high rainrate difference (exceeding given thresholds) among neighbouring gauges and between subsequent measures of the same instrument. Table 52 summarizes the data pre-processing performed in different Countries, while Table 53 and Table 54 report the different matching approaches for H01-H02 and H03-H05, respectively.

As for the temporal matching, the used approaches are rather homogeneous within the Groups: instantaneous measurements are matched with next ground cumulated values over the different available intervals, ranging from 1 minute (Turkey) to 1 hour (Italy, Germany). Cumulated estimates, obviously, are compared to ground measured rain amounts over the same cumulation intervals.

As for spatial matching, different approaches are considered, also taking into account the different spatial structure of the satellite IFOVs. Two basic ideas are pursued: pixel-by-pixel matching or ground measure averaging inside satellite IFOV. The second approach seems to be more convenient, especially when the “large” IFOV of H01 and H02 are concerned. Probably it is mandatory for H02 also take into account that the size of the IFOV changes across the track and could become very large. The first approach, e.g. nearest neighbour, can be more effective for H03 and H05 products.

Country	Type of interpolation	Quality control (Y/N)
Belgium	Barnes over 5x5 km grid	Y
Bulgaria	Co kriging	Y
Germany	Inverse square distance	Y
Italy	Barnes over 5x5 km grid	Y
Poland	No	Y (except cold months)
Turkey	No	Y

Table 52 Data pre-processing strategies

	H01		H02	
Country	Spatial matching	Temporal matching	Spatial matching	Temporal matching
Belgium*	N/A	N/A	N/A	N/A
Bulgaria*	N/A	N/A	N/A	N/A
Germany	matching gauges are searched on a radius of 2.5 km from the IFOV centre	each overpass is compared to the next hourly rain amount	matching gauges are searched on a radius of 2.5 km from the IFOV centre	each overpass is compared to the next hourly rain amount
Italy	mean gauges value over 15x15 km area	each overpass is compared to the	Gaussian-weighted mean gauges value	each overpass is compared to the

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	centred on satellite IFOV	next hourly rain amount	centred on satellite IFOV	next hourly rain amount
Poland	mean gauges value over the IFOV area (rectangular)	each overpass is compared to the next 10-minutes rain amount	mean gauges value over the IFOV area (rectangular)	each overpass is compared to the next 10-minutes rain amount
Turkey	weighted mean (semi variogram) gauges value centred on satellite IFOV	each overpass is compared to the corresponding 1-minute rain rate	weighted mean (semi variogram) gauges value over centred on satellite IFOV	each overpass is compared to the corresponding 1-minute rain rate

Table 53 Matching strategies for comparison with H01 and H02

*Belgium and Bulgaria use raingauges only for cumulated precipitation validation.

	H03		H05	
Country	Spatial matching	Temporal matching	Spatial matching	Temporal matching
Belgium*	N/A	N/A	Nearest neighbour	rain amounts in the same number of hours are compared (24 hours)
Bulgaria*	N/A	N/A	Nearest neighbour	rain amounts in the same number of hours are compared (3 and 24 hours)
Germany	matching gauges are searched on a radius of 2.5 km from the IFOV centre	each overpass is compared to the next hourly rain amount	matching gauges are searched on a radius of 2.5 km from the IFOV centre	rain amounts in the same number of hours are compared (3, 6, 12 and 24 hours).
Italy	Nearest neighbour	the average rainrate over a given hour is compared to next hourly rain amount	Nearest neighbour	rain amounts in the same number of hours are compared (3,6,12 and 24 hours).
Poland	mean gauges value over the pixel area	each overpass is compared to the next 10-minutes rain amount	mean gauges value over the pixel area	rain amounts in the same number of hours are compared (3,6,12 and 24 hours).
Turkey	weighted mean (semi variogram) gauges value centred on satellite IFOV	each overpass is compared to the corresponding 1-minute rain rate	weighted mean (semi variogram) gauges value over centred on satellite IFOV	rain amounts in the same number of hours are compared (3,6,12 and 24 hours).

Table 54 Matching strategies for comparison with H03 and H05

*Belgium and Bulgaria use raingauges only for cumulated precipitation validation.

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Conclusions

After this inventory some conclusion can be drawn.

First, it seems the raingauge networks used in this validation activities are surely appropriated for the validation of cumulated products (1 hour and higher), while for instantaneous estimates the use of hourly cumulated ground measurements surely introduces intrinsic errors in the matching scores, that can be estimated as very large. The validation of instantaneous estimates should be carried on only when gauges cumulation interval is 10 to 15 minutes (as in Poland). Values cumulated over shorter intervals (5 or even one minute, as it is done in Turkey) are affected by large relative errors in cases of low/moderate rainrates.

Different approaches for the estimates matching are considered, and probably could be a good idea to harmonize them among partners. As an example, for H02 a document was delivered by the developers, where the best estimate-ground reference matching strategy was indicated, and also Angelo Rinollo delivered few years ago the code for the Gaussian weight of the antenna pattern in the AMSU/MHS IFOV.

Anyway, different approaches over different Countries are leading to very similar values in the considered skill scores, indicating probably two things: 1) none of the considered approaches can be considered as inadequate and (more important) 2) the differences between ground fields and satellite estimates are so large that different views in the data processing do not results in different numbers.

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10 Annex 3: Working Group 2 “Radar data”

PROPOSAL

Radar rainfall estimation is influenced by several error sources that should be carefully handled and characterized before using it as a reference for ground validation of any satellite-based precipitation products.

The main issues to deal with are:

1. system calibration,
2. contamination by non-meteorological echoes, i.e. ground clutter, sea clutter, “clear air” echoes (birds, insects), W-LAN interferences,
3. partial or total beam shielding,
4. rain path attenuation,
5. wet radome attenuation,
6. range dependent errors (beam broadening, interception of melting snow),
7. contamination by dry or melting hail (“hot spots”),
8. variability of the Raindrop Size Distribution (RSD) and its impact on the adopted inversion techniques

Some of them are typically handled by resorting to standard procedures, some others requires the availability of dual-polarized observations. Generally speaking, there are not correction methodologies applicable worldwide. The knowledge of the radar system and the environmental conditions makes the difference when approaching such problems.

During the Precipitation Product and Hydrological Validation workshop held in Bratislava the 20-22 of October 2010 the Precipitation Product Validation Group (PPVG) has decided to set up a working group on the radar data use in the validation procedures. This WG is not aimed at promoting the acceptance of shared data processing chain.

What really matter for us is the characterization of the error sources through the construction of appropriate “quality maps”.

As requested by the hydro-meteorological community, many operational institutions already provide such information, others are currently working on this task.

The main aims of this WG are:

- to describe the characteristics and generated products of PPVG radar networks;
- to produce a referenced documentation on minimal requirements for certifying the radar products quality, radar rainfall products testing and the procedure for satellite products validation;
- to develop the code to be used in the PPVG for satellite products validation.

Activities:

First step - collect:

- characteristics ((polarization, beam width, maximum range, range, resolution, scan frequency, geographical coordinates, scan strategy[elevations], number of integrated samples, etc.) of the radar networks which composes the PPVG
- adopted processing chain;

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- generated products (including the quality map, if any);

Start Time - End time : December 2010 - February 2011

First Report: 10th of February 2011

Second step- define on the base of published papers and studies of the characteristics of the radar data available inside the PPVG:

- minimal requirements for certifying the radar products quality;
- radar rainfall products testing;
- identification of the test bed scenario for satellite products validation.

Start Time-End time: January 2011 – July 2011

Second Report: 31st of March 2011

Final Report: 31st of July 2011

Third step- code (possible Matlab) realization for:

- comparison between radar data and satellite products on SSML, AMSU-B and SEVIRI satellite grid.

Start Time-End time: June 2011- November 2011

Codes delivery and related documentation: 30th of November 2011

Composition of the working group:

Coordinators: Estezr Labo (HMS) Hungary and Gianfranco Vulpiani (DPC), Italy

Participants: Belgium, Germany, Hungary, Italy, Slovakia, Turkey.

FIRST REPORT AND SECOND REPORT

Reported by Eszter Lábó, Hungarian Meteorological Service

Contributors: Gianfranco Vulpiani (DPC, Italy), Angelo Rinollo (Belgium), Jan Kanak and Luboslav Okon (Slovakia), Firat Bestepe (Turkey), Rafal Iwanski (Poland), Claudia Rachimow (Germany)

Description of tasks:

In the HSAF project, satellite-based precipitation estimations are compared regularly with the radar-derived precipitation fields. However, radar rainfall products are influenced by several error sources that should be carefully analyzed and possibly characterized before using it as a reference for validation purposes.

However, we have to emphasize that the radar data used for validation purposes is not developed by the validation groups themselves. They are developed within specialized radar working teams in many of the countries. Therefore, it should not be the aim of the work of the Radar WG to improve the radar data used; however, it is specifically expected from the current activities to characterize radar data and error sources of the ground data coming from the radar networks of the Precipitation Validation Group (PPVG).

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Main error sources of radar rainfall estimations are listed in the Radar Working Group description document:

1. system calibration,
2. contamination by non-meteorological echoes, i.e. ground clutter, sea clutter, “clear air” echoes (birds, insects), W-LAN interferences,
3. partial or total beam shielding,
4. rain path attenuation,
5. wet radome attenuation,
6. range dependent errors (beam broadening, interception of melting snow),
7. contamination by dry or melting hail (“hot spots”),
8. variability of the Raindrop Size Distribution (RSD) and its impact on the adopted inversion techniques

Moreover, several studies have been on radar quality assessments like *S' alek M, Cheze J-L, Handwerker J, Delobbe L, Uijlenhoet R. 2004.: Radar techniques for identifying precipitation type and estimating quantity of precipitation. COST Action 717, Working Group 1 – A review. Luxembourg, Germany; or Holleman, I., D., Michelson, G. Galli, U. Germann and M. Peura, Quality information for radars and radar data, Technical rapport: 2005, EUMETNET OPERA, OPERA_2005_19, 77p.*

Our main purpose for the first step was to collect characteristics (polarization, beam width, maximum range, range, resolution, scan frequency, geographical coordinates, scan strategy [elevations]...) of the radar networks which composes the PPVG adopted processing chain; and the generated products (including the quality map, if any). This report is intended to present the results of the overview of different radar capacities and instruments in each of the participating countries.

Radar sites and radars:

In the PPVG group, we have all together 54 radars used, or in the plan to be used. Their distribution in the countries is:

- Belgium (1 radar)
- Germany (16 radars – not BfG products)
- Hungary (3 radars)
- Italy (18 radars)
- Slovakia (2 radars)
- Poland (8 radars)
- Turkey (6 radars)

These radars cover wide range of geographical area: from the longitude 5.50562 in Wideumont, Belgium to the most Eastern area with longitude 32°58'15" in Ankara, Turkey; and from the Northern latitude of 54°23'03,17" in Gdańsk, Poland to the latitude of 36°53'24" in Mugla, Turkey and lat 37,462 in Catania, Italy.

Radars are built at different elevations above the sea level. In mountainous countries, they are placed at elevations more than 1000m above sea level; whereas in flat countries like Hungary or Belgium, their height position is not exceeding 400m. This information collected will be useful in the future steps of the Working Group to assess the partial or total beam shielding by mountains in the propagation way of the radar signals.

All radars are C-band radars, working at frequency in C-band, at 5.6 GHz. This is important to know that our radar system is comparable.

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All radars are equipped by Doppler capacity which means that ground clutters can be removed from the radar data measurements effectively; however, not all of them have dual polarization which would be important to correct rain path attenuation.

Scan strategies:

We have explored the scan strategy for each of the radars used. In this matter, all countries have shared their information on the number of elevations, minimum and maximum elevations, scan frequency, maximum nominal range distance, and range resolution.

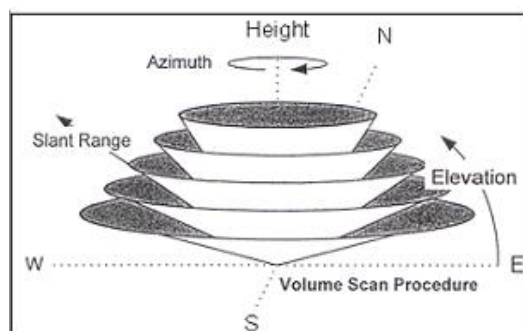


Figure 95 Volume scan procedure

We can conclude that the scan frequency ranges from 5 minutes in Belgium, Germany and Slovakia to 10 minutes in Turkey and Poland, and 15 minutes in Hungary; and varying frequency for Italian radars. The number of elevation stays between 4 and 15, in average around 10.

The range distance used is 240 km in general. But in some places in Italy, and for the Turkish radars, the maximum range distance used is 120 km, or even less, e.g. 80 km.

Range resolution is 250 m in Belgium, 250, 340, 225, and sometimes 500 m for the Italian radars, 500 m for one of the Hungarian radars, and 250m for the other two, Polish radars can work with 125 m and 250 m resolution, and in Turkey it is 250 m for all the radars.

All in all, the scan strategies within the PPVG countries are well-balanced and similar to each other; though they vary from one radar to the other, even within countries.

All radars are regularly maintained and calibrated, which is a good indicator of the continuous supervision of quality of radar data, and the important element to sustain radar data quality.

Overview of radar products used for validation in the HSAF project:

The Table at the end of the report is provided to summarize the available products generated from radar measurements, and the processing chain used to generate them. Finally, the list of the radar products used for the validation work is included in the last row.

Radar rainfall products are obtained after processing the measured radar reflectivity at different elevations of the radar scan strategy. After each elevation, the PPI (Plan Position Indicator) products and the CAPPI (Constant Altitude PPI) products are calculated. PPI is the measurement of the radar antenna rotating 360 degrees around the radar site at a fixed elevation angle. CAPPI products are derived from this, by taking into account the radar displays which give a horizontal cross-section of data at constant altitude. The CAPPI is composed of data from several different angles that have measured reflectivity at the requested height of CAPPI product.

The PPVG group uses mostly CAPPI products for calculation of rainfall intensities; except for Hungary, which uses the CMAX data (maximum radar reflectivity in each pixel column among all of the radar

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elevations) for deriving rainfall intensities. However, the rest of the countries have also chosen different elevation angles for the CAPPI product which provides the basis for rain rate estimations. Additionally, we have to say that the countries apply different techniques of composition of radar data that were not specified in this questionnaire. The composition technique is important in areas which are covered by more than one radar measurements. Also, the projection applied is varying from one country to the other.

To sum up, the radar products used are not harmonized, different techniques are applied. However, each of them is capable to grasp rainfall and to estimate rainfall intensity.

As for the accumulated products, we see that Belgium uses 24-hourly accumulations, with rain gauge correction, Italy uses 3, 6, 12, 24h accumulations without gauge-correction; in Hungary 3, 6, 12, 24h data is used, but only the 12h and 24 hourly accumulations are corrected by rain gauges, in Poland and Slovakia no rain gauge correction is applied. Poland has only 6, and 24 hourly data. Turkey has 3,6,12,24h data, and applies rain gauge correction for 1 hourly data. It is important to note that techniques used for accumulation are numerous, even within the same country they can differ from one accumulation period to another. E.g. in Hungary, the 3,6h accumulations are derived from summing up the interpolation of the 15minute-frequent measurements into 1 minute-intervals; whereas the 12, and 24 h accumulations are summed up from 15 minute measurements, but corrected with rain gauge data.

