



# CHALMERS

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## **Undersökning och utveckling av multi- filterbox**

### **För mätningar på spuriöser**

Examensarbete inom högskoleingenjörsprogrammen Dataingenjör och Elektroingenjör

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## **Foreword**

We would like to thank Michael Johansson for the opportunity to work with this bachelor thesis. We would also like to thank our supervisors, Göran Hult and Jörgen Ankarberg, who have helped us during the work. Thanks to Samir Kilim and Martin Hedin for help with programming and theoretical questions. We would also like to extend our thanks to Jonas Noreus for his help with questions on how to write this thesis.

David Wahlberg & Lucas Wiman

Göteborg, 2014

## Summary

This report describes the theoretical design of a flexible filter box for Ericsson at Lindholmen, which purpose is to be able to be used in the measurement of spurious emissions, which are unwanted interfering frequencies, outside radio frequency bands. The filter box needs, over a wide frequency range, to amplify low power spurious emissions to make them measurable and attenuate the carrier signal so the instruments used in combination with the filter box does not break. The report describes the procedure of investigating viable components for the filter box which fits with the requirements in terms of noise, size and cost of each component. These components were only studied in theory using datasheets and information from distributors as it would be very expensive to order them for the purpose of testing. The idea of using tuneable filters as components for the filter box in order to cover a wider variety of frequency bands and lower the amount of necessary filters was looked into. Based on the investigation of noise and size a filter box configuration was developed. In theory it meets the noise, size and intermodulation requirements; however the amount of intermodulation, a form of distortion in passive non-linear elements, from all components cannot be determined in theory and could therefore be incorrect. An application written in the programming language Agilent VEE was developed to add the possibility of controlling the filter box with a computer. However, since there were no actual physical components to test with the application the use of stubs was required, stubs are replacements for real components to simulate the components behaviour. As a result, the application itself requires further development so it can integrate with physical components. In addition, the outline of an automatic measurement algorithm for the filter box was developed. The algorithms purpose is to ensure instruments do not break during measurements using the filter box.

## Abstract

Den här rapporten beskriver den teoretiska designen av en flexibel filterbox för Ericsson Lindholmen vars syfte är att användas för mätningar av spuriösa, som är oönskade störande frekvenser utanför radiofrekvensband. Filterboxen måste, över en vid frekvensräckvidd, kunna förstärka svaga spuriösa för att göra dem mätbara, samt att dämpa bärvågen så att instrumenten som används tillsammans med filterboxen inte går sönder. Rapporten beskriver de tillvägagångssätt som använts för att undersöka om komponenter för filterboxen klarar de brus-, storlek- och kostnadskrav som ställts. Komponenterna studerades enbart i teori med hjälp av datablad och information från distributörer eftersom det hade varit för dyrt att beställa in alla komponenter och testa dem. Idén med att använda filter med inställbar frekvens i filter boxen för att täcka så många frekvensband som möjligt, och samtidigt minska mängden filter som krävs för boxen har undersökts. Baserat på undersökningarna av brus och storlek, utvecklades en filterboxkonfiguration som teoretiskt sätt klarar brus-, storlek- och intermodulationskraven. Men mängden passiv intermodulation, en typ av distortion i passiva icke-linjära element, från alla komponenter kunde inte bestämmas med enbart teori. P.g.a detta så är intermodulationsfrågan fortfarande osäker. En applikation, skriven med programspråket Agilent VEE, utvecklades för att lägga till möjligheten att styra den tänkta filterboxen med en dator. Eftersom det inte fanns några fysiska komponenter att testa med applikationen så fick stubbar användas, stubbar är ersättningskod för att simulera komponenternas uppförande. Detta medför att applikationen behöver fortsatt arbete så den kan integreras med framtida fysiska komponenter. Utöver programmet designades grunderna för en automatisk styrningsalgoritm för filterboxen. Dess syfte är att försäkra att inga instrument eller komponenter går sönder under mätningar med filterboxen.

## **Abbreviations**

BW – Bandwidth

CW – Constant Wave

dBc – decibel in relation to carrier

DUT – Device under test

LNA – Low noise amplifier

IL – Insertion loss

IM – Intermodulation

OOB – Out-of-Band

PIM – Passive Intermodulation

RS – Requirement Specification

RX – Receiver

SEM – Spurious Emissions

SNR – Signal-to-Noise Ratio

TX – Transmitter

VR – Verification Report

VS – Verification Specification

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# 1. INTRODUCTION

This chapter contains the background, purpose, delimitations and the scope of the project.

## 1.1 Background

Ericsson uses filters for verification measurements on radio units to radio base stations. At the product verification section, specific filter boxes are used for measurements on different radio bands which make their setup and configuration trivial. However, at the design/integration section these measurements take a lot of time, each set of measurements can take hours to setup and calibrate and they are extremely sensitive to external influence and the position of the cables. Switching from one radio unit to another could lead to the failing of the measurement setup, resulting in several hours of work being spent setting up the measurement again. A way to possibly avoid this problem would be the development of a multi-filter box with several sets of filters, controlled by a computer (See Figure 1).

The product design section at Radio Design Center-Lindholmen is interested in a general multi-filter box used for specific out of band measurements. As of currently, these kinds of measurements are done at system verification. However, because of time constraints at product design, there are occasions when there is no time to wait for system verification to do the measurements. Therefore, it would be of interest for the product design section to have their own filter box for measurements.

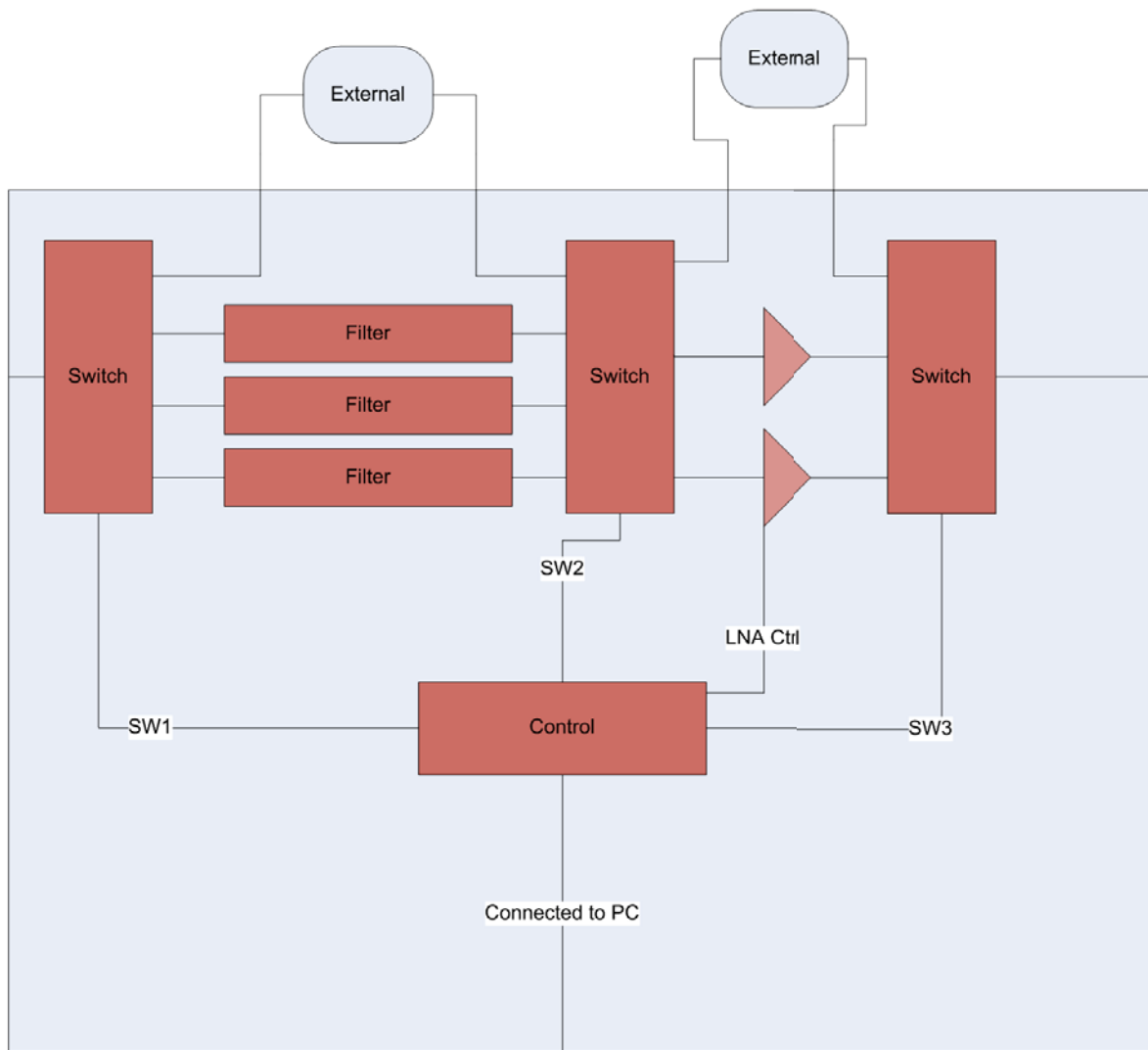


Figure 1: Early sketch of filter box

## 1.2 Purpose

The purpose of this report is to determine if it is possible to create a flexible filter box for verification measurements on radio units for radio base stations. The filter box should be able to attenuate a carrier signal to a level where a spectrum analyser can measure very weak signals out-of-band, and also amplify spurious emissions, the very weak signals, in case that they are underneath the noise floor of the spectrum analyser. This investigation is meant to give a good theoretical framework for the possibilities of physically constructing the filter box, should it be proven reasonable. This includes costs, size and various component requirements for the filter box.

## 1.3 Delimitations

In-depth software simulations of the filter box will not be investigated due to cost and time constraints. For the same reasons, the filter box will only be constructed in theory. The filter box's main purpose is to measure out-of-band spurious emissions; other applications may be possible, but they are not the focus of the investigation.

## **1.4 Scope**

This investigation shall determine the requirements for the various measurements and the restrictions they put on the system used for measurement and the filter box. The filter box shall not limit the system used for measurement, in terms of signal-to-noise ratio. Additionally, possible components and layouts for the filter box will be investigated, with costs and limitations in mind. Also, the graphical programming language Agilent VEE will be used to program a way to control the planned filter box.

## **1.5 Disposition**

This report is written with each title in the method chapter running in chronological order of what was conducted. The result chapter covers the final result, discussion and possible future plans for the project.

# **2. FRAME OF REFERENCE**

This chapter describes various terms that may not be commonly known for the reader and provides a better explanation.

## **2.1 Theoretical terms**

This section describes various terms and theory used in the project.

### **2.1.1 Spurious emissions**

Spurious emissions are unwanted radio frequencies outside the channel. The spurious emissions can consist of harmonic emissions, parasitic emissions, intermodulation products and frequency conversion products. Spurious emissions can appear in the bandwidth and outside of the bandwidth of a band. [1]

### 2.1.2 S-parameters

S-parameters, which are also known as “scattering parameters”, are used to quantify how radio frequency energy propagates through a multi-port network. S-parameters provide a means to accurately describe the properties of more complex networks as “black boxes”. For example, when a radio frequency enters on one port some part of the signal is reflected back out of the same port, some of it “scatters” and propagates through other ports, some of it might become amplified and some of it dissipates as heat or electromagnetic radiation. The S-parameters of a two-port network are generally known as:

$S_{11}$  = voltage reflection coefficient of the input port  
 $S_{12}$  = reverse voltage gain  
 $S_{21}$  = forward voltage gain  
 $S_{22}$  = voltage reflection coefficient of the output port

These parameters are often placed within a matrix (see Formula 1). [2]

$$\begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix}$$

*Formula 1: S-parameter matrix*

These parameters are used to calculate gain, insertion loss, return loss etc. For this report the most important S-parameters will be  $S_{11}$  and  $S_{21}$  which are used for insertion loss and gain.

### 2.1.3 Noise

In electronic circuits, there is thermal noise, which is generated from components in the circuit when the components have a higher temperature than 0 Kelvin. [3] This noise will negatively affect a signal, e.g. the signal from a radio transmitter.

Signal-to-Noise Ratio abbreviated “SNR”, is the ratio between signal and noise power and is usually expressed in decibels. A high SNR is important to differentiate the signal from the noise. [4] SNR is affected negatively by the Noise Factor of components; Noise Factor is the ratio of input SNR to output SNR expressed in linear. Instead of Noise Factor, Noise figure is often specified for components.

$$\text{Noise Figure} = 10\log(\text{Noise Factor})$$

*Formula 2: Noise Figure to Noise Factor conversion*

$$\text{SNR}_{dB} = 10 \log_{10}\left(\frac{P_{signal}}{P_{noise}}\right) = P_{signal,dB} - P_{noise,dB}$$

*Formula 3: SNR in dB*

### 2.1.4 Decibel-milliwatts (dBm)

Decibel-milliwatt (dBm) is a power measurement relative to 1 milliwatt, and is expressed as:

$$x = 10 \log \frac{P}{1mW}$$

*Formula 4: Watt to dBm*

And

$$P = 1mW * 10^{\frac{x}{10}}$$

*Formula 5: dBm to Watt*

Where P is the power in Watt and x is the power in dBm.

It is used to measure the absolute power because of its capability to express both large and small values in a small form. dBm is used in radio, microwave and fiber optic work. [5] 0dBm equals 1mW, 30dBm equals 1W, 40dBm equals 10W and so on. Calculating power with dBm is simple since most components specify parameters, such as insertion loss or gain, in dB. For example, an amplifier with 20dB gain will amplify a 20dBm signal to 40dBm.

$$20dBm + 20dB = 40dBm$$

In linear, using the same numbers: an amplifier with 100 gain will amplify a 0.1W signal to 10W.

$$100 * 0.1W = 10W$$

### **2.1.5 Passive Intermodulation (PIM)**

Passive intermodulation is a form of intermodulation distortion that produces interference in high frequency circuits. This can for example affect the wanted signal from a radio transmitter by hiding it or distorting it. Passive intermodulation occurs when two or more signals exist in a passive and non-linear device or element. The signals meld and mix with each other, generating a completely different signal. [6] The PIM level is related to the carrier power, an increase of 1dB carrier power approximately results in a 3dB higher PIM level. [7]

## **2.2 Electronic components**

This section describes the components used for this project.

### **2.2.1 Tuneable Filters**

For the purposes of this project, all electronic filters will be categorised as high frequency components. A tuneable filter allows the user to control a bandpass or bandreject filter by tuning where to start rejecting or letting through desired frequencies. This can be controlled by turning a small knob on the device or controlling the filter digitally, using an optional remote digital interface,

such as GPIB. [8]

### 2.2.2 Directional Coupler

Couplers are passive devices used to split a portion of the power travelling in one transmission line out through another connection or port. The coupler is a four port device consisting of an input port, an output port, a coupled port and an isolated port (See Figure 2). The main line is usually between ports 1 and 2 and is suited to carry higher power levels while port 3 and 4 are better suited for lower powers because they are intended to only carry a small proportion of the main line power. A coupler does not have set ports, any port of the 4 can be the input port, resulting in the directly connected port being assigned as the transmitted port, the adjacent port becomes the coupled port and the diagonal port becomes the isolated port. [9] For example, a 10dB coupler (See Figure 3) attenuates the power by 10db.