All above implies that more probably the quality and error of rainfall and rain rate accumulations is differing from one country to another; and cannot be homogeneously characterized.

Conclusion of the questionnaire:

Maintenance

All the contributors declared the system are kept in a relatively good status.

Correction factors for error elimination:

These correction factors are diverse in the countries, not homogeneous distribution of correction methods:

- all contributors compensate for non-meteorological echoes (Clutter)
- RLAN interferences implemented in Hungary, Slovakia- in development.
- Poland and Slovakia correct attenuation. In other countries, it is not accounted for.
- Some of the countries are testing new procedures for dealing with VPR (Italy) and Partial Beam Blockage, PBB effects. VPR (Vertical Profile of Reflectivity) used in Turkey.

This means that the corresponding rainfall estimates are diverse, and the estimation of their errors cannot be homogenized.

However, each country can provide useful information of the error structure of its rainfall products based on its own resources: e.g. if they have already defined Quality Indicators, or estimations of errors based on studies of comparison of radar and rain gauge data in the country itself.

In the future, possible separation of reliable and quasi-reliable radar fields would be possible. Separation would be based on radar site/geographical areas/event type/radar products. Selected cases will be suitable enough to be used as a reference for the H-SAF products validation.

Satellite product testing will be carried out in areas with higher reliability. Statistical results will be

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evaluated and compared to previous data. As such, the accuracy of statistical results of PPVG with radar data as ground reference will be able to be established.

References

References have been collected from each country describing radar data, radar data quality, and radar data quality estimation techniques. This list will be the baseline for further work of the Radar WG.

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Poland

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	BELGIUM	ITALY	HUNGARY
List of Available Products.	Rain rate 240 Km; rain rate 120 Km; velocity (120 Km); MAX (240 Km); VVP2 Windprofiles; Hail Probability; Hail Probability 24h Overview; 1, 3, 24 Hr Rainrate accumulation;		CMAX, PPI, CAPPI(2.5 km), VIL, ETops, Base, HailProbability
Is any quality map available?	NO	YES	NO
Processing chain	Clutter removal (time-domain Doppler filtering and static clutter map); Z-R: a=200, b=1.6	Clutter suppression by Fuzzy Logic scheme using Clutter map, Velocity, Texture. Z-R: a=200, b=1. VPR correction under testing.	RLAN(wifi) filter; Clutter removal; attenuation correction + beam blocking correction => next Year (2012) VPR => No Z-R: a=200, b=1.6
Description of instantaneous radar product used in HSAF Validation Activities	PCAPPI-1500m Cartesian grid, 600m resolution	Nationale composite: CAPPI 2 km, CAPPI 3 km, CAPPI 5 km, VMI, SRI Projection: Mercator Resolution: 1 km Threshold: No	National composite, (CMAX) Projection: stereographic (S60) Resolution: 2 km Threshold: 7dBZ No rain gauge correction
Description of accumulated radar product used in HSAF Validation	24-h accumulation with range-dependent gauge adjustment, Cartesian grid, 600m resolution	Acc. periods: 1, 3, 6, 12, 24h Projection: Mercator Resolution: 1 km Threshold: No	Acc.periods: 3,6,12,24h National composite, (CMAX) Projection:

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Activities		No rain gauge correction	stereographic (S60) Resolution: 2 km Threshold: 7dBZ Rain gauge correction applied for 12, 24 hourly data
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	POLAND	SLOVAKIA	TURKEY
List of Available Products.	PPI, PCAPPI, RHI, MAX, EHT, SRI, PAC, VIL, VVP, HWIND, VSHEAR, HSHEAR, LTB, SWI, MESO, WRN. List of non-operational products: LMR, CMAX, UWT, VAD, SHEAR, SWI, MESO, ZHAIL, RTR, CTR, WRN.	CAPPI 2 km, Etops, PPI 0.2, Base, Cmax, Hmax, VIL, Precip. Intensity, 1h-, 3h-, 6h-, 24h-acc. precip., 1h-acc. SRI 1km, 2km agl	MAX, PPI, CAPPI, VIL, ETOPS, EBASE, RAIN Accumulation (1,3,6,12,24h)
Processing chain	Doppler method clutter removal; attenuation correction - yes; VPR => No Z-R: a=200, b=1.6	Clutter filtering: frequency-domain IIR filter; Atmospheric attenuation correction; Z-R: a=200, b=1.6 RLAN filtering in development	Clutter Removal, VPR Correction, Z-R: A=200 b=1.6
Is any quality map available?	NO, in development	NO	NO
Description of instantaneous radar product used in HSAF Validation Activities	National composite, (SRI); Projection: azimuthal equidistant (standard: ellipsoid); Resolution: 1 km; Threshold: 5 dBZ; No rain gauge correction.	National composite CAPPI 2 km Projection: Mercator Resolution: 1 km Threshold: -31.5 dBZ No rain gauge correction	CAPPI, Projection: Azimuthal Equidistant Resolution: 250 m Threshold: ? Rain Gauge Correction (with limited number of gauges)
Description of accumulated radar product used in HSAF Validation Activities	Acc. Periods: 1, 6, 24h; National composite (PAC), Projection: azimuthal equidistant (standard: ellipsoid); Resolution: 1 km; Threshold: 0,1 mm; No rain gauge correction	Acc. periods: 3, 6, 12, 24h National composite CAPPI 2 km Projection: Mercator Resolution: 1 km Threshold: -31.5 dBZ No rain gauge correction	Acc.periods: 1,3,6,12,24h Projection: Azimuthal Equidistant Resolution: 250 m Threshold: ? Rain gauge correction applied for 1h Rain Acc.

Table 55 List of products used

11 Annex 4: Study on evaluation of radar measurements quality indicator with regards to terrain visibility

Ján Kaňák, Ľuboslav Okon, SHMÚ

For validation of H-SAF precipitation products it is necessary to know errors distribution of used ground reference. In this case precipitation intensity or accumulated precipitation measured by SHMÚ radar network is considered as a ground reference. To find distribution of errors in radar range next steps must be done:

- simulations of terrain visibility by radar network using 90m digital terrain model
- statistical comparison of radar data against independent rain gauge data measurements
- derivation of dependence (regression equation) describing the errors distribution in radar range with regard to terrain visibility, based on rain gauge and radar data statistical evaluation
- computation of error distribution maps using regression equation and terrain visibility

24-hour cumulated precipitation measurements from 68 automatic precipitation stations from the period 1 May 2010 – 30 September 2010 were coupled with radar based data. Distribution of gauges according their elevation above the sea level is shown in next figure.

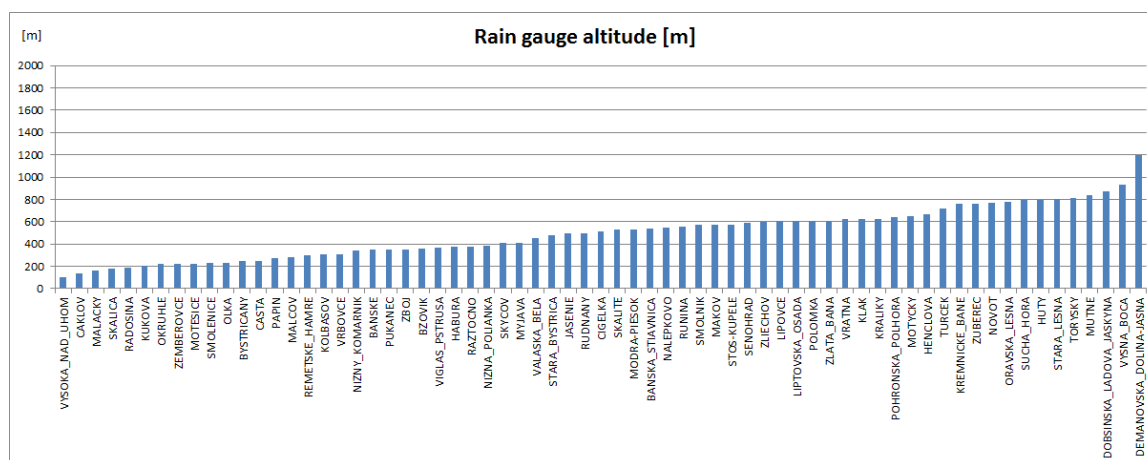


Figure 96 Distribution of rain gauges according their altitude above the sea level

To simulate terrain visibility by meteorological radars Shuttle Radar Topography Mission (SRTM) data were used as an input into radar horizon modeling software developed in SHMÚ. Details about SRTM can be found at http://en.wikipedia.org/wiki/Shuttle_Radar_Topography_Mission or directly at <http://www2.jpl.nasa.gov/srtm/>. SRTM model provides specific data set of terrain elevations in 90 m horizontal resolution in the whole HSAF area where HSAF validation by radars is performed. Modelling software parameters were adjusted for single radar according real scanning strategy:

Radar Site	Malý Javorník	Kojšovská hoľa
Tower height	25m	25m
Range	1200pixels/240km	1200pixels/200km
Resulted resolution	200m/pixel	166,67m/pixel
Min elevation	-0,1 deg	-0,8 deg
Refraction	1,3 (standard atmosphere)	1,3 (standard atmosphere)
Elevation step	0,01 deg	0,01 deg

Azimuth step	1/40 deg	1/40 deg
Layer minimum	500 m	500 m
Layer maximum	1000 m	1000 m
Max displayed height	5000 m	5000 m

Radar horizon model provides the following outputs (maps of radar range):

- terrain elevation
- minimum visible height above the sea level
- minimum visible height above the surface
- Layer visibility (defined by minimum and maximum levels)

Results of the horizon model for Malý Javorník and Kojšovská hoľa radar sites are shown on Figure 97. To evaluate the radar visibility over the whole radar network composite picture of minimum visible height above the surface was created and is shown on Figure 98.

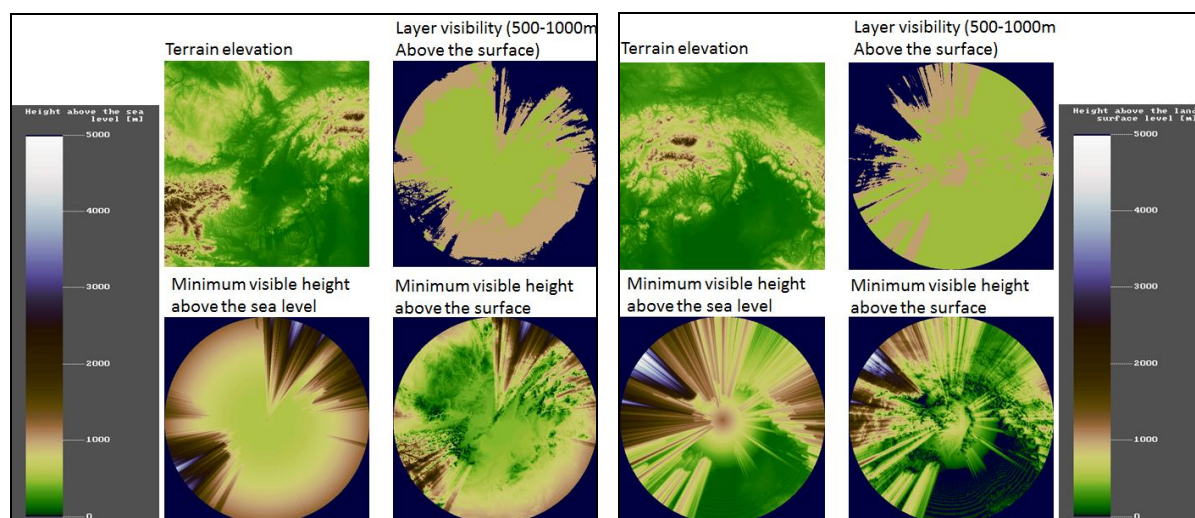
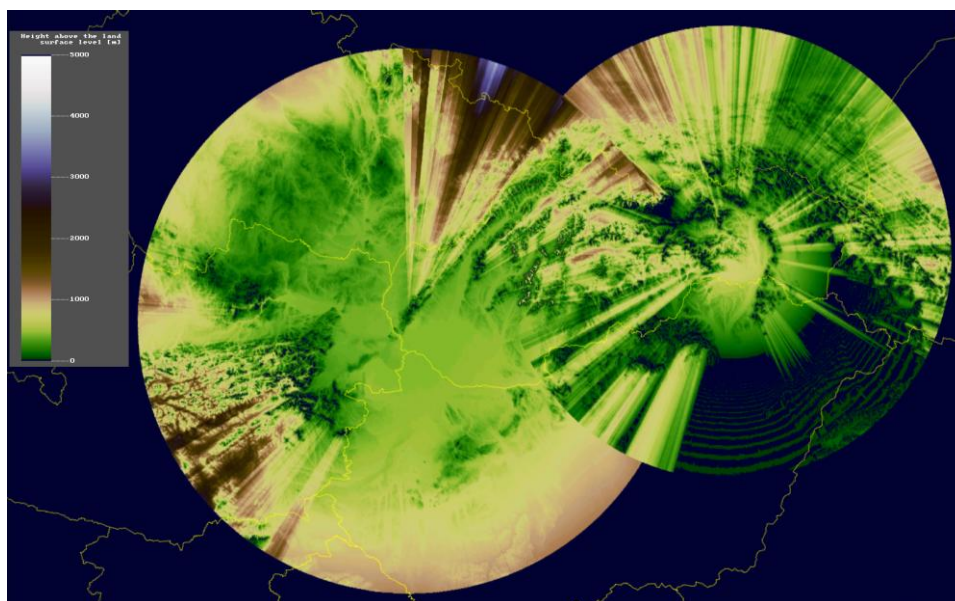


Figure 97 Radar horizon model output for Malý Javorník (left) and Kojšovská hoľa (right) radar sites

Colour scale on left corresponds to the products showing heights above the sea level, scale on right corresponds to the products showing heights above the surface.



**Figure 98 Composite picture of minimum visible height above the surface over the whole radar network.
Compositing algorithm selects the minimum value from both radar sites**

In next step minimum visible heights above the rain gauge stations were derived from the composite picture. Distribution of rain gauges according to the minimum visible height of radar beam is shown on next figure. It should be noted that while radar beam elevation is reaching 3000m in northern central part of composite picture, no rain gauge station was available in this region. Only rain gauge stations with minimum visible heights in the interval (0m; 1100m) were available in this study.