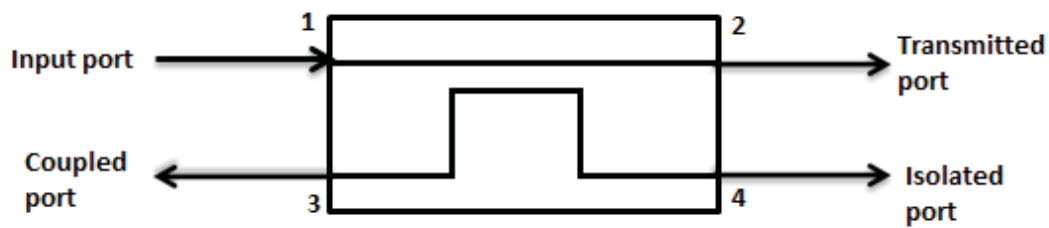


Figure 2: Directional coupler and ports

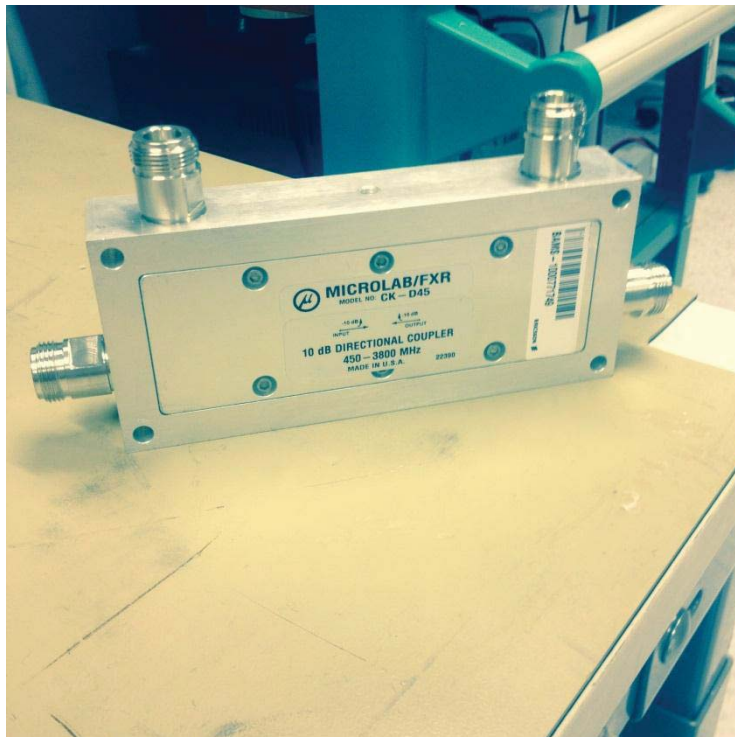


Figure 3: Directional Coupler

### 2.2.3 Switches

All switches this report refers to are electromechanical switches suited for RF and microwave applications (See Figure 4). In this report it is assumed the reader has the basic knowledge of how a switch works. However, the terms TTL and cut-off power circuit might come across as unfamiliar. TTL logic stands for “transistor-transistor-logic” and is used to enable the status of the switch to be controlled by the level of the TTL logic input. [10]

A cut off power circuit is an option on some switches that allows it to cut off the DC current on the actuator after switching, thus saving energy. [11]



*Figure 4: Revolver switch*

### 2.2.4 GPIB

GPIB, also known as ”General Purpose Interface Bus”, is a bus developed by Hewlett-Packard in the 1960s. It is used to connect and control programmable instruments and is widely used as a standard worldwide. The control of the instrument can be implemented in different ways, either with an external controller such as a GPIB-USB interface (See Figure 5) or a GPIB Plug-in Controller card. [12]



*Figure 5: GPIB-USB interface*

## **2.3 Agilent VEE**

Agilent VEE (Visual Engineering Environment) is a visual test programming environment used for tests, measurement and instrument control applications (See Figure 6). The programming language is graphical and flow driven. A developer can connect graphical high-level objects to each other and the way these objects are connected controls the flow of the application.



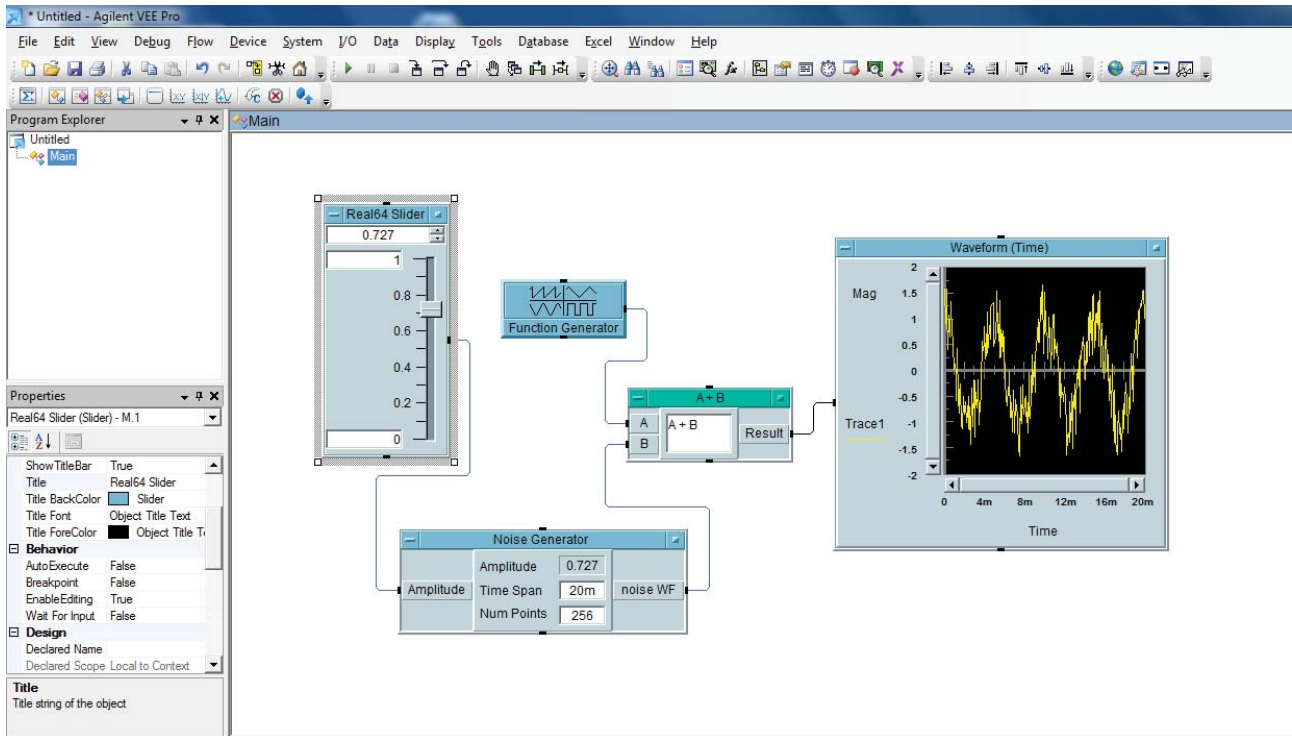


Figure 6: Example VEE application

Objects are the components used to create an application in VEE. Every single object represents programming lines and instructions used in more common programming languages, such as C or Java. An object can, once it executes, do an assortment of functions, such as displaying a graph or executing MATLAB script. In addition, a VEE program may contain user-defined objects, which are objects the user has created. These user-defined objects can also contain several existing objects. In the Agilent VEE programming environment an object can be shown in two different modes, Icon view and Open view. Icon view is where the object is minimized to cover as little space as possible on the screen, while the Open view is used to further inspect the object to get a better idea of what it contains and its instructions (See figure 7).

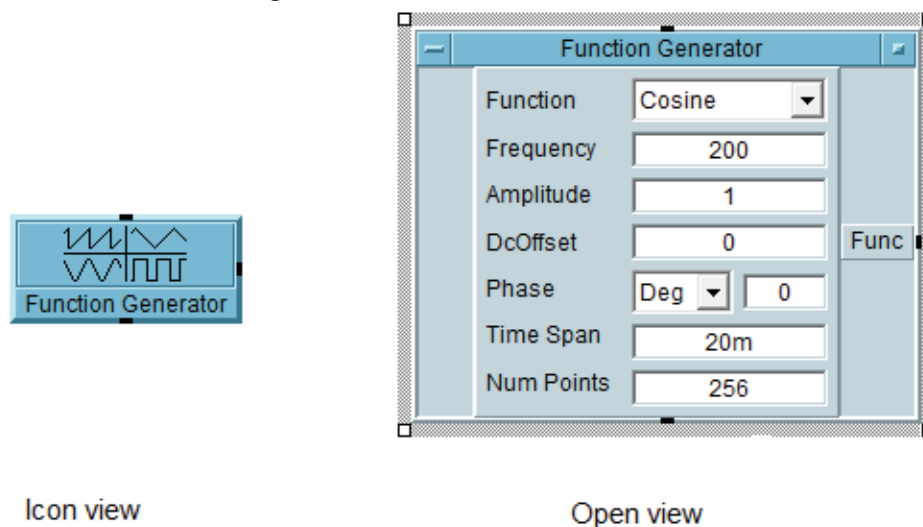
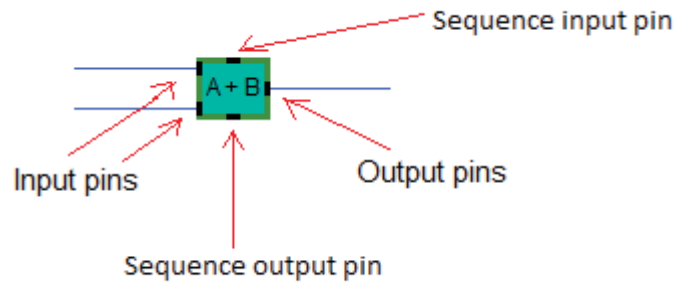


Figure 7: Object views

When objects are connected, they create a "thread". Data flows between objects in packages called "containers". The container can hold data in various forms. For example, the data can be a scalar number, an array of 500 strings or simply nil, which is an empty container. As a container of data arrives to the input pin of an object it is called "pinging" and when the container comes out at the output pin of the object the output pin is activated. There can also be pins at the top and bottom of an object. These pins are called the sequence input and sequence output pins. The sequence input pin at the top of an object, if connected, holds the execution of an object until the pin receives an empty container i.e. the sequence input pin gets pinged. The sequence output pin at the bottom of an object, when connected, becomes activated once the object and all data propagation have finished executing (See figure 8).



*Figure 8: Object pins*

The flow of data in Agilent VEE applications moves from left to right and then from top to bottom from each object. In detail, it works the following way. First, the data input pins and sequence-in pins, if connected, are pinged. Secondly, the object executes. Thirdly, the output pins are activated. Fourthly, the data propagates from left to right. Finally, the sequence out pin is activated to show that the object has finished executing and propagates an empty container from top to bottom. This output pin does not always need to be connected to something, but can be used to make sure an object starts to execute only after the sequence output pin has sent a container to the objects sequence input pin. When an Agilent VEE program is running, if there is more than one thread in the program, they will all execute at the same time.

Creating a user interface in Agilent VEE can be done by switching between panel and detail view and specifying the properties of each object, if they are going to be used for the panel view. The panel view represents the user interface and what the operator will be able to see once the application is running (See figure 9 and 10). The user can control the program with various graphical objects, representing knobs, sliders and buttons. Each object in the panel view has a corresponding object in the detail view. [13]

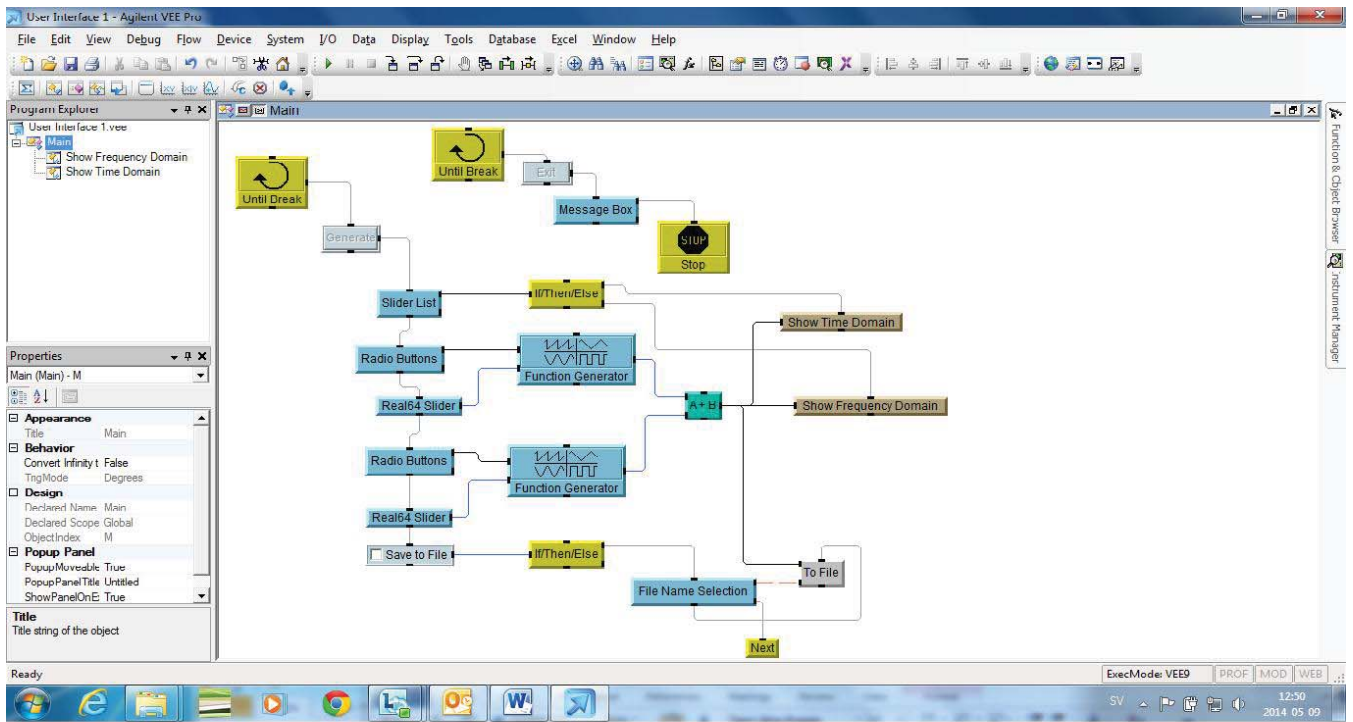


Figure 9: VEE Application detail view

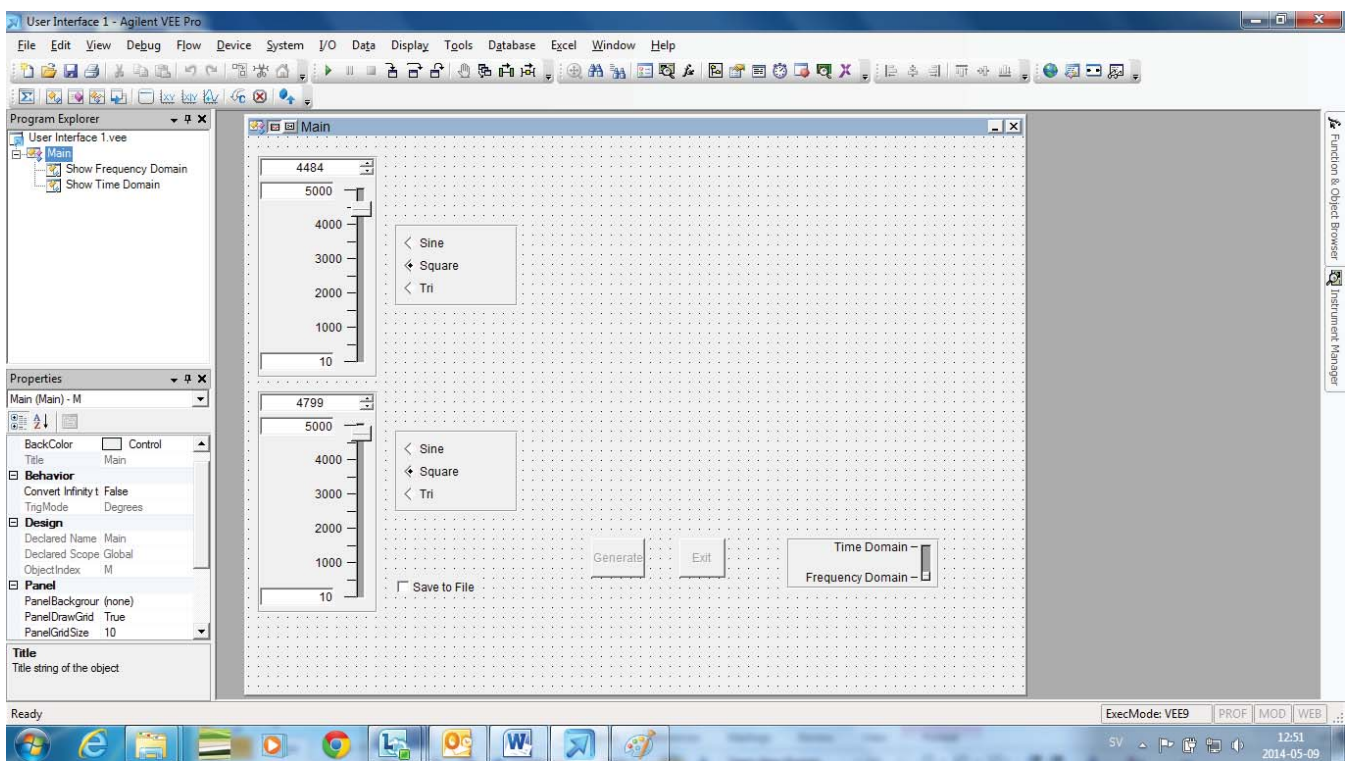


Figure 10: VEE Application panel view

## 3. PROCESS

This chapter describes the various methods and procedures used in the project.

### 3.1 Collection of basic data

First of all, research had to be made to develop a better understanding of the various measurements which the filter box was supposed to be included in. To accomplish this, several reports were studied. The documents were provided by supervisor Jörgen Ankarberg, who is working with software and hardware integration at the product design section of Ericsson. These documents consist of VS, VR and RS reports, which describe the requirements and the procedure for the tests.