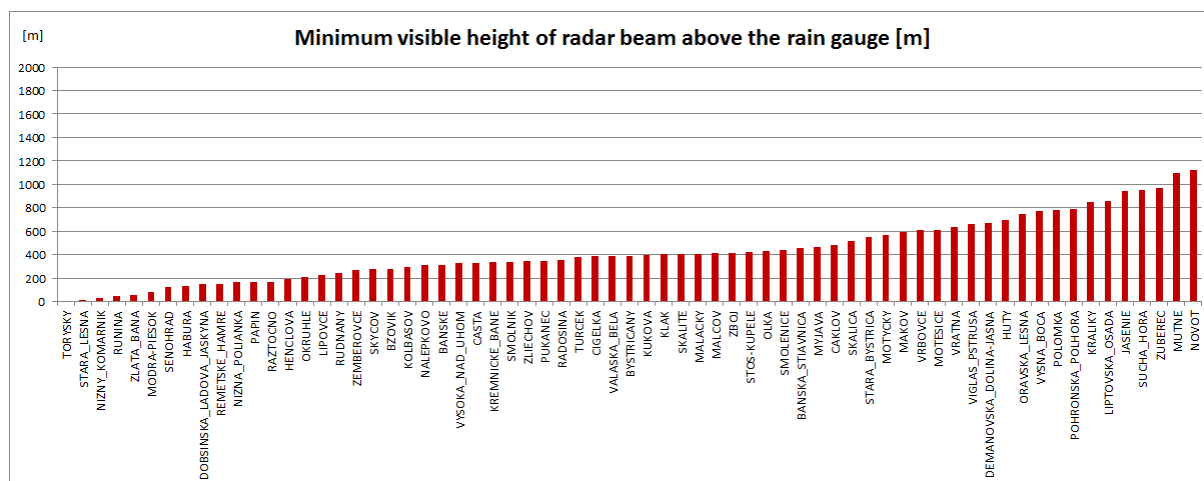


Figure 99 Distribution of rain gauges according to the minimum visible height of radar beam

To understand dependence of radar precipitation estimations and rain gauge values on gauge altitude above the sea and on radar beam altitude the scatterplots of $\log(R/G)$ versus station altitude shown on next figure and $\log(R/G)$ versus radar beam altitude shown on Figure 101 were generated. Quite wide scattering can be observed but quadratic polynomial trend lines indicate that in general radar underestimates precipitation and this underestimation is proportional to station elevation and radar beam elevation.

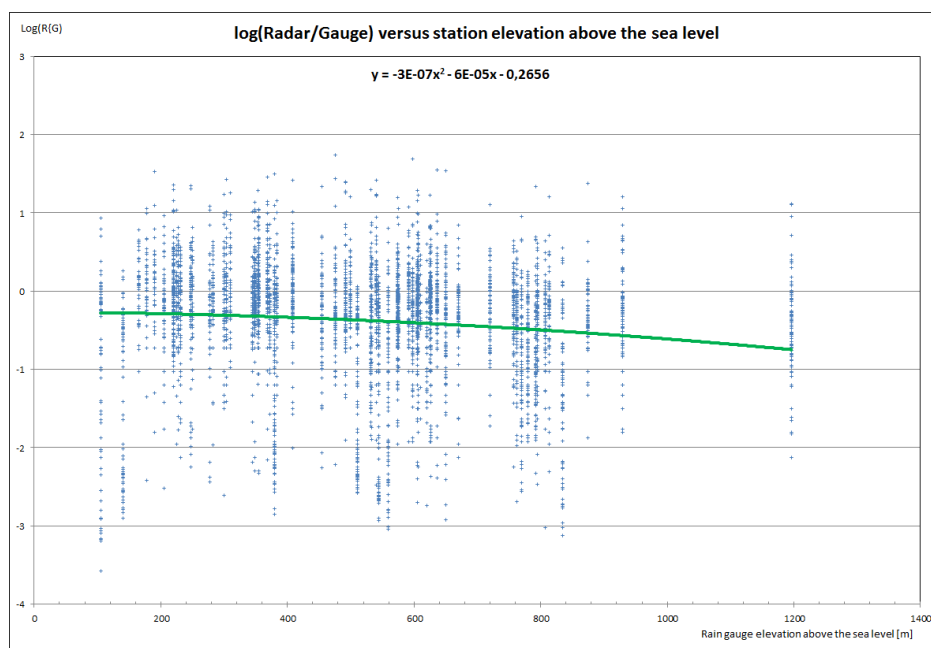


Figure 100 Scatterplot of log(R/G) versus station altitude shows general underestimation of precipitation by radar

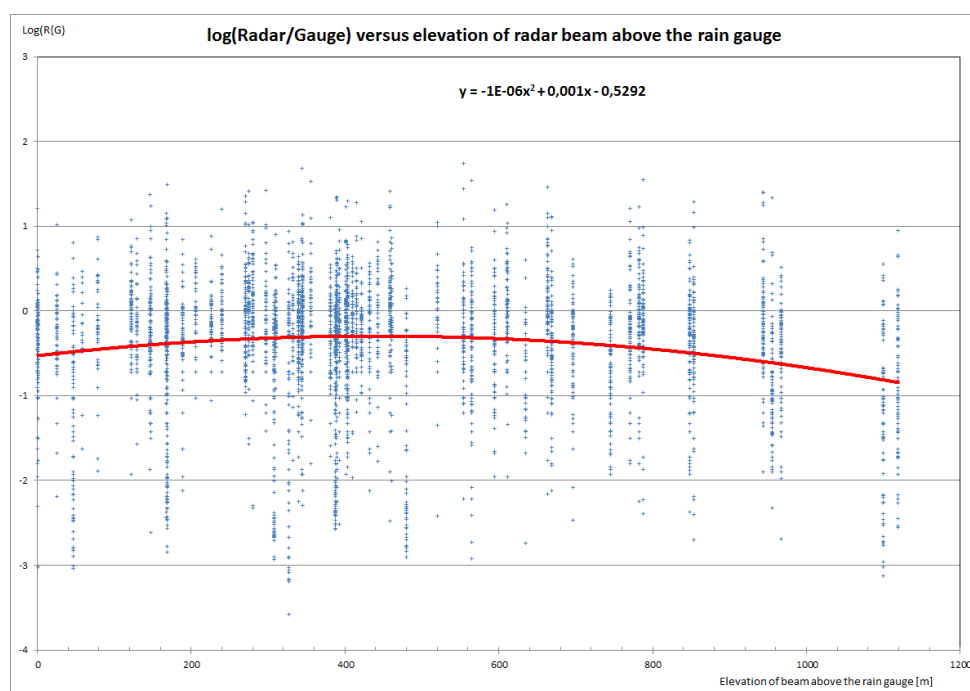


Figure 101 Scatterplot of log(R/G) versus radar beam altitude shows increased underestimation of radar for high and close to zero radar beam elevations

Polynomial trend line on the Figure 98 differs from trend line of Figure 101. While in case of rain gauge altitudes the lowest underestimation by radar can be observed for the lowest rain gauge altitudes, in case of radar beam altitudes the lowest underestimation by radar is observed for radar beam elevation about 500m. Stronger underestimation for rain gauges with close to zero radar beam elevation can be explained by partial signal blocking by terrain obstacles. These are the cases when rain gauge station is close to the top of terrain obstacle.

Finally set of statistical parameters for each single rain gauge station was computed: mean error, standard deviation, mean absolute error, multiplicative bias, correlation coefficient, RMSE and relative RMSE. Relative RMSE and Mean Error were selected to be specified for radar precipitation measurement over the whole radar range. For this purpose quadratic or linear polynomial trend lines were created as is shown on next figure.

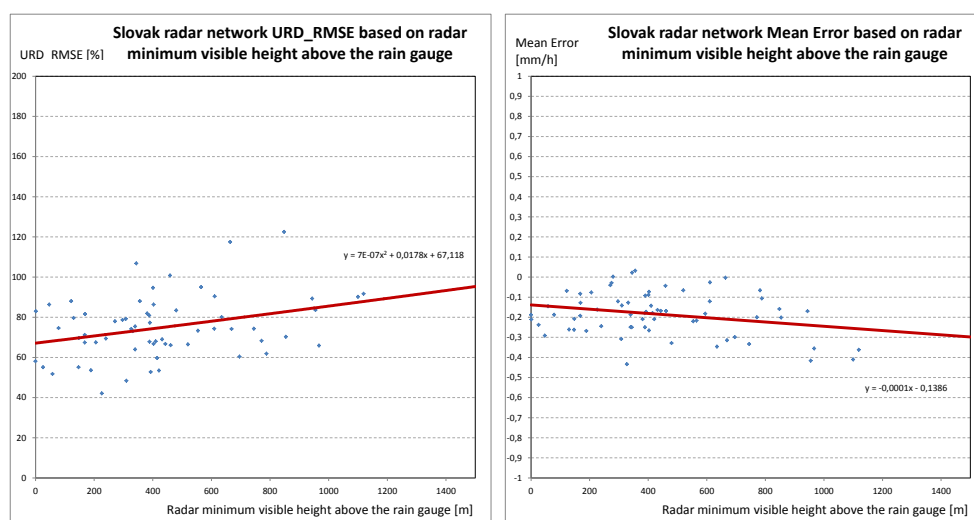


Figure 102 Relative RMSE (left) and Mean Error (right) computed independently for each rain gauge station in radar range and corresponding trend lines extrapolated for beam elevation up to 1500m

Relative RMSE and Mean Error can be specified for each pixel of radar network composite map using regression equations which describe dependence on minimum radar beam elevation above the surface. This can be considered as quality indicator maps of radar measurements with regard to terrain visibility by current radar network of SHMÚ as is shown in next two figures.

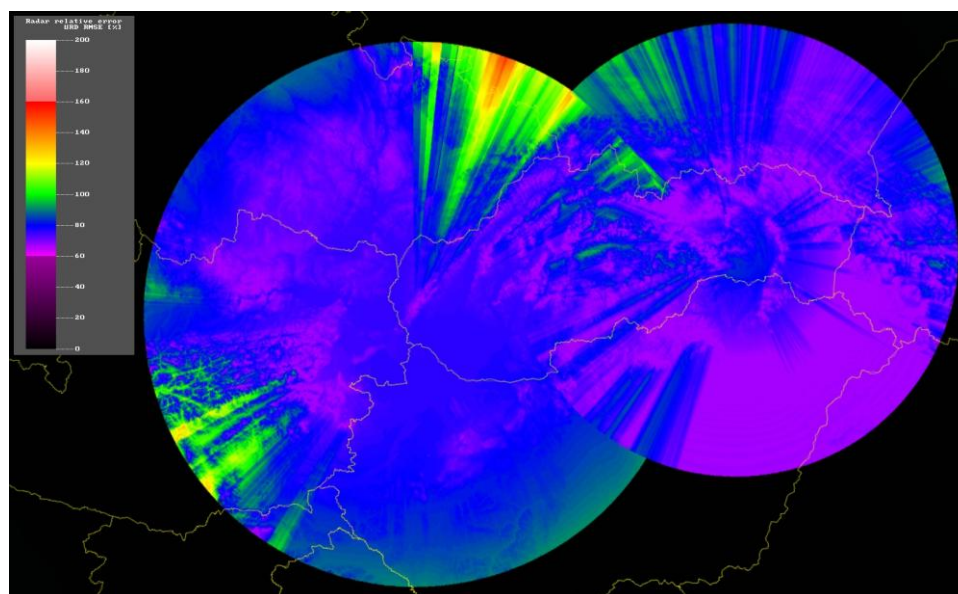


Figure 103 Final relative root mean square error map of radar measurements with regard to terrain visibility by current radar network of SHMÚ

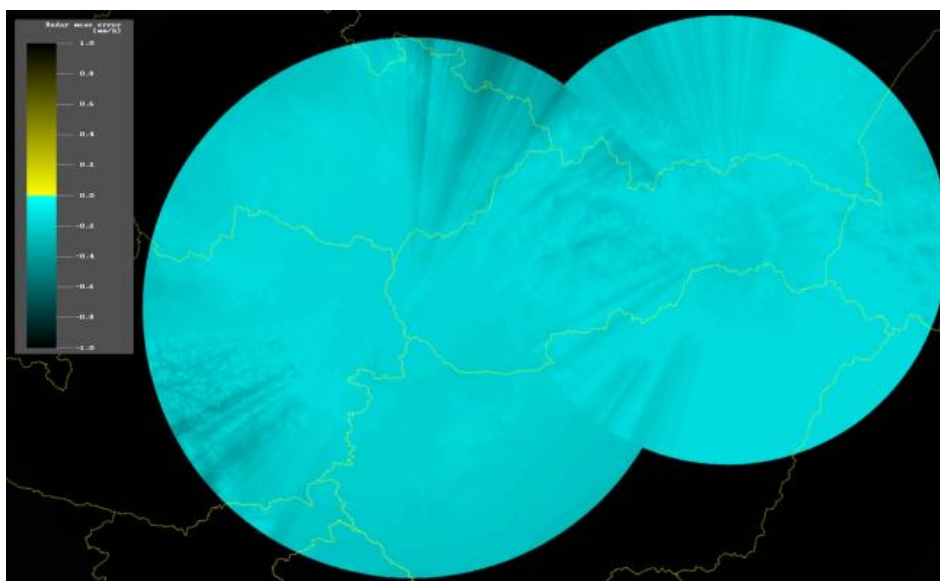


Figure 104 Final mean error map of radar measurements with regard to terrain visibility by current radar network of SHMÚ. General underestimation of precipitation by radars is observed

Conclusions

Considering the fact that reference precision of rain gauges used in this study is not sufficient and they do not reflect real ground reference of precipitation fields, obtained results can be considered as a ceiling guess of radar measurements quality indicator with regards to terrain visibility. This result includes also the error of rain gauge network itself.

Also averaged mean error, root mean square error and relative root mean square error values were computed for 68 rain gauge stations located in radar horizons:

Averaged mean error: -0,184 mm/h for instantaneous or -4,42 mm for 24 hours cumulated precipitation

Averaged RMSE: 0,395 mm/h for instantaneous or 9,48 mm for 24 hours cumulated precipitation

Averaged URD_RMSE: 69,3 % for 24 hours cumulated precipitation

It should be noted that all computations in this study were based on 24 hour cumulated precipitation and only re-calculated into instantaneous precipitation. Values of errors in case of instantaneous precipitation can be significantly higher because of short time spacing. Therefore it is planned in the future to calculate errors of radar measurements separately for instantaneous and for cumulated precipitation.

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12 Annex 5: Working Group 3 “INCA Precipitation for PPV”

PROPOSAL

The “precipitation ground reference” can be only based on certain conceptual models. The validation activity inside H-SAF project is composed by hydrological and product validations. Precipitation captured by river basin is transformed by set of processes into the river discharge. This set of processes is described by hydrological discharge models and by river discharges measured by hydrological equipments. Moreover validation of precipitation products cannot be overcasted by only an evaluation of methods describing transformation of precipitation into river discharge. For this reason a common validation methodology to compare satellite precipitation estimations with ground data (radar and rain gauge) inside the H-SAF project has been defined. The validation of precipitation field is a difficult task and a continuous study of possible validation methodology improvement is necessary. The Precipitation Product Validation Group decided during the last internal workshop held in Bratislava from 20-22 of October 2010 to set up various working groups for the investigation of possible improvement of the validation methodology. One of these working groups is “INCA precipitation for PPV” group.

Definition of INCA Precipitation Products: INCA system consists of computational modules which enable us to integrate various sets of precipitation data sources – raingauge network, radar network, NWP models outputs and climatological standards into common precipitation product, which can describe well the areal instantaneous and cumulated precipitation fields.