For each frequency band it is of great importance that the transmission does not interfere with other frequencies outside the specified bandwidth. The test case has different requirements depending on the frequency band. [14] Ericsson measures spurious emissions for frequencies from DC up to around 13 GHz. The requirement for the amount of spurious emissions can vary depending on the band and what frequency interval that is being measured. Some intervals might have a stricter requirement while others allow a more relaxed requirement. The strictest requirement is around -115 dBm which is a very small amount of allowed spurious emissions.

### 3.2 Fundamental theory

To be able to design the filter box, the necessary background theory was necessary to learn. According to supervisor at Chalmers, Göran Hult, it is important to know how S-parameters work. Jörgen Ankarberg at Ericsson noted the importance of noise and attenuation in regards to the filter box, so these terms needed to be investigated. Another issue is so called passive intermodulation, which is difficult to estimate without physical components. See the theoretic reference for more information regarding “Passive Intermodulation”.

### 3.3 Filter box design

In order to make a filter box as general as possible, it will need to cover all frequency bands of interest to Ericsson. The bands are located at very different frequencies; from as low as 700 MHz up to 2700 MHz, therefore filters with many different frequency ranges will be required. Furthermore, since the spurious emission measurements are conducted out-of-band, it will be necessary to measure from 0 Hz up to as high as 12.75 GHz. The table below (Table 1), sent in an email from Jörgen Ankarberg, represents various frequency bands tested at Ericsson.

	UL (MHz)	DL (MHz)	Band
B0	890 – 915	935 – 960 FDD	900P
B1	1920 – 1980	2110 – 2170 FDD	2100
B2	1850 – 1910	1930 – 1990 FDD	1900
B3	1710 – 1785	1805 – 1880 FDD	1800
B4	1710 – 1755	2110 – 2155 FDD	AWS
B5	824 – 849	869 – 894 FDD	850
B6	830 – 840	875 – 885 FDD	
B7	2500 – 2570	2620 – 2690 FDD	2600
B8	880 – 915	925 – 960 FDD	900E
B9	1749.9– 1784.9	1844.9–1879.9 FDD	17/1800
B10	1710 – 1770	2110 – 2170 FDD	
B11	1427.9–1452.9	1475.9–1500.9 FDD	1500
B12	698 – 716	728 – 746 FDD	700
B13	777 – 787	746 – 756 FDD	700
B14	788 – 798	758 – 768 FDD	700
B17	704 – 716	734 – 746 FDD	700
B20	832 – 862	791 – 821 FDD	800DD
B25	1850 – 1915	1930 – 1995 FDD	1900G
B33	1900 – 1920	1900 – 1920 TDD	
B34	2010 – 2025	2010 – 2025 TDD	(A-band)
B35	1850 – 1910	1850 – 1910 TDD	
B36	1930 – 1990	1930 – 1990 TDD	
B37	1910 – 1930	1910 – 1930 TDD	
B38	2570 – 2620	2570 – 2620 TDD	(D-band)
B39	1880 – 1920	1880 – 1920 TDD	(F-band)
B40	2300 – 2400	2300 – 2400 TDD	
B41	2496 – 2690	2496 – 2690 TDD	(Sprint)

*Table 1: Bands and frequencies*

He also mentioned that the more interesting bands for the spurious emission measurements are B1, B3, B7, B8, B12 and B13. UL (uplink) corresponds to the receiver frequencies for that particular band, while DL (downlink) is the transmitter frequencies.

To settle what was needed of the filter box, input from Ericsson was necessary to define the requirements. A requirement specification was written based on those requirements (See Appendix A). Various datasheets for filters were studied to determine if they fulfill the requirements for the planned filter box. To make the filter box even more general, tuneable filters were investigated, as they would allow sweeping across frequencies. Using tuneable filters would in theory allow for a more general configuration that can be used for a wider variety of measurements, and not only the OOB TX measurements which is the main purpose of the filter box. In addition, the total amount of components needed for the filter box is likely to be reduced by using tuneable filters. All components, which are going to be used for the planned filter box, will contribute with an amount of noise and attenuation which will need to be calculated for the entire system. The cost for each component will also need to be taken into account. As the final system configuration will need to be reasonably sized, approximations on size had to be made. For the different components, contact was established with manufacturers and distributors, in order to inquire about the prices and further specification of the components.

### 3.3.1 Filter box specification

The requirements for the filter box were determined by discussing with the supervisor at Ericsson and reading the various documents related to measurements. To be able to measure signals at -

115dBm with a SNR of >5dB, the signal first needs to be amplified to -85 dBm or higher, as the noise floor of the spectrum analyser used at the product design section is around -90dBm at a resolution bandwidth of 100kHz. Additionally the PIM of components will have to be taken into account so that the SEM from the DUT can be differentiated from the intermodulation (IM) products caused by the filter box. The received constant wave can have an average power of up to 100W which is more than most components can handle. To prevent breaking any components, a coupler will have to be used to lower the signal power to 10W or less before it enters the filter box. All components should have an impedance of 50Ω to minimize reflections caused by unmatched impedances. Frequencies measured vary from 0 Hz up to 12.75 GHz, with the relevant bands in the 700 MHz to 2700 MHz range.

Using the frequencies for the previously mentioned range, a set of three ranges were written down (Table 2) in order to get a better perspective of the specifications needed for tuneable filters. The start number was obtained using the band with the lowest starting frequency within that range, while the stop number represents the highest frequency. The bandwidth (BW) is the minimum and maximum bandwidths for the given range. A list of requirements for the filter box was specified using the assumptions above. (See Appendix A for the filter box requirements)

Start	Stop	BW (Mhz)
699	960	10-35
1710	2170	45-75
2500	2690	70

*Table 2: Possible filter ranges*

### 3.3.2 Selecting filters

Using the table of possible filter ranges (Table 2), a number of different filters were found at K&L Microwave. [15] Among these, tuneable band reject and bandpass filters were included. The tuneable filters are able to sweep over frequencies while the non-tuneable ones cover specific bandwidths. Many of the filter datasheets stated that they were able to be digitally controlled, which according to Martin Hedin and Samir Kilim, at Ericsson, would work with Agilent VEE, but instrument drivers would need to be written for the tuneable filters in order to control them as the filters are not included in standard libraries of Agilent VEE. Instrument drivers are interfaces which allow the instrument to be controlled remotely from the PC. [16]

The idea of using a separate bandreject filter for each band was discarded due to the following reasons; Size, cost and inflexibility. Regarding size, it is of interest to keep the box as compact as possible. Using one filter solely for the purpose of covering a single band significantly increases the number of filters needed, compared to using a tuneable filter to sweep over frequencies, thus covering several bands.

When it comes to cost, it is assumed more filters results in a higher cost, even though tuneable filters are individually more expensive. Finally, the use of non-tuneable filters would result in a configuration where the only variable part is the externally connected components; which decreases flexibility of the filter box.

By looking at different data sheets for an assortment of tuneable filters, the tuneable notch filters were also rejected as the sweeping range was too small, therefore many different filters would still

be needed. Furthermore, while the centre frequency is tuneable, the bandwidth is not, so it could not match all bands within the sweeping ranges, for some bands it was too narrow, whereas for others it was too wide. The bandwidth of the bands varies between 10MHz and 75MHz, while the 3dB BW for the tuneable notch filters in the relevant frequency range varies between 6MHz and 27MHz, i.e. to attenuate the carrier, more than 4 cascaded filters would be needed for a particular band.

With both types of notch filters out of the picture, tuneable bandpass was investigated. Sweeping the bandpass filter outside of the band, with the band in the filters stopband, would allow for more flexibility as it does not rely on the filter having a specific bandwidth. With this idea, and the much wider frequency ranges of the bandpass filters, only a few filters would be needed to cover most, if not all, bands in the requirement specification.

In addition to covering as many bands as possible, the filters also needed to fulfil the requirements for stopband attenuation; attenuating the carrier so that the SEM can be measured by the spectrum analyser, as well as being able to measure as close to the carrier as possible.

With a stopband attenuation of 50dB, enough to bring a 10W carrier down to 0.1mW, the tuneable filters which were looked into should handle the first requirement if the filter is considered ideal. However, in reality, no filter is ideal. Additionally a drawback with having the flexibility of tuning is that the shape factor of a tuneable filter is not as good as a non-tuneable filter. The reason for this is that tuneable filters as of currently have a lower order than normal non-tuneable filters. This affects the stopband negatively and measuring close to the carrier might become a limitation. Regardless, it was decided that using two tuneable filters, for 0.5-1GHz and 1.5-3GHz respectively, as a base for the filter box and search for filters complimenting them.