The main aims of INCA precipitation for PPV group are:

- to identify the INCA precipitation products which can be considered as “precipitation ground reference” and used for validation of H-SAF products, both instantaneous and cumulated precipitation fields
- to identify the techniques of comparison the INCA precipitation products with satellite precipitation products;
- to develop the code to be used in the PPVG for a correct verification of satellite precipitation product performances with INCA;
- to produce a well referenced documentation on the methodology defined;
- to perform H-SAF products validation based on these techniques and INCA precipitation products;

Activities:

First step:

- identify experts/contact persons inside INCA community which can provide information on INCA system, like methods of precipitation data integration, product formats, data coverage, products availability and quality;
- collect and study INCA methods and products, and to consider how these methods meet requirements of H-SAF precipitation products validation;

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- compare precipitation field reconstructed using radar data, raingauges data, and INCA products for some case studies;

Start Time-End time: December 2010 – March 2011

First Report: 31st of March 2011

Second step:

- develop common upscaling software tools for proper upscaling of identified INCA products into native H-SAF product's grids;
- select extreme weather events and make case studies on comparison the INCA and H-SAF relevant precipitation products;
- in case of positive case studies to perform batch validation of H-SAF products and provide standard validation statistical outputs (continuous and multicategorical statistics);

Start Time-End time: April 2011 – November 2011

Second Report: 31st of July 2011

Final Report: 30th of November 2011

Composition of the working group:

Coordinator: Jan Kanak (SHMU)

Participants: members of H-SAF consortium, which are in parallel involved in development of INCA products – Belgium, Germany, Italy, Hungary, Slovakia, Turkey.

FIRST REPORT

Coordinator: Ján Kaňák (Slovakia)

Participants: Claudia Rachimow and Peter Krahe (Germany), Ľuboslav Okon, Jozef Vivoda and Michal Neštiak (Slovakia), Rafal Iwanski and Bozena Lapeta (Poland), Silvia Puca (Italy)

Introduction

This report presents outcomes of the initial activities performed within the “INCA products” working group. In the first part information on the INCA or INCA-like systems available in the participating countries are summarized. The second part of the report presents several case studies comparing precipitation fields estimated by radars, raingauges and the INCA system. Results of the statistical comparison of the PR-OBS-2 product with the different reference fields for selected precipitation events are also included.

Summary of the INCA system survey

As a first step of survey experts/contact persons were identified inside the INCA group community as listed in the following table.

Country	Contact person/expert	E-mail address
Slovakia	Jozef Vivoda	jozef.vivoda@shmu.sk
	Michal Neštiak	michal.nestiak@shmu.sk
Poland	Rafal Iwanski	rafal.iwanski@imgw.pl
Germany	Claudia Rachimow	rachimow@bafg.de
	Peter Krahe	krahe@bafg.de

Table 56 List of contact persons

Within the participating countries there are two types of systems providing precipitation analyses usable for H-SAF validation: **INCA** (developed by ZAMG, Austria) and **RADOLAN** (DWD, Germany). The INCA system is currently under development as INCA-CE (Central Europe) and is used in pre-operational mode in Slovakia and Poland. The RADOLAN system is used in Germany operationally and is already utilized for the H-SAF products validation.



Figure 105 Coverage of Europe by the INCA and RADOLAN systems

Here below a brief description of the INCA and RADOLAN systems follows. More information on both systems can be found in the documentation which is available on the H-SAF ftp server:
/hsaf/WP6000/precipitation/WG_groups/WG3-inca/documentation

Brief description of the INCA system

The INCA (Integrated Nowcasting through Comprehensive Analysis) analysis and nowcasting system is being developed primarily as a means of providing improved numerical forecast products in the nowcasting and very short range forecasting. It should integrate, as far as possible, all available data sources and use them to construct physically consistent analyses of atmospheric fields. Among the input data sources belong:

- NWP model outputs in general (P, T, H, clouds ...)
- Surface station observations (T, precipitation)
- Radar measurements (reflectivity, currently 2-d, 3-d in development)
- Satellite data (CLM, Cloud type, in development for use in precipitation analysis)

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- Elevation data (high resolution DTM, indication of flat and mountainous terrain, slopes, ridges, peaks)

The INCA system provides:

- **High-resolution analyses** – interest of validation WG-3
- Nowcasts
- Improved forecasts

of the following variables:

- Temperature (3-d field)
- Humidity (3-d)
- Wind (3-d)
- **Precipitation (2-d)** – interest of validation WG-3
- Cloudiness (2-d)
- Global radiation (2-d)

The INCA precipitation analysis is a combination of station data interpolation including elevation effects, and radar data. It is designed to combine the strengths of both observation types, the accuracy of the point measurements and the spatial structure of the radar field. The radar can detect precipitating cells that do not hit a station. Station interpolation can provide a precipitation analysis in areas not accessible to the radar beam.

The precipitation analysis consists of the following steps:

- i. Interpolation of station data into regular INCA grid (1x1 km) based on distance weighting (only nearest 8 stations are taken into account to reduce bull-eyes effect)
- ii. Climatological scaling of radar data by means of monthly precipitation totals of raingauge to radar ratio (partial elimination of the range dependence and orographical shielding)
- iii. Re-scaling of radar data using the latest rain gauge observations
- iv. Final combination of re-scaled radar and interpolated rain gauge data
- v. Elevation dependence and orographic seeding precipitation

In the final precipitation field the raingauge observations are reproduced at the raingauge station locations within the limits of resolution. Between the stations, the weight of the radar information becomes larger the better the radar captures the precipitation climatologically.

Important factor affecting the final precipitation analysis is accuracy and reliability of the raingauge stations. In order to eliminate the influence of raingauge stations providing evidently erroneous data, the SHMÚ is developing the blacklisting technique which temporarily excludes such stations from the analysis. Currently, the stations can be put into the blacklist only manually but development of the automated blacklisting is expected in near future.

Brief description of the RADOLAN system

RADOLAN is a routine method for the online adjustment of radar precipitation data by means of automatic surface precipitation stations (ombrometers) which has started on a project base at DWD in

1997. Since June 2005, areal, spatial and temporal high-resolution, quantitative precipitation data are derived from online adjusted radar measurements in real-time production for Germany.

The data base for the radar online adjustment is the operational weather radar network of DWD with 16 C-band sites on the one hand, and the joined precipitation network of DWD and the federal states with automatically downloadable ombrometer data on the other hand. In the course of this, the precipitation scan with five-minute radar precipitation data and a maximum range of 125 km radius around the respective site is used for the quantitative precipitation analyses. Currently, from more than 1000 ombrometer station (approx. 450 synoptic stations AMDA I/II-and AMDA III/S-of DWD; approx. 400 automatic precipitation stations AMDA III/N of DWD; approx. 150 stations of the densification measurement network of the federal states) the hourly measured precipitation amount is used for the adjustment procedure.

In advance of the actual adjustment different preprocessing steps of the quantitative radar precipitation data are performed. These steps, partly already integrated in the offline adjustment procedure, contain the orographic shading correction, the refined Z-R relation, the quantitative composite generation for Germany, the statistical suppression of clutter, the gradient smoothing and the pre-adjustment. Further improvements of these procedures are being developed.

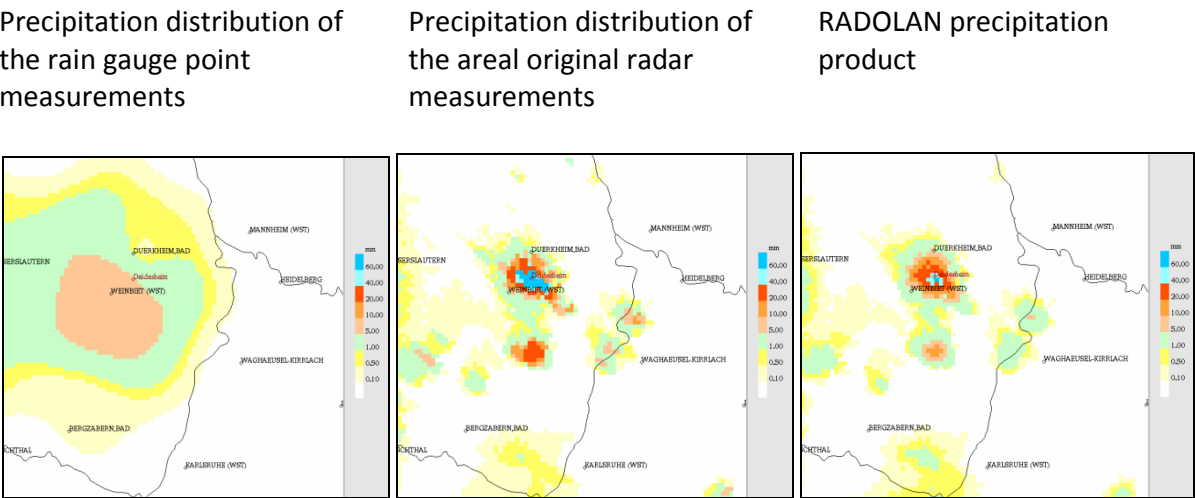


Figure 106 Procedure of the RADOLAN online adjustment (hourly precipitation amount on 7 August 2004 13:50 UTC)

In order to collect more detailed information about both types of systems a questionnaire was elaborated and completed by Slovakia, Poland and Germany. The questionnaire provided details such as geographical coverage (see Figure 105) input data inventory or availability of different instantaneous and cumulated precipitation products. The final version of the questionnaire is shown in the next table and is also available on the H-SAF ftp server: /hsaf/WP6000/precipitation/WG_groups/WG3-inca/questionnaire.

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Group of information	Item	GERMANY	POLAND	SLOVAKIA domain1	SLOVAKIA domain2
Availability of documentation for INCA or similar (German) system [Yes/No]	If possible please attach link or documentation	Dokumentation received during Helsinki validation meeting	Documentation available from ZAMG	Documentation available from ZAMG	Documentation should be issued in future
Definition of geographical area covered by INCA or similar (in Germany) system	Grid size in pixels	900x900	741x651	501x301	1193x951
	Min longitude	3.5943 E	13.82 E	15.99231 E	8,9953784943 E
	Max longitude	15.71245 E	25.334 E	23.09630 E	25,9996967316 E
	Min latitude	46.95719 N	48.728 N	47.13585 N	45,0027313232 N
	Max latitude	54.73662 N	55.029 N	50.14841 N	53,000579834 N
	Space resolution	1 km	1 km	1 km	1 km
Input data	Number of radars in network	Composite of 16 national radars	Composite of 8 national radars	Composite of 2 national radars	Composite of 5 international radars
	Number of precipitation stations	1300	475 (Poland only)	397 (SHMU, CHMI, ZAMG, IMWM)	TBD
	Blacklist for precipitation stations [Yes/No]	?	Yes	Yes	Yes
Density of raingauge stations	Map of density of precipitation stations [Yes/No]	?	TBD	TBD	TBD
Output data	Instantaneous precipitation based only on raingauge network, time resolution, timelines	5 min	No	Yes, 15 min	Yes, 15 minute
	Instantaneous precipitation based only on radar network, time resolution, timelines	5 min	No	Yes, 5 minute	Yes, 5 minute
	Instantaneous precipitation based on combined raingauge and radar network, time resolution, timelines	5 min	Yes, 10 minutes	Yes, 5 minutes	Yes, 5 minutes
	Cumulative precipitation based only on raingauge network, time intervals, timelines	5 min, 1,3,6,12,18,24 hours	No	Yes, min 5 min, available 1,3,6,12,24 hours	Yes, min 5 min, available 1,3,6,12,24 hours
	Cumulative precipitation based only on radar network, time intervals, timelines	5 min, 1,3,6,12,18,24 hours	No	Yes, min 5 min, available 1,3,6,12,24 hours	Yes, min 5 min, available 1,3,6,12,24 hours
	Cumulative precipitation based on combined raingauge and radar network, time intervals, timelines	5 min, 1,3,6,12,18,24 hours	Yes, min 10 minutes, available in future	Yes, min 5 min, available 1,3,6,12,24 hours	Yes, min 5 min, available 1,3,6,12,24 hours
Dates for selected case studies	Case 1	will be set	No	29.3.2009	
	Case 2		No	1.-3.6.2010	
	Case 3		No	20.6.2010	
	Case 4		No	15.-16.8.2010	
	Case 5		No		
Availability of own software for upscaling INCA data into native satellite grid	H01	yes	No	No	No
	H02	yes	No	No	No
	H03	yes	No	No	No
	H04	no	No	No	No
	H05	yes	No	No	No
	H06	yes	No	No	No

Table 57 Questionnaire

Case studies

Several case studies comparing the INCA analyses with their source precipitation fields from radars and raingauges and with selected H-SAF products have been elaborated at SHMÚ. The precipitation fields from individual observations have been compared visually but have also been used as a “ground reference” for statistical analysis of the PR-OBS-2 product during selected precipitation events.

Case study PR-OBS-1 vs. INCA,15 August 2010 15:00 UTC

This is the first case study elaborated at SHMÚ which compares the PR-OBS-1 product with precipitation fields produced by the INCA system. In order to make precipitation fields from the microwave instruments and ground observations at 1 km resolution comparable, the INCA precipitation fields have been upscaled into the PR-OBS-1 native grid using the Gaussian averaging method.

Ellipses in next figure represent the satellite instrument IFOVs with colour corresponding to the upscaled radar, rain-gauge and INCA analysis rain-rate value in case of next figure a), b) and c), respectively, or the satellite rain-rate value in case of next figure, part d).

As can be seen in next figure, part b) the rain-gauge network captured intense precipitation near the High Tatras mountain in the northern part of Slovakia where only low precipitation rates were observed by radars (next figure, part a) The resulting INCA analysis is shown in next figure, part c).

The corresponding PR-OBS-1 field (next figure, part d)) shows overestimation even when compared with the rain-gauge adjusted field of the INCA analysis.

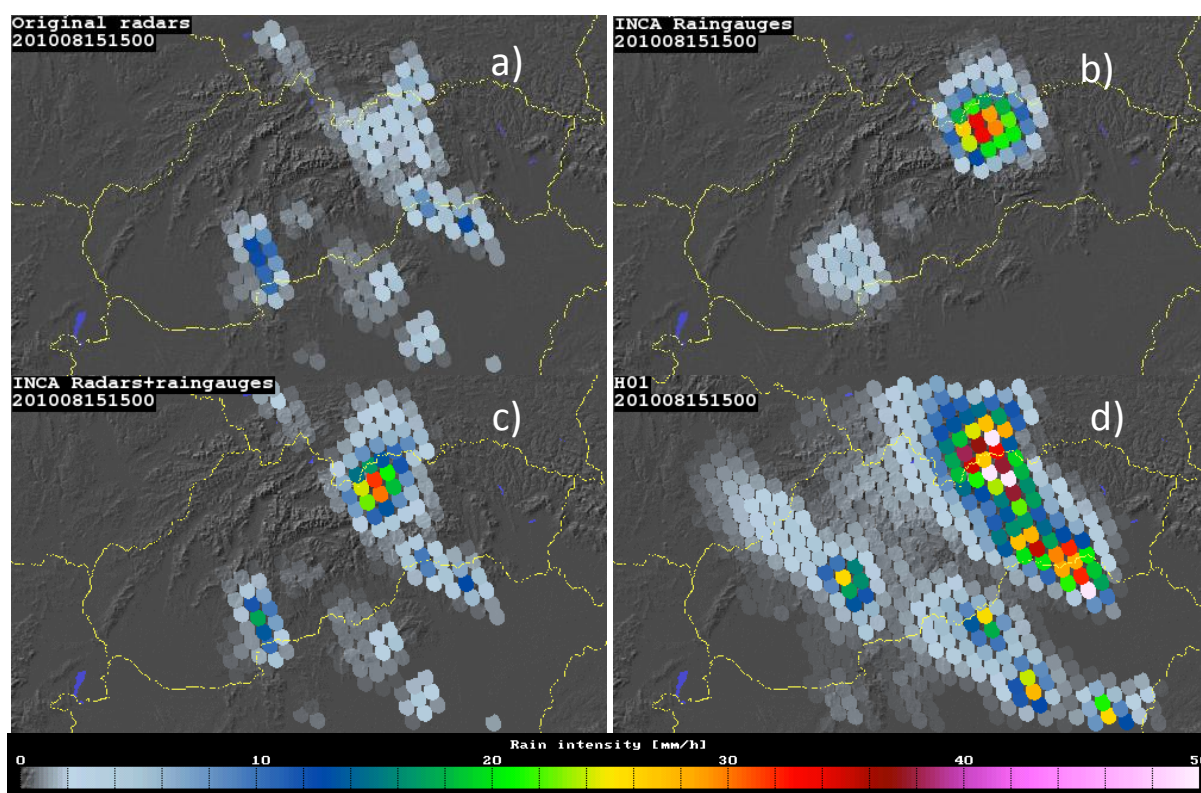


Figure 107 Precipitation intensity field from 15 August 2010 15:00 UTC obtained by a) radars, b) interpolated raingauge data, c) INCA analysis and d) PR-OBS-1 product

Visual comparison of the precipitation fields

In this section two case studies from 15 August 2010 focused on performance of the INCA analyses are presented.