Having covered all bands, except for two very low priority ones, within the range of both tuneable filters, only three more filters would be needed for measurements in the full range of DC-13GHz; a lowpass filter for DC-0.5Ghz (See Figure 11), a bandpass filter for 1-1.5Ghz (See Figure 12) and a highpass filter for 3-13GHz (See Figure 13). Considering where the bands lie, each filter was quoted to a manufacturer. The following were the specifications sent to the manufacturer, with additional comments on why these specifications were requested:

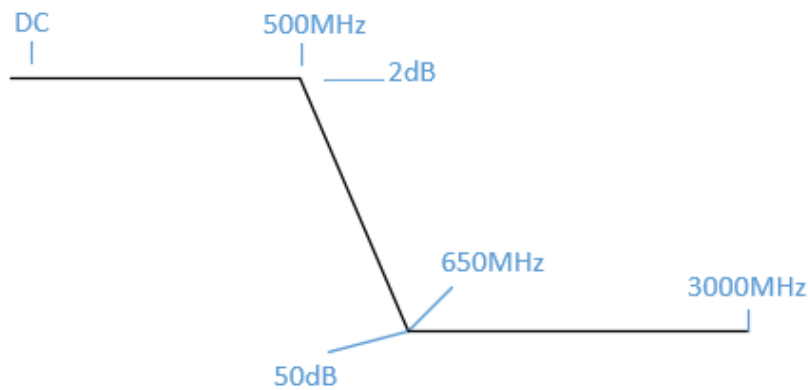
*All filters able to handle 10W CW.*

This is the highest power components need to handle if a 10dB coupler is used.

*Lowpass*

*Passband insertion loss: 0-500MHz 2dB*

*Stopband attenuation: 650-3000MHz 50dB*



Figur 11: Requested Lowpass filter frequency response

The passband covers the frequencies up to the where the first tuneable bandpass filter operates, the stopband has some margin up to 699MHz which is where band B12 starts.

*Bandpass*

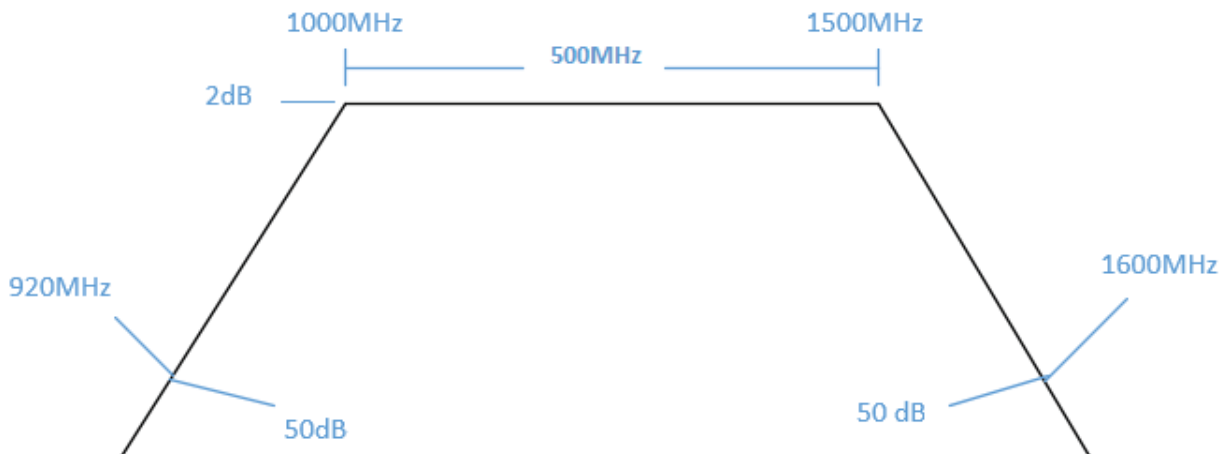
*Centre frequency: 1250MHz*

*Bandwidth: 500MHz*

*Passband insertion loss: 1000-1500MHz 2dB*

*Stopband attenuation: 0-920MHz 50dB*

*Stopband attenuation: 1600-3000MHz 50 dB*



Figur 12: Requested Bandpass filter frequency response

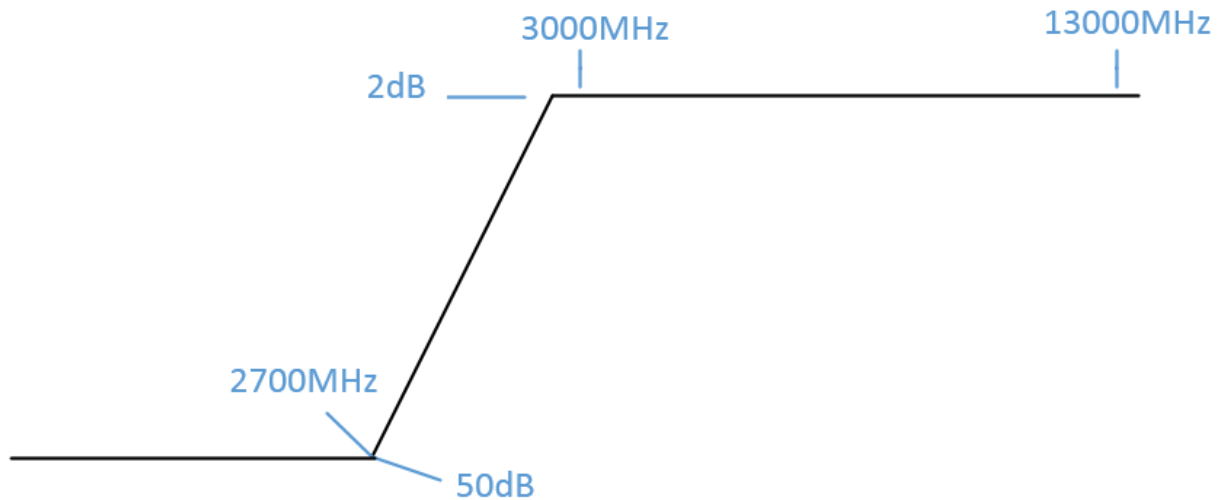
Passband covers the frequencies between the tuneable filters' range. The lower stopband includes Band 8 uplink; however the filter is not steep enough to include the downlink of the band, which stops at 960MHz. Upper stopband at 1600MHz leaves ample room for band 3 that start at 1710MHz. Note that band 11 and 21 is inside the passband of this filter. These are the two bands previously mentioned as low priority and are not critical for the main application of the filter box.



*Highpass*

*Passband insertion loss: 3000-13000MHz 2dB*

*Stopband attenuatino: 0-2700 MHz 50dB*

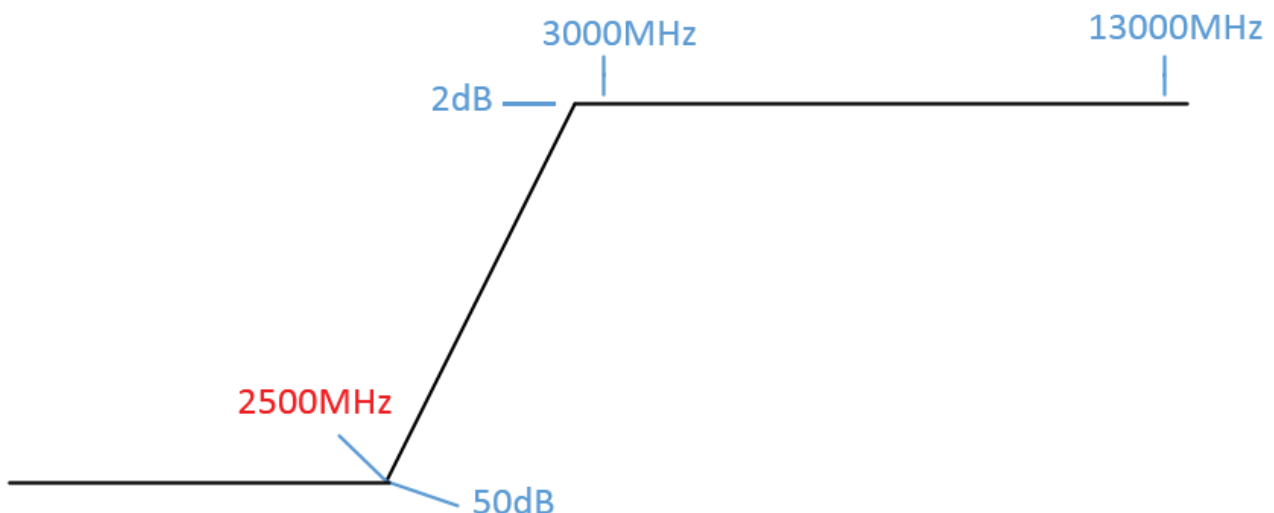


*Figur 13: Requested Highpass filter frequency response*

The passband covers the remaining frequencies up to 13GHz and the stopband works for all relevant bands, the closest being the downlink of band 7 at 2690MHz.