15 August 2010, 06:00 UTC

This case illustrates potential of the INCA system to correct errors in radar precipitation measurements due to radar beam attenuation in heavy precipitation. As can be seen in Fig. 3a) the radar measured precipitation near centre of the circled area was relatively weak. However, as Fig. 3c) suggests, the precipitation was probably underestimated by radars because an intense convective cell occurred directly in path of the radar beam (dashed line in Figure 108 part c). The raingauge network (Figure 108 part b) captured the intense precipitation underestimated by radars and improved the INCA analysis (Figure 108 part c).

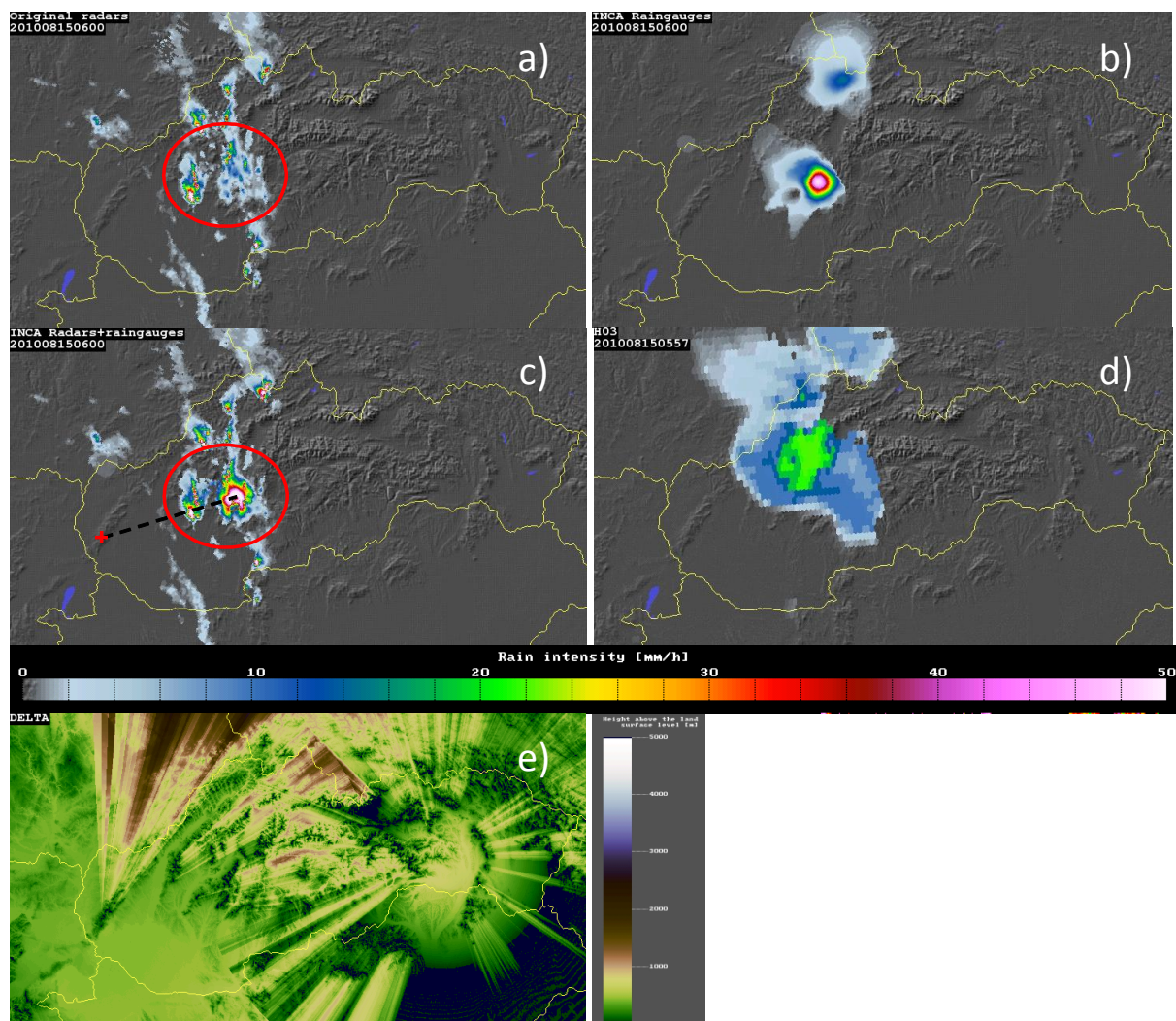


Figure 108 Precipitation intensity field from 15 August 2010 6:00 UTC obtained by a) radars, b) interpolated raingauge data, c) INCA analysis and d) PR-OBS-3 product (5:57 UTC) supplemented with map of minimum visible height above surface level (SHMU radar network)

15 August 2010, 08:00 UTC

The case from 08:00 UTC (Figure 109) gives an example of partial correction of radar beam orographical blocking by the INCA analysis. The radar precipitation field in the north-western part of Slovakia (Figure 109a) is affected by orographical blocking as indicated by relatively high minimum elevations of radar beam above this location in Figure 109e). Also in this case information from raingauge network (Figure 109b) supplemented the radar field in the resulting INCA analysis (Figure 109c).

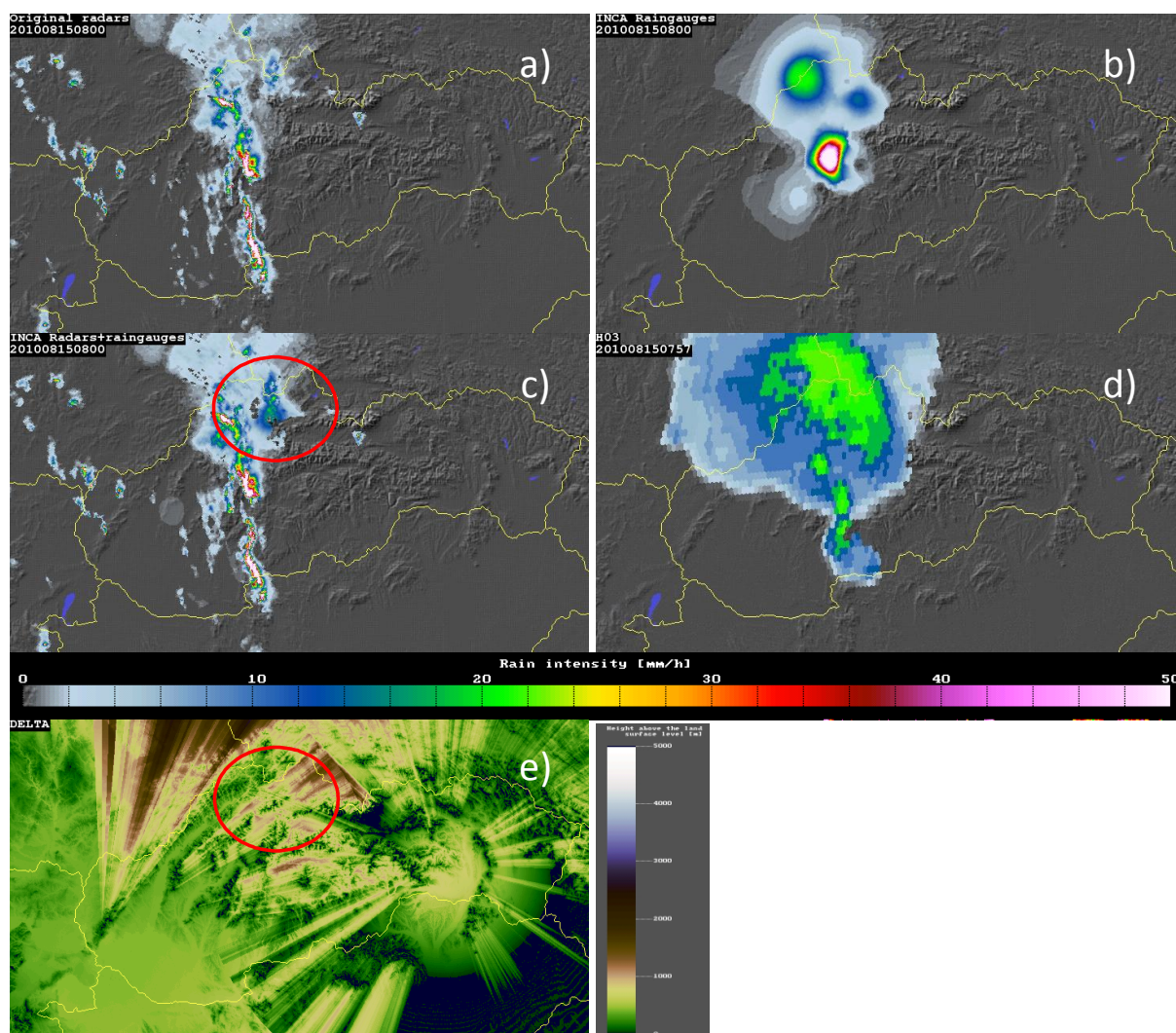


Figure 109 Precipitation intensity field as in previous figure, except for 8:00 UTC

Statistical analysis of the PR-OBS-2 product on selected precipitation events

As a first step towards utilizing the INCA precipitation analyses for the H-SAF validation, it has been decided to perform at SHMÚ a statistical analysis of the H-SAF products using the precipitation fields from INCA, radars and raingauges as a “ground reference” data for selected precipitation events. Since this task required modification of the SHMÚ software currently used for upscaling radar data, until now results for the PR-OBS-2 product are only available.

In order to eliminate interpolation artefacts in the areas outside the raingauge network occurring in the INCA analyses, only the PR-OBS-2 data falling inside the Slovakia territory were taken into account in the statistical analysis.

Overall five precipitation events with different prevailing type of precipitation have been selected for the statistical analysis as listed in next table.

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Event	Period (UTC)	Precipitation type
1	15 August 2010 00:00 - 21:00	convective
2	16 August 2010 06:00 - 23:45	convective
3	15 September 2010 15:00 - 18 September 2010 09:00	mixed
4	21 November 2010 20:00 - 22 November 2010 23:45	stratiform
5	28 November 2010 15:00 - 29 November 2010 10:00	stratiform

Table 58 List of precipitation events selected for statistical analysis

For each precipitation event and each “ground reference” data a set of continuous and dichotomous statistical scores was computed. The scores and thresholds of the precipitation classes were adopted from the H-SAF common validation methodology.

As an example, the results of selected statistical scores obtained with different reference data for the event 1 and 4 are shown in next two figures respectively.

Due to the small number of compared PR-OBS-2 observations during the selected precipitation events (overall convective: 1864 observations, stratiform: 2251, mixed: 3409) the obtained results may not be representative enough. Therefore it is questionable if any conclusion about dependence of the investigated “ground reference” data on the long-term validation results can be made. It is proposed that statistical analysis using longer validation period will have to be performed.

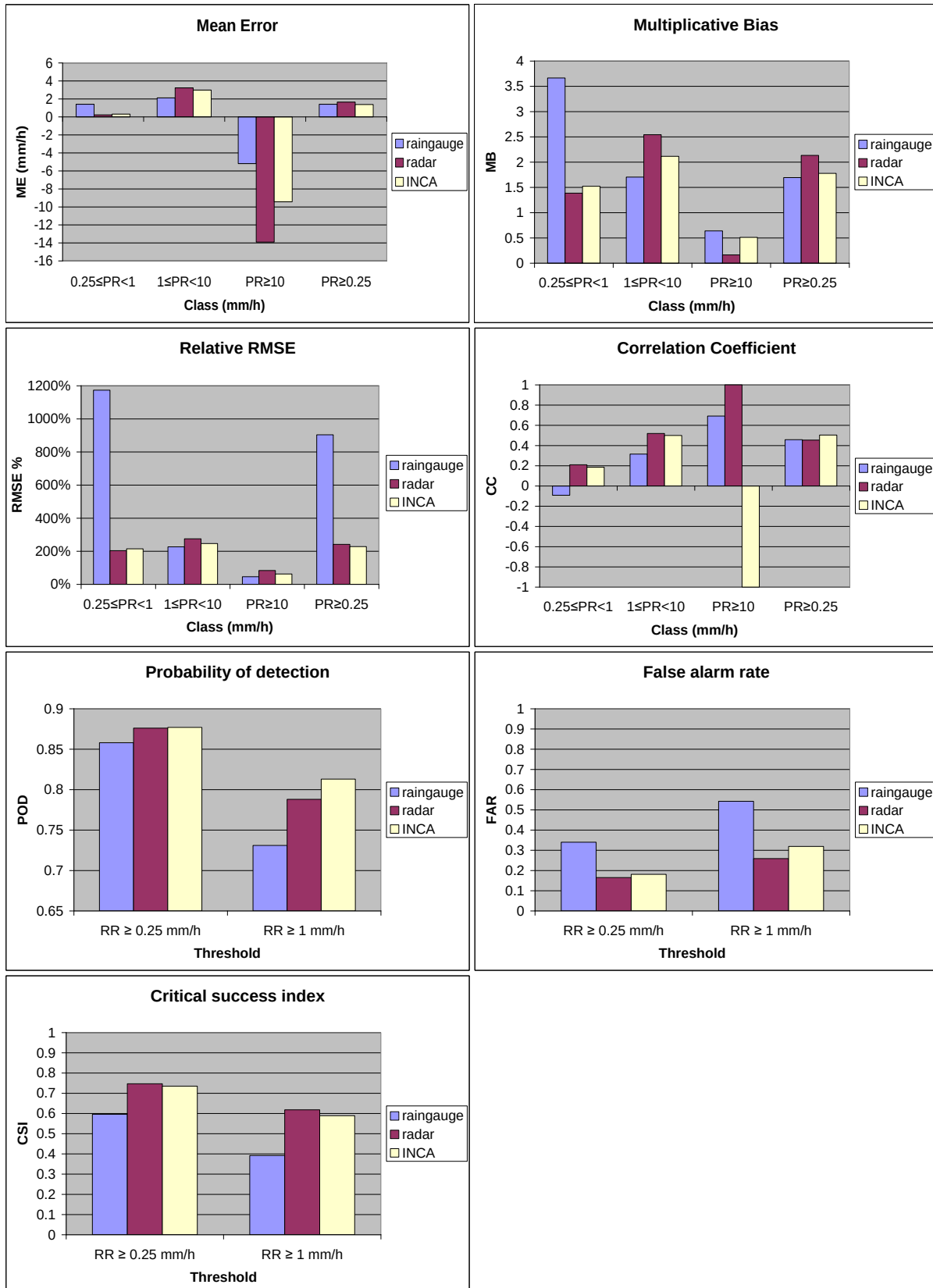


Figure 110 Comparison of selected statistical scores for the PR-OBS-2 product obtained by different “ground reference” data; valid for event 1 (convective)