The specifications sent covers all required bands for TX, but misses out on the RX of band 8), it also includes all other bands except for 11 and 21. If measurements are to be made on those bands, an external filter will have to be connected.

The specifications returned from the manufacturer matched the requested specifications, with the exception of the highpass filter which had the following frequency response (See Figure 14):



*Figur 14: Actual Highpass filter frequency response*

Having the stopband at 2700MHz was not possible and was changed to 2500MHz; resulting in support for B7, TX 2500-2570MHz and RX 2620-2690MHz, being excluded for frequencies over 3GHz without the use of an external filter.

### 3.3.3 Selecting amplifiers

According to supervisor Jörgen Ankarberg, it was likely for the filter box configuration to use an amplifier in the signal path to make the signal readable. Typically an amplifier is placed first in a cascaded system to increase SNR compared to amplifying at a later stage. However, for the filter box, if the amplifier is placed so it amplifies the signal before the carrier is attenuated; the other components would be destroyed. The spectrum analyser at Ericsson has a noise floor around -90dBm, to be able to measure SEMs as low as -115dBm they have to be amplified first.

Considering the signal is coupled by a 10dB coupler before entering the filter box, the SEMs are down to -125dBm. Insertion loss and cables attenuate the signal further, resulting in a power around -135dBm, depending on path and frequency. For a SNR over 5dB an amplification of 50dB or more is required. To leave some room for error, an amplifier with 55dB gain was selected. The insertion loss of the amplifier is relevant as it affects the attenuation; however the amplifiers found with sufficient gain to fit the requirement had quite high insertion loss compared to amplifiers with lower gain, so the insertion loss had to be accepted regardless.

### 3.3.4 Selecting switches

To choose the signal path through the filter box, high frequency switches are needed. By reading excel-sheets with existing filter box configurations provided by Ericsson, a few options and manufacturers were found. Four switches, two with six input ports and two with four input ports, are required for the envisioned setup. These ports connectors should ideally match the connectors of the components, ensuring that no loss of signal power due to mismatched connector types occurs. Since the signal path through the box, regardless of frequency and power, passes all switches, they need to handle the full frequency range, DC-13GHz, as well as 10W CW. An additional property to consider is that PIM levels should be as low as possible. When investigating the control of switches, Samir Kilim at Ericsson stated that the switches were able to be integrated with Agilent VEE to allow digital control. Including TTL logic and cutoff power circuits would improve usability and lower power consumption. He also noted that adding an indicator to the switch would help the testers verify that the correct switch is activated. When contacting a seller on these matters, each of the added attributes would increase the price of the switches, but even with all options selected it would still be within reason.

### 3.3.5 Additional components

The use of couplers will be required for some measurements, but they will be connected to the input port of the filter box. This makes it possible to use components with lower power handling than 100W, as the coupler attenuates the power of the signal before it enters the filter box.

An attenuator will be used with the automatic measure algorithm (presented in 3.4.4) to prevent the spectrum analyser from breaking when tuning the filters. Additionally, according to Jörgen Ankarberg, a test setup for spurious measurements in-band usually features a path with around 50dB attenuation, so having the choice of using an attenuator instead of an amplifier can be useful to make the filter box more flexible, thus a 40-50dB attenuator will be included in the filter box.

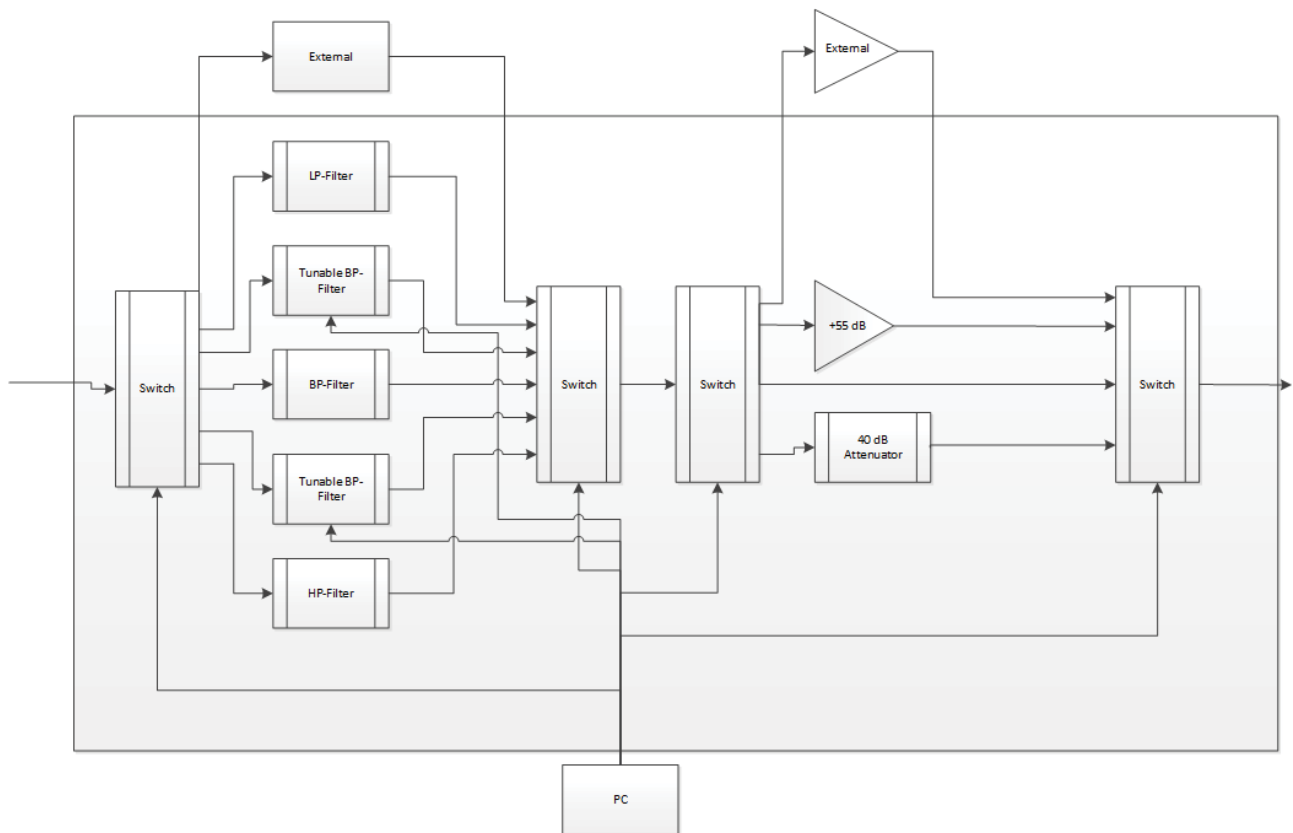
To connect all components with each other, radio frequency coaxial cables are going to be used. In a fixed setup like the filter box, semi-rigid cables can be useful. They generally offer better electrical

properties than flexible cables, but at the expense of not being formable. [17] Even so, the flexible type has previously been used in filter boxes for specific bands at Ericsson and consequently should offer satisfactory properties. Moreover, since no design and layout of the inside of the box is confirmed, only the flexible kind will be considered as they can be used almost regardless of how the inside is configured. It is important that the cables have the right connectors; hence they will have to be specified after all other components are chosen so everything matches. Also of importance is the PIM generated by the cables, it cannot be higher than the lowest requirement for SEM from the DUT; otherwise the PIM might be mistaken for SEM.

Should the filter box, with the proposed components, be insufficient for a measurement, one or two external components can be connected, one instead of a filter and one instead of the amplifier or attenuator.

### 3.3.6 Visualisation of the filter box

After the decision on components was complete, a schematic of the filter box was created (See Figure 15). A connection without a component between the two last switches is included in case no gain is necessary for the measurements. Furthermore, Jörgen Ankarberg noted that it is good to have the option of a straight path through the box, though the type of switches used can have a maximum of six input ports so no such path exists between the first two switches. It is, however, possible to connect a cable instead of an external component, thus the option of a non-modified path exist.