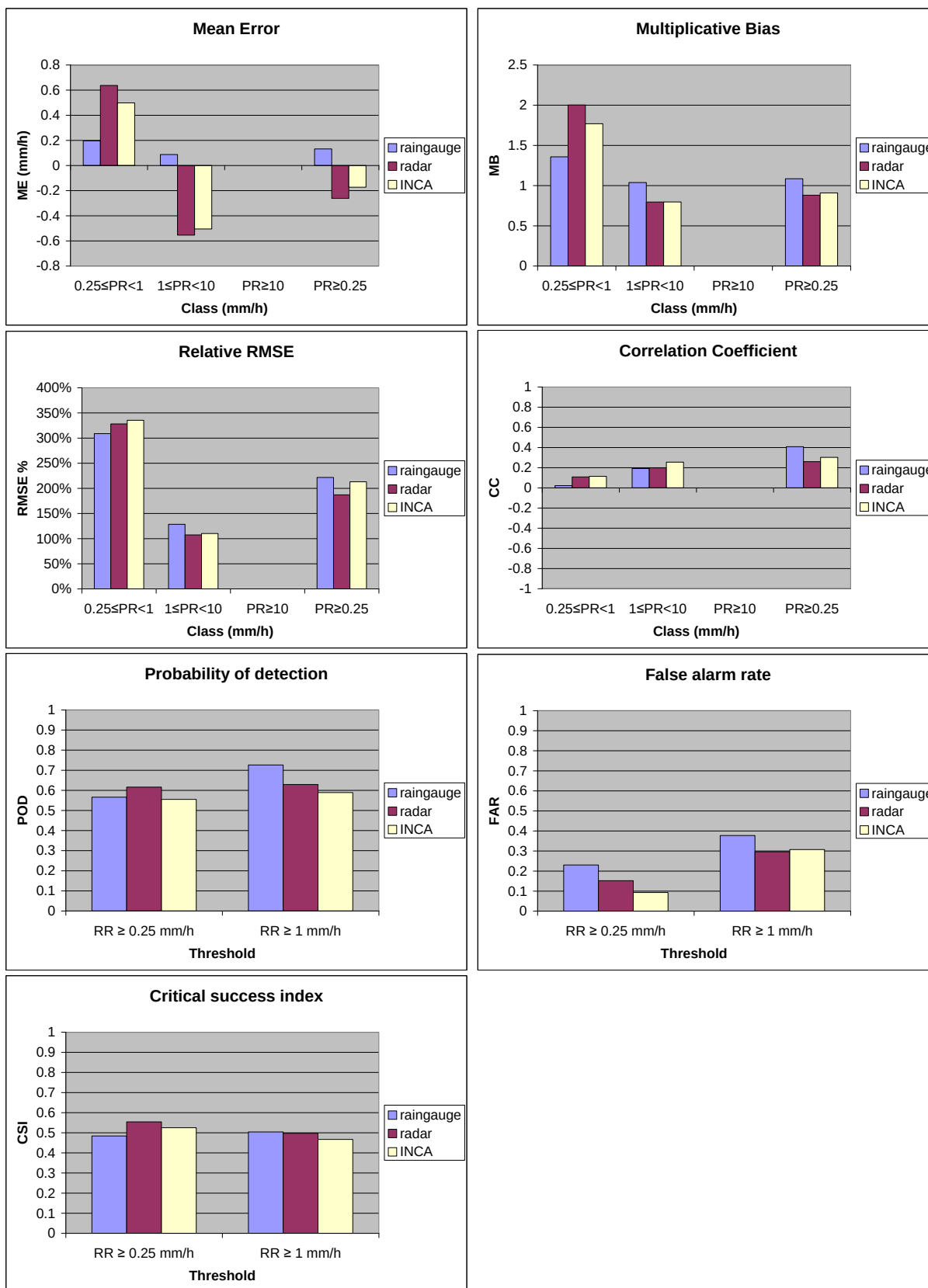


Figure 111 Comparison of selected statistical scores for the PR-OBS-2 product as in previous figure except for event 4 (stratiform)

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Conclusion

The INCA system as a potential tool for the precipitation products validation is available in Slovakia and Poland, in both countries being run in pre-operational mode. It is still relatively new system undergoing continuous development. More sophisticated algorithms of the precipitation analysis (e.g. assimilation of the 3-D radar data) can be expected from its development in frame of the ongoing INCA-CE project.

In Germany similar precipitation analysis system called RADOLAN is being run operationally. This tool is already used for validation of the H-SAF precipitation products in this country.

The accuracy and reliability of the raingauge stations significantly affect final precipitation analysis of the INCA or INCA-like systems and therefore need to be checked. In order to solve this problem an automated blacklisting technique is going to be developed at SHMÚ (currently blacklisting is used in manual mode).

The case studies presented in the report comparing the INCA analyses with corresponding input precipitation fields from radars and raingauges pointed out the benefits of the INCA system. It has been shown that the system has potential to compensate errors due to effects like radar beam orographical blocking but also to correct instantaneous factors affecting radar measurement quality like radar beam attenuation in heavy precipitation what cannot be achieved by standard methods of climatological radar data adjustment.

First attempts to utilize the INCA analyses as a “ground reference” data for the H-SAF products validation have been done by statistical analysis of the PR-OBS-2 product during selected precipitation events.

The software for upscaling the INCA precipitation field into the H-SAF products grid will have to be developed. Since the grids of INCA and RADOLAN have similar horizontal resolution to the common radar grid, the radar upscaling techniques can be applied also on the INCA or RADOLAN data. In frame of the unification of the validation methodologies the same common upscaling software could be shared between both radar (WG2) and INCA (WG3) working groups in the future.

References:

- T.Haiden, A. Kann, G. Pistotnik, K. Stadlbacher, C. Wittmann: Interated Nowcasting through Comprehensive Analysis (INCA) System description. ZAMG, Vienna, Austria, 4 January 2010
- André Simon, Alexander Kann, Michal Neštiak, Ingo Meiold-Mautner, Ákos Horváth, Kálmán Csirmaz, Olga Ulbert, Christine Gruber: Nowcasting and very short range forecasting of wind gusts generated by deep convection. European Geosciences Union General Assembly 2011, Vienna, Austria, 03 - 08 April, 2011
- Ingo Meiold-Mautner, Benedikt Bica, Yong Wang: INCA-CE: A Central European initiative in nowcasting applications. Central Institute for Meteorology and Geodynamics, Hohe Warte 38, 1190 Vienna, Austria
- Ingo Meiold-Mautner, Yong Wang, Alexander Kann, Benedikt Bica, Christine Gruber, Georg Pistotnik, Sabine Radanovics: Integrated nowcasting system f or the Central European area: INCA-CE. Central Institute for Meteorology and Geodynamics (ZAMG), Hohe Warte 38, 1190 Vienna, Austria

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13 Annex 6: Working Group 4 “PR-ASS-1 (COSMO grid) validation”

PROPOSAL

The aim of the group is to find, in cooperation with the developing team of PR-ASS-1, the most reliable way to validate the PR-ASS-1 product, which is provided on the COSMO model grid in a rotated coordinate system, and to develop software tools for a common validation methodology of the product.

Activities:

First step – defining the best validation strategy for PR-ASS-1, depending on the resolution of the ground data used. Implementation of prototype software for grid-cutting and ground data up-scaling in the COSMO grid (with the help of Lucio Torrisi, CNMCA).

Start Time - End time : November 2010 - December 2010

First Report: 20th of December 2010

Second step- up-scaling software tools dissemination and checks by the different validation teams. Eventual improving and refining if needed.

Start Time-End time: January 2011 – February 2011

Final Report: 28th of February 2011

Codes delivery and related documentation: 28th of February 2011

Composition of the working group:

Coordinator: Angelo Rinollo (RMI, Belgium) supported by Federico Porcù (University of Ferrara, Italy) and Lucio Torrisi (CNMCA, Italy)

Participants: Belgium, Bulgaria, Germany, Italy, Hungary, Slovakia, Turkey.

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REPORT

H-SAF project – WP 6100 - Working Group 4: Development of a common procedure for validation of PR-ASS-1 in the native COSMO model grid

A.Rinollo (RMI, Belgium), F.Porcu' (Università di Ferrara, Italy), L.Torrisi (CNMCA, Italy)

Validation technique depends on data resolution

The task of the present group is to develop a common validation procedure for the PR-ASS-1 product, characterized by the COSMO model native grid, which is built up in a rotated coordinate system. Depending on the resolution of the ground data, we decided to suggest two different approaches:

- in case of ground data with a spatial sampling similar to the one of COSMO (that is the typical case of raingauge networks), the nearest-neighbor approach is suggested. In this case, no upscaling is needed.
- in case of a resolution of the ground data much finer than the one of COSMO (that is the case of many radar products), then the upscaling to the native COSMO grid is recommended. For this case, we are currently working on a common upscaling procedure.

Methodology

The main issue in this task is the fact that PR-ASS-1 is based on the rotated coordinate system of the source model (COSMO), while the ground observations are normally based on geographical coordinates.

For this reason, in case upscaling is needed, a regular portion (i.e. a fixed number of rows and columns) is extracted from the COSMO grid. Then all the coordinates of the ground data are converted in the rotated system, and associated to the grid cell in which they fall in.

At this stage, upscaling technique is straightforward: the upscaled value associated to every grid cell is simply the arithmetical average of all the ground observations falling into that cell.

Software development: extraction of a regular subset in the PR-ASS-1 files

The first program we developed, useful to all groups (with both the validation approaches) allows to select a fixed number of rows and columns in the PR-ASS-1 files, given the geographical extremes of the chosen validation area. In this way, it's possible to process uniquely the data falling in and around the region of interest.

Software development: upscaling of fine-resolution data to the COSMO grid

A prototype version of the upscaling procedure has been developed and successfully tested over Belgium. It consists of two programs: the first creates a “lookup table”, a file which states a correspondence between every point of the observational grid (radar in this case) and the corresponding cell of the chosen subsection of the COSMO grid in which it falls. The second upscales every observational file to the COSMO grid, given the lookup table, and it is part of the Belgian validation procedure previously developed by E. Roulin (RMI, Belgium).

Preliminary testing results

Here are the preliminary results obtained by testing the upscaling procedure over Belgium. On the left the original images (from Wideumont radar, RMI, Belgium) and on the right the corresponding upscaled images. The images appear correctly upscaled.

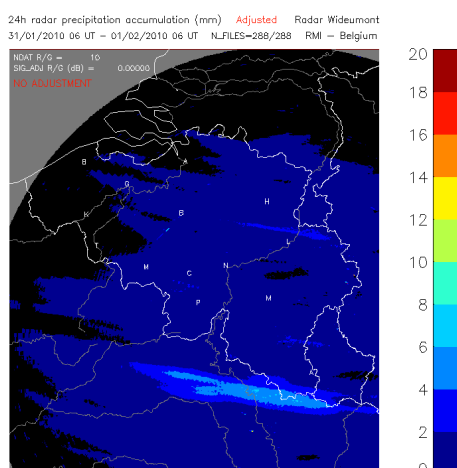


Figure 112 The Wideumont radar image of 1/2/2010 (cumulated rainfall in the previous 24 hours, raingauge-adjusted)

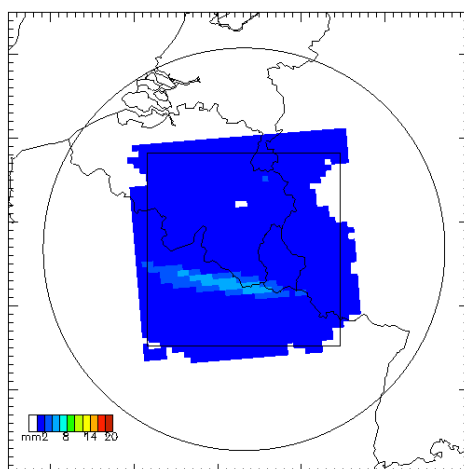


Figure 113 The Wideumont radar image of 1/2/2010 upscaled to the COSMO grid

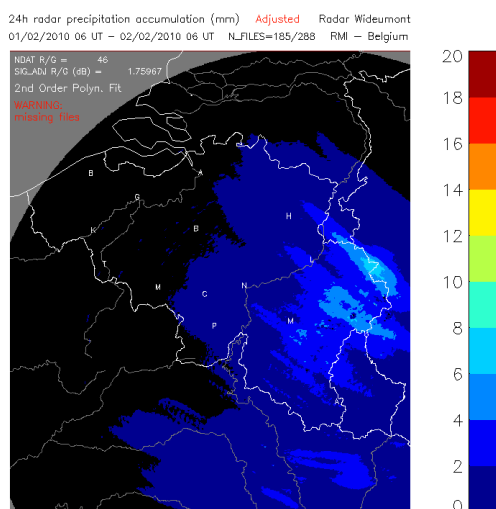


Figure 114 The Wideumont radar image of 2/2/2010 (cumulated rainfall in the previous 24 hours, raingauge-adjusted)

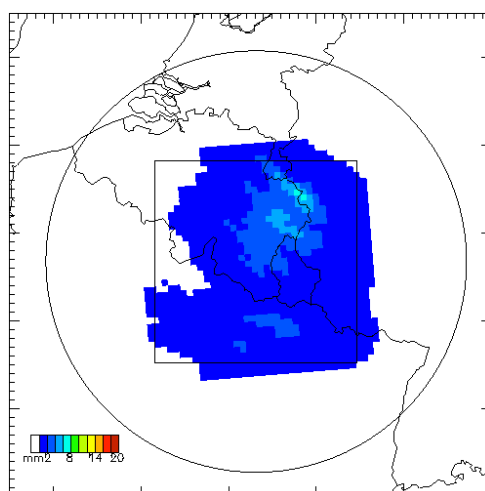


Figure 115 The Wideumont radar image of 2/2/2010 upscaled to the COSMO grid

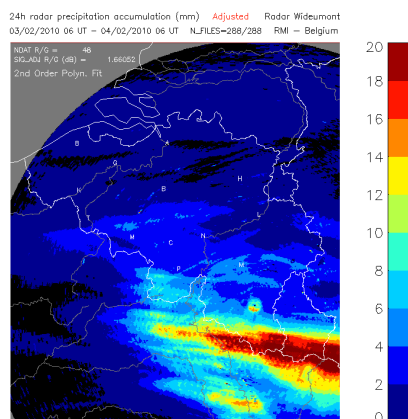


Figure 116 The Wideumont radar image of 4/2/2010 (cumulated rainfall in the previous 24 hours, raingauge-adjusted)

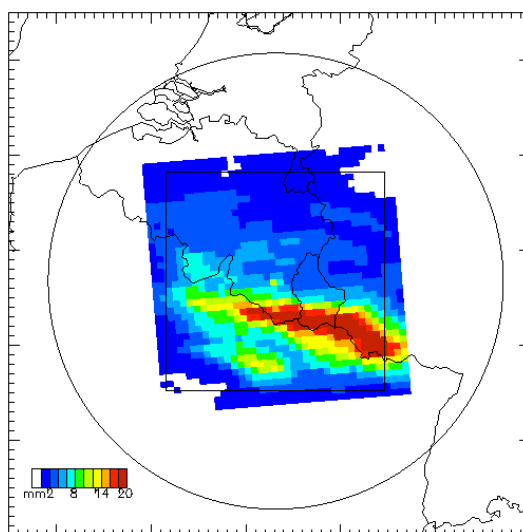


Figure 117 The Wideumont radar image of 4/2/2010 upscaled to the COSMO grid

Adaption of the software to all the groups and delivery for testing: present status

After successful testing over Belgium, the software has been adapted for common use by all the other groups, and then delivered for testing. Some feedback from Hungary and Slovakia has already been received and used for improvements. The testing by all the groups is still in progress.

References

About the COSMO model rotated grid, see:

<http://www.cosmo-model.org/content/model/documentation/core/cosmoDyncsNumcs.pdf>
pages 21-27.

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14 Annex 7: Working Group 5 “Geographical maps – distribution of error”

PROPOSAL

Validation activities performed during Development Phase for land and coast areas showed the difference in H-SAF precipitation products quality depending on geographical localisation. Those first achievements as well as the request from Hydrological Validation Group to provide the error characteristic of precipitation products for test catchments made Precipitation Validation Group to set up a Working Group for creating geographical maps of error distribution. The main goals of this working group are:

- to investigate the opportunity to create geographical maps of error distribution for H-SAF validation;
- to define (if necessary) the methodology for spatial representation of precipitation products errors;
- to produce a well referenced documentation on the methodology defined;
- to produce two short reports on the results obtained (first: by 31st of March 2011 and second by 30th of November 2011);
- to develop if necessary the code to be used in the PPVG for a correct generation of the defined geographical maps of error distribution.

Activities:

First step – to define the methodology

- selection of the appropriate methodology for spatial distribution of precipitation products errors taking into consideration spatial and temporal characteristics of each product;
- first study performed for selected Polish test catchments as well as Polish territory;

Start Time - End time : December 2010 - March 2011

First Report: 31st of March 2011

Second step

To define the precipitation products errors maps for country – members of PPVG.

- collection of collocated ground data and satellite products for selected period (possibly through 6300);
- creation of the error maps for territory of PPVG country - members for selected period;
- analysis of the achieved results emphasizing the errors distribution obtained for test catchments;
- analysis of the possible solutions for operational creation of the error maps and selection of the best one;
- creation the software (if necessary).

Start Time-End time: March 2011 – November 2011

Second Report: 30th of November 2011

Coordinator: Bozena Lapeta (IMGW, Poland)

Members: Ibrahim Somnez (ITU, Turkey)

H-SAF project – Validation Programme- WP 6100 –
Working Group 5: Geographical maps – distribution of error**Bozena Lapeta (IMGW, Poland)**First report – March 31st, 2011**Introduction**

The Working Group 5 aims at creating geographical maps of H-SAF products' error and analyzing its usefulness for H-SAF validation. The idea of this work stemmed from hydrological validation community that is interested in distribution of the error over the catchments. In this report the results obtained during the first step of WG5 activities aiming at selection of the best method for mean error specialization are presented.

Selection of spatialisation algorithm – first results

The most important issue in creating geographical distribution of any parameter is the algorithm for spatial interpolation. As there is no universal spatial interpolation method that can be applied for any parameters, the first step in the creation of maps of H-SAF precipitation products error was the selection of the interpolation algorithm. Commonly used Ordinary Kriging, Inverse Distance Weighted and Natural Neighbour methods were tested firstly. The analysis was performed for monthly average mean error of H-05 3 h cumulated precipitation for selected months. In the analysis data from Polish rain gauges were used. In the next figure the example mean error maps for July 2010 obtained using three mentioned above algorithms are presented.

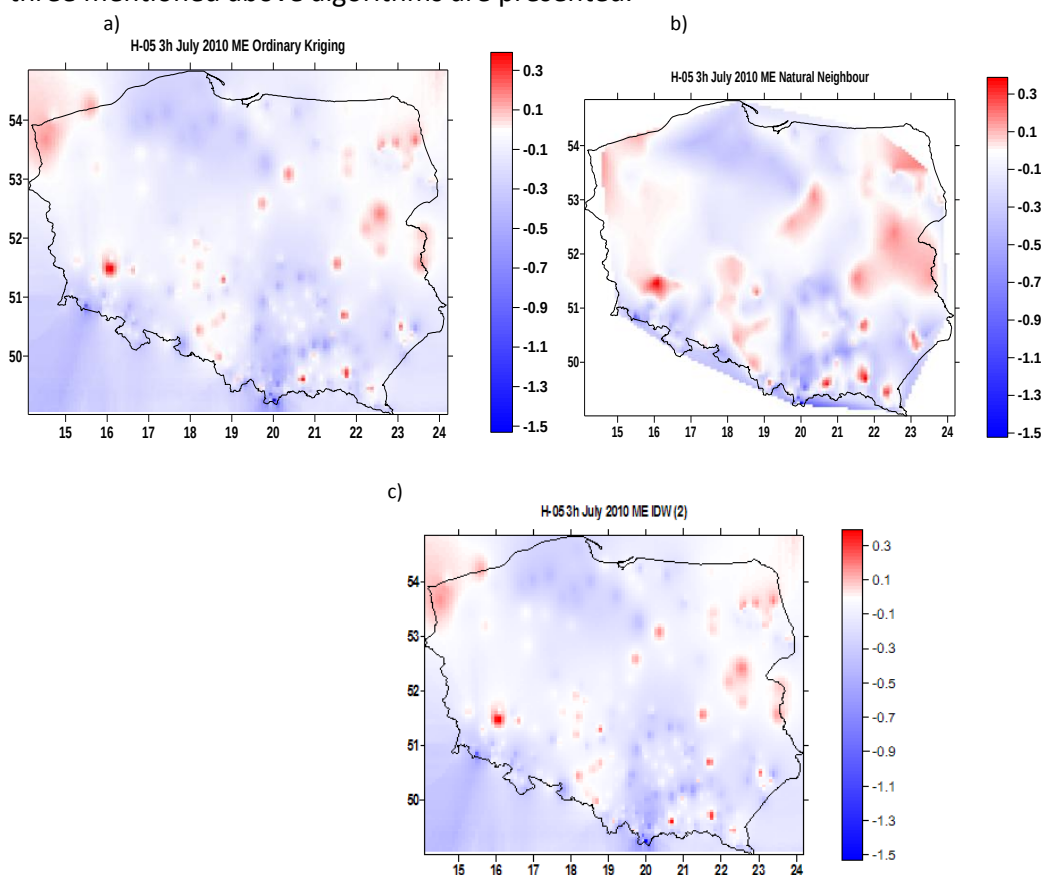


Figure 118 Distribution of the monthly average H-05 3 h cumulated precipitation Mean Error calculated for July 2010 using three methods: a) Ordinary Kriging, b) Natural Neighbour, and c) IDW (2)

One can see that the obtained maps do not differ significantly, however, for the map created with the use of Natural Neighbour method, the maximum and minimum values are less pronounced than on the other two maps. Moreover, application of Natural Neighbour method does not allow for extrapolating the distribution beyond the area defined by stations.

In order to evaluate the quality of the error distribution, the cross validation was performed and the results are presented on the next figure.

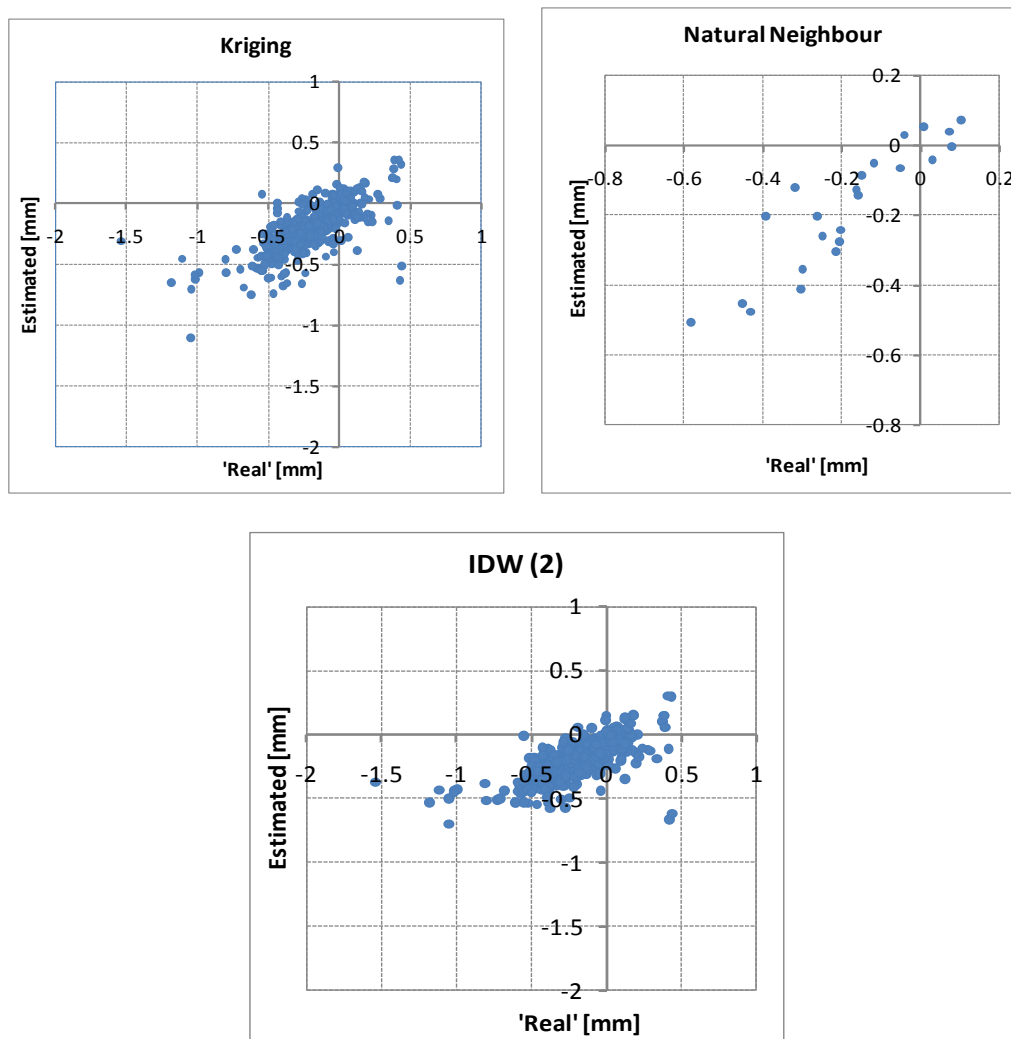


Figure 119 Cross validation results obtained for three different methods for spatial interpolation

For all methods, the results are similarly scattered around the perfect estimation, however, for IDW(2) some underestimation was found for negative ME values. The values of Mean Residual and Mean Absolute Residual defined as mean and mean absolute difference between Estimated and Real values of ME are presented in the next table.

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	Mean Residual	Mean Absolute Residual
Kriging	-0.004	0.09
Natural Neighbour	0.007	0.06
IDW(2)	-0.009	0.10

Table 59 Mean Residual and Mean Absolute Residual values obtained for three algorithms for spatial interpolation using cross-validation approach

The lowest value of Mean Absolute Residual was found for Natural Neighbour method, what indicates that application of this algorithm may allow for minimizing the systematical error introduced by spatialisation method. Therefore this method seems to be the best for creating the geographical distribution of H-SAF products error for countries characterized by terrain geographical configuration similar to the Polish one.

Conclusions

The analysis performed for ME of H-05 3 h cumulated product obtained using data from Polish network of rain gauges showed that Natural Neighbour interpolation method seems to be the best one for creating maps of H-SAF products error. However, application of Natural Neighbour method does not allow for extrapolating the distribution beyond the area defined by stations, what is a disadvantage of these methods.

As the maps are to be created for the whole H-SAF domain, presented above results should be verified over other countries. Therefore, in the next step of WG5 activities the study will be performed for other countries and for the errors calculated using radar data.

15 Annex 8: Comments on the Validation Results for Products PR-OBS-1, PR-OBS-2 And PR-OBS-3

Casella F. *, Dietrich S. *, Levizzani V. *, Mugnai A. *, Laviola S. *, Petracca M. ***, Sanò P. *, F. Zauli **

* CNR-ISAC, ** CNMCA, ***VS EUMETSAT

The results of WGs said that is not possible to consider radar and raingauge fields like the reference and the accuracy indicated in the table 63, RMSD, is the degree of closeness of measurements of a quantity to its actual reference value. The reference value of precipitation fields is not available, and the measurement available are a limited picture of the reference. Then it is important to evaluate which are the limits of “available reference” and then to understand the sources of errors of data used to evaluate the satellite outputs. Taking in account this consideration a direct comparison of the requirements with the result of validation is not correct, since they have different meanings:

- the requirements indicate what **error** is allowed by the user to the satellite product to be significantly useful (*threshold*), or to produce a step improvement in the application (*target*) or to produce the maximum improvement before entering saturation (*optimal*); it is the RMSE of satellite v/s reference.

- the result of validation activities indicate the **difference** between the satellite measurement and the ground measurement utilized as a reference; it is the RMSD of satellite v/s reference.

Between target and optimal	Between threshold and target	Threshold exceeded by < 50 %	Threshold exceeded by ≥ 50 %
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PR-OBS1	Requirements			Result of validation
	threshold	target	optimal	
Accuracy RMS (> 10 mm/h)	30 %	20 %	10 %	89 %
Accuracy RMS (1-10 mm/h)	60 %	40 %	20 %	117 %
Accuracy RMS (< 1 mm/h)	200 %	100 %	50 %	232 %

Table 1 - Simplified compliance analysis for product PR-OBS-1

PR-OBS2	Requirements			Result of validation
	threshold	target	optimal	
Accuracy RMS (> 10 mm/h)	50 %	30 %	15 %	87 %
Accuracy RMS (1-10 mm/h)	60 %	40 %	20 %	115 %
Accuracy RMS (< 1 mm/h)	120 %	80 %	40 %	202 %

Table 2 - Simplified compliance analysis for product PR-OBS-2

PR-OBS3	Requirements			Result of validation
	threshold	target	optimal	
Accuracy RMS (> 10 mm/h)	80 %	40 %	20 %	92 %
Accuracy RMS (1-10 mm/h)	160 %	80 %	40 %	106 %
Accuracy RMS (< 1 mm/h)	320 %	120 %	80 %	195 %

Table 60 Simplified compliance analysis for product PR-OBS 1-2-3

Obviously, it is RMSD > RMSE, since RMSD is inclusive of:

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- the error of satellite measurements $RMSE_{sat}$ (that is what we would like to know from validation);
- the error of ground measurements $RMSE_{ground}$ (that should be known by the owners of the stations);
- the error of the comparison methodology $RMSE_{comparison}$ (that should be estimated by metrologists).

Then we should consider It should be: $RMSE = (RMSE_{sat}^2 + RMSE_{ground}^2 + RMSE_{comparison}^2)^{1/2}$

In the final part of the H-SAF Development Phase attempts have been made to evaluate $RMSE_{ground}$.

All validation groups (not only for precipitation, but also for soil moisture and snow) have been requested to quote figures to characterise the errors of the ground reference that they used. The various team did this after consultation with the operational units in charge of the observing networks in their institutes. For precipitation the following figures were quoted.

Unit	Ground system	Rain rate	24-h accumulated
UniFerrara	Rain gauge	50 %	25 %
	Radar	100 %	50 %
BfG	Rain gauge	5 + 35 %	5 + 35 %
SHMU	Radar	100 % or 15 mm/h (for RR > 10 mm/h)	50 + 100 %
OMSZ	Radar	100 %	50 %
IRM	Rain gauge (interpolated)		70 + 100 %
	Gauge-adjusted radar		50 %
IMWM	Gauge	30 %	
TSMS	Gauge	25 %	10 %
Error range	Gauge	5 + 50 %	5 + 100 %
	Radar	50 + 150 %	50 + 100 %

Table 61 Errors of the ground reference provided by all validation groups

The values of table 64, apart from details, indicates that the errors due to the ground reference are of the same order than the threshold requirements. It is interesting to note that the validation activity has indicated that the results from rain gauge and radar are comparable, whereas the error of radar should be definitively higher. This means that radar is favored in the third error type, $RMSE_{comparison}$.

$RMSE_{comparison}$ is in reality a composition of several errors. It refers to the limitations of the comparison method that, in spite of all efforts envisaged and implemented by the validation teams, has left residual errors difficult to be further reduced, but needing evaluation by in-depth investigation. A short list is:

- upscaling/downscaling processes to make compatible the instrument resolution and the ground station representativeness have been applied, for instance by applying Gaussian filters, but the statistics of residual errors are not available; this problem affects radar to a minor extent than raingauge, that may explain why comparisons with radar finally are not worse than with rain gauge;
- the raingauge's representativeness of IFOV;

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- pixel geolocation is retrieved by using the information made available by satellite owners, and it is not perfect; it is necessary to evaluate how much mislocations impact on the accuracy of the comparison. The effect is clearly larger for convective precipitation. This may explain why product PR-OBS-3 is apparently performing better than PR-OBS-1 and PR-OBS-2: the high resolution minimizes mislocation errors.
- similarly, time mismatching is a source of error, more effective for convective precipitation, hence the advantage of PR-OBS-3; and also of radar, contributing to reduce the effect of intrinsic lower accuracy.
- parallax errors introduce mislocation of satellite precipitation, with associated comparison errors, larger for convective precipitation because of deeper penetration in the upper troposphere.

These (and maybe other) error sources need to be analyzed in detail in order to determine their contribution to the overall $RMSE_{comparison}$. WG and VS started to evaluate the sources of errors, awaiting the final results is it possible to reconsider the requirements like to understand the thresholds of requirements in table 63. Then it is need to anticipate the likely size of these errors. The very low POD values and very high FAR values, as well as the invariably poor values of the correlation coefficient, indicate that $RMSE_{comparison}$ could be dominant in the error partitioning with $RMSE_{sat}$ and $RMSE_{ground}$. An estimate of the errors due to the various effects impacting the $RMSE_{comparison}$ is not difficult. It is not necessary to build a large statistics, but just perform experiments using a few campaigns carried out over one dense rain gauge network, and one well-calibrated radar. In fact, the purpose is simply to evaluate the size of $RMSE_{comparison}$, not to reduce it (that would require a large effort, probably improductive).

For the sake of providing an example, it is noted that, if the three contributions $RMSE_{sat}$, $RMSE_{ground}$ and $RMSE_{comparison}$ were of comparable size, equipartitioning of the error would improve the RMSD by a factor $3^{1/2} = 1.7$, and the figures resulting from the current validation would match at least the threshold requirements.

In order to obtain an estimate of $RMSE_{comparison}$ and then a more accurate estimation of $RMSE_{sat}$, CNR-ISAC performed an experiment based on its polarimetric C-band radar (*Polar 55C*) located close to Rome, surrounded by a network of 14 rain gauges in an area of 14 km × 14 km (approximately the pixel of SSM/I at 85.5 GHz and of AMSU-B/MHS) generally used for the radar calibration. Assuming Polar 55C as “reference”, the the spread of rain gauge measurements resulted as follows:

$RR > 10 \text{ mm/h} : 50 \% \quad 1 < RR \leq 10 \text{ mm/h} : 80 \% \quad RR < 1 \text{ mm/h} : 150 \%$

A similar experiment, with 2 rain gauges in reduced area of 5 km × 5 km (approximately the pixel of SEVIRI at middle latitude), shows similar results. That’s means that

In order to obtain an estimate of upscaling / downscaling and interpolation process theoretical experiment of some methodologies has been implemented. Hypothetic perfect fields are been defined and a grid of perfect measurements has been defined. The experiment assumed different typologies of precipitation field respect the variance of precipitation intensity in the field. To obtain the field of perfect measurements some grid points from the precipitation field are been

removed. The experiment removed the perfect rain gauge long a regular grid to simulate an unreal distribution of non realistic rain gauges.

The sampling has been done at different grid spacing (2, 3 and 4 time the perfect field) to obtain new data at different spatial density. Then, the algorithm performances of up/down scaling procedure to reproduce the original field are been evaluated. The work has been implemented for 4 different algorithms: Barnes, Inverse Distance Squared (IDS), kriging and Nearest Neighbor (NN).

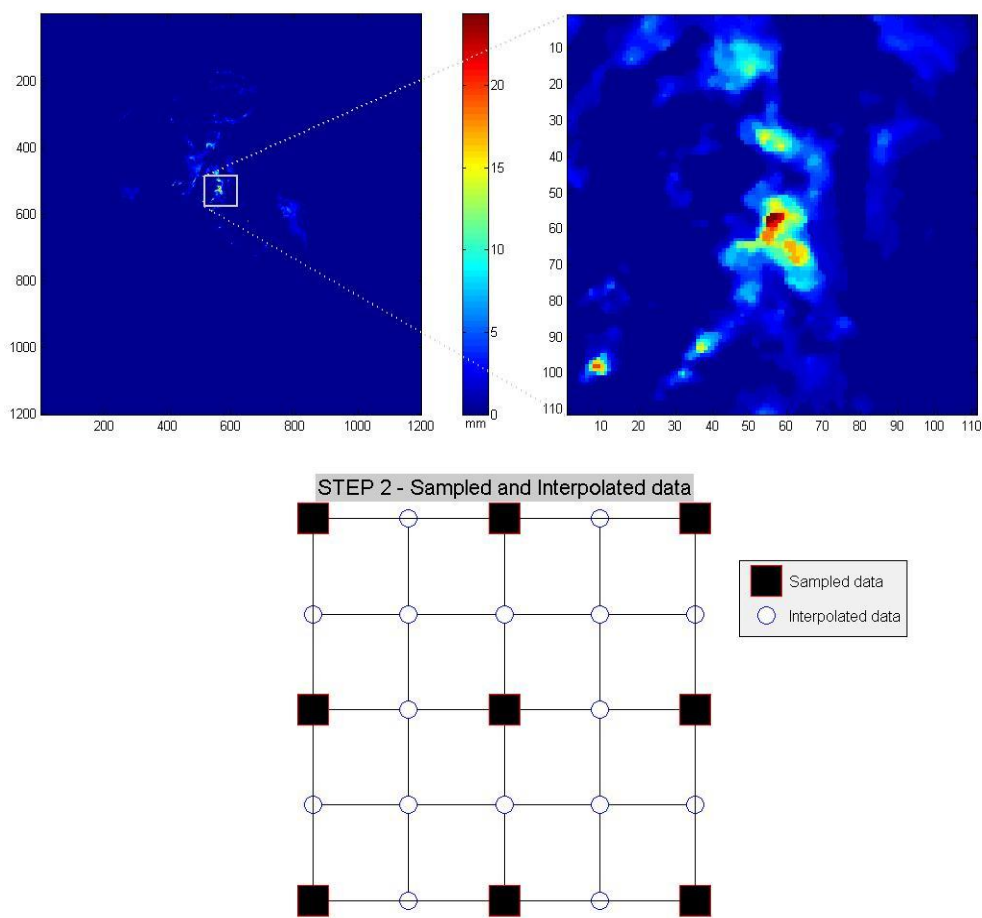


Figure 120 Example of sampled data for a regular grid. In right on the upper part a detail of field studied, below the original grid of field for step 2. From the field the white circles mean the data removed from the map. The black squares mean the position of perfect measurement. The techniques of up/down scaling reproduce the field only from the perfect measurements

The algorithms used in the validation group are similar to the Barnes algorithm. This like-Barnes algorithm creates a grid of regular step where each node contains the data calculated from all data weighted by distance from the node itself. The calculation is done several times (through successive iterations) in order to minimize errors in the precipitation field.

In the following table 65 are reported the values of RMSE were sat_i is the sampled and captioned data and $reference_i$ is the value of perfect field.

$$RMSE\% = \sqrt{\frac{1}{N} \sum_{i=1}^N \frac{(sat_i - true_i)^2}{true_i^2}} * 100$$

N is the total number of pairs data in which the *reference* value is different by 0.

Algorithms	Step 2	Step 3	Step 4
Barnes	32 ± 11 %	52 ± 34 %	68 ± 43%
Kriging:	35 ± 12 %	58 ± 36 %	77± 62 %
NN:	56 ± 20 %	77 ± 45 %	96 ± 50 %
IDS:	63 ± 37 %	71 ± 41 %	81.± 43 %

Table 62 RMSE% and standard deviation of interpolation algorithms for 3 different regular grids

In the cases studied, Barnes appears to be the algorithm with the lower mean value of RMSE% and their standard deviation than the other interpolation algorithms, and the error of interpolation can be evaluated in the 30% for the step 2 that means an ideal condition were the rain gauge are disposed long a regular grid with a distance that the half of phenomenon length. The structure of precipitation depends from precipitation typology, time and spatial resolution, therefore phenomenon length cannot be considered absolute.

An irregular distribution of perfect measurements has been considered also. For each step the number of perfect measurement has been redistributed randomly to simulate the rain gauge network. In the figure 124 below the white circles mean the position of perfect measurement points. In the figure 124 below the white circle mean the position of perfect measurement points in the best case (step 2). The results shown again the Barnes technique the best choice to reproduce the field.

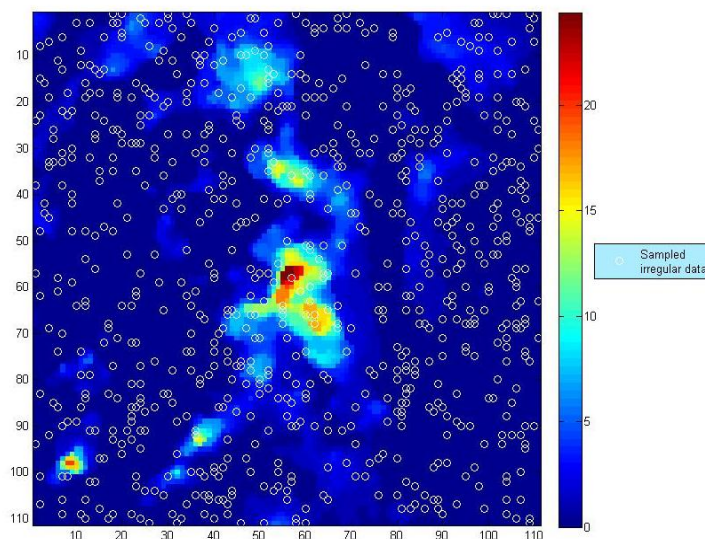


Figure 121 randomly distribution of perfect measurement to remap the field on a regular grid

Assuming the best condition (step 2 for the regular grid), an evaluation of spread of RMSE respect the structure of precipitation field has been done. In the figure 125 below the Barnes and Kriging

techniques show a low dependence from the standard deviation of field, ie the level of inhomogeneity of field. The performance of up/down scaling techniques are reported in table below:

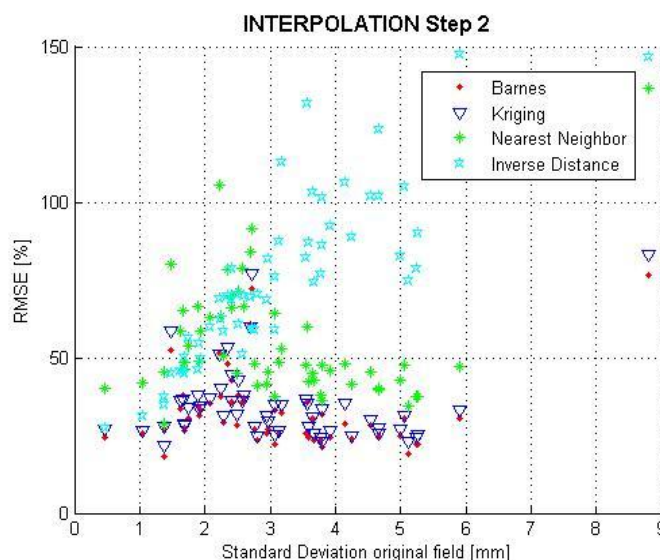


Figure 122 STD vs. RMSE% for interpolations by step 2

Taking into account the results discussed before is possible to define a range of uncertainty that is necessary to consider when comparing the results of validation with operational requirements. More effort has to be done to understand if exist a link between the error of remap procedure and precipitation intensity, but the preliminary study shows that in the best case an error of 30% has to be considered for the up/down scaling remapping procedure.

Using the previous equation we can derive: $RMSE_{sat} = (RMSD^2 - RMSE_{ground}^2 - RMSE_{comparison}^2)^{1/2}$ where, $RMSD$ is provided by the validation activity, $RMSE_{ground}$ is provided by tab. 64 using the University of Ferrara numbers. At the moment for the $RMSE_{comparison}$ is assumed: equal to three values resulting from the ISAC study for validation w.r.t. rain gauges, and equal zero for validation w.r.t. radar, plus a 30% for the remapping procedure.

Conclusions:

- 1) It is believed that the results of the validation activity cannot be substantially improved: they are most probably consistent with the size of the error sources (satellite, ground stations and comparison method). This needs to be confirmed by evaluating the size of the error associated with the limits of the comparison technique.
- 2) It must be considered that the total $RMSD$ is affected by other-than-satellite terms, one of which $RMSE_{ground}$, very difficult to be reduced, and the other one, $RMSE_{comparison}$, possibly dominant (and also very difficult to be reduced). This tells us that the validation figures have a large component, which is independent from the structure of the algorithm.
- 3) However, the case for continuing algorithm improvement is very strong. Data are produced for being used, and the better the quality, the higher the impact. The fact that the current validation

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methodology cannot completely evaluate the intrinsic error of satellite data is regrettable, but should not prevent a better representation of the physics in the retrieval model.

4) The case for continuing the validation activity essentially as it is now, or improving it if considered cost-effective, is also very strong since it is necessary to continuously watch that the product generation chain works correctly.