Figur 15: Filter box configuration

### 3.3.7 Noise and attenuation calculations

The noise figure of passive components is equal to their attenuation i.e. the attenuation is equal to the insertion loss of each component. [18] Using this information together with the already provided insertion loss and gain of the amplifier, the total attenuation and SNR of the selected components can be calculated to examine if the components match the requirements. The cascaded attenuation for the filter box is calculated with Friis formula for noise factor (See Formula 6):

$$F_{total} = F_1 + \frac{F_2 - 1}{G_1} + \frac{F_3 - 1}{G_1 G_2} + \dots + \frac{F_n - 1}{G_1 G_2 \dots G_{n-1}}$$

*Formula 6: Friis formula for noise factor*

Where  $F_n$  is the noise factor and  $G_n$  is the gain of a component. The attenuation of the box will vary depending on the frequency; a higher frequency generally equals a higher attenuation. Cables can have a large impact on attenuation, especially at high frequencies. Since cable lengths between components are not known, no exact calculations can be made. Presented here are the best-case and worst-case scenarios for unwanted attenuation without regards to cabling.

Best-case scenario: Frequency at 1-1,5GHz means the switches operate at their best insertion loss (IL), 0.2 dB, while also allowing the use of the filter with the lowest IL, 0.3dB, the non-tuneable bandpass filter.

$$F_{Best} = 1.0471 + \frac{1.0715-1}{0.955} + \frac{1.0471-1}{0.955*0.9333} + \frac{1.0471-1}{0.955*0.9333*0.955} + \frac{1.9953-1}{0.955*0.9333*0.955*0.955} + \frac{1.0471-1}{0.955*0.9333*0.955*0.955*316227.766} = 2.4545$$

Converting Noise Factor to Noise Figure:

$$Noise\ Figure = 10\log 2.4545 = 3.9dB$$

Worst-case scenario: Frequency at 13GHz results in the worst IL, 0.5dB, for the switches and using the highpass filter, which is tied with the tuneable filters for the worst IL at 1dB:

$$F_{Worst} = 1.1220 + \frac{1.2589-1}{0.8912} + \frac{1.1220-1}{0.8912*0.7943} + \frac{1.1220-1}{0.8912*0.7943*0.8912} + \frac{1.9953-1}{0.8912*0.7943*0.8912*0.8912} + \frac{1.1220-1}{0.8912*0.7943*0.8912*0.8912*316227.766} = 3.6465$$

Conversion to dB:

$$10\log 3.6465 = 5.62dB$$

As seen by the equations, there is a notable difference in attenuation between best- and worst-case even without taking the cabling into consideration. However, to investigate the cable influence on attenuation, an average of 30cm cable between stages was assumed, which including input port to the first switch and the last switch to output totals 210cm. Using the formula for attenuation provided by cable manufacturer Huber+Sunher (See Formula 7):

$$\text{Attenuation: } a * f^{0,5} + b * f \text{ dB/m}$$

*Formula 7: Attenuation formula*

Where “f” is frequency in GHz and “a” and “b” are coefficients specified for the cable.  
 For the “SUCOFORM\_141\_CU” cables considered for the box:

$$a = 0.355$$

$$b = 0.04$$

At 0.5GHz and 210cm :

$$0.355 * 0.5^{0,5} + 0.04 * 0.5 = 0.27\text{dB/m}$$

$$2.1\text{m} * 0.27\text{dB/m} = 0.567\text{dB}$$

At 13GHz and 210cm:

$$0.355 * 0.513^{0,5} + 0.04 * 13 = 1.8\text{dB/m}$$

$$2.1\text{m} * 1.8\text{dB/m} = 3.78\text{dB}$$

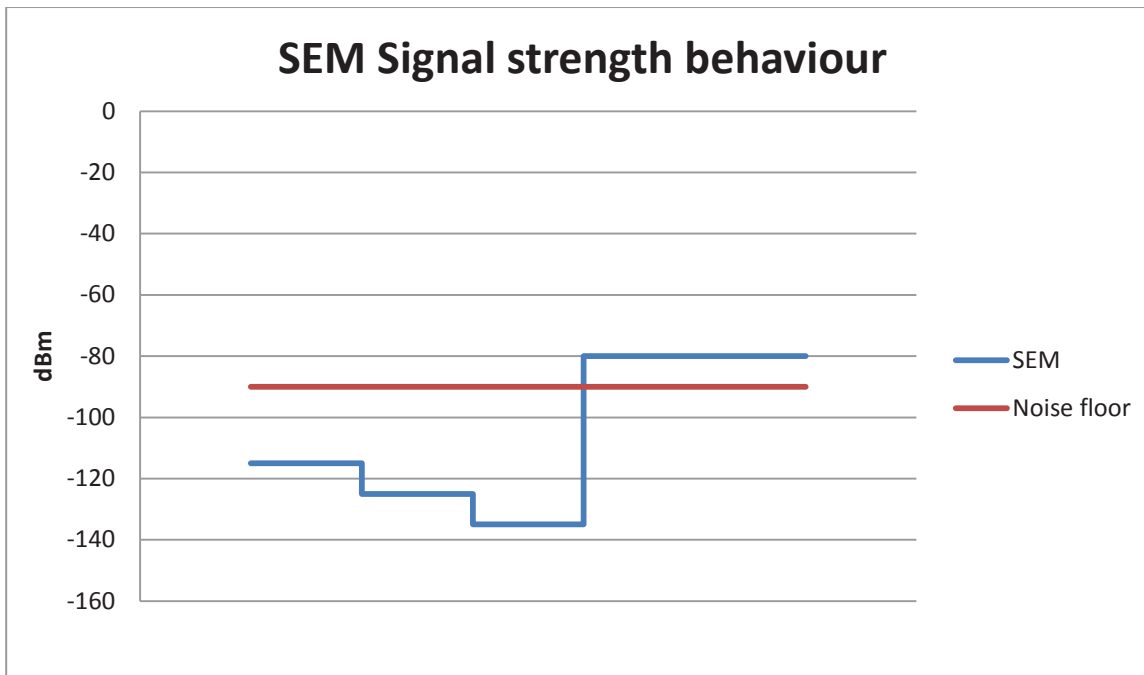
In the worst case scenario of noise factor for the filter box the value is 5.62dB and the worst case scenario for cables is 3.78dB. Adding these values gives a total of 9.4dB attenuation. Assuming the filter box is receiving a signal of -115 dBm, it is then coupled by 10dB resulting in -125dBm. From the components and cables the signal is further attenuated to -134.4dBm. At this point the signal needs to be amplified in order to be distinguishable. The 55dB amplifier increases the signal to -79.4dBm, which is above the noise floor at -90 dBm. With these values the SNR can be established.

$$SNR_{db} = (-79.4) - (-90) = 10.6 \text{ dB}$$

As can be seen from this calculation, the signal is 10.6 dB stronger than the noise at the worst case scenario with a signal at -115 dBm and the total attenuation of 9.4 dB.

As noted above, these values are just to acquire an idea of what attenuation to expect from the cabling and will most likely differ slightly when compared to reality.

Below is a graph displaying how the spurious emissions signal power changes as it passes through the filter box. When the strictest spurious emissions signal strength is unmodified their level is at -115 dBm (See Figure 16).



Figur 16: SEM Signal strength behaviour

### 3.3.8 Intermodulation

Components used in these calculations were specified at 43dBm carrier while calculations are made at 40dBm, therefore the PIM levels will be slightly better compared to the specified level.

The weakest spurious emission that is to be measured has a power of -115dBm, and the strongest carrier is 50dBm CW. 50dBm is too much for most components in the filter box, so coupling a carrier with a 10dB coupler to lower its maximum power to 40dBm is needed while also lowering the SEM to -125dBm. With the carrier at 40dBm, using cables and switches specified to -160dBc PIM at 43dB CW would result in around -129dBm passive intermodulation products, which is too much for the -125dBm signal to be consistently measurable due to the SNR being lower than 5dB. Measurements on the strongest CWs would therefore need additional attenuation to lower the PIM levels. In contrast, using cables and switches with -130dBc PIM would result in -99dBm PIM products, which is not low enough to measure the weak SEMs even with further attenuation. This leads to the -160dBc PIM components being required before the carrier has been attenuated by a filter. After the signal has passed through a filter, the carrier should be attenuated to -10dBm or less, which means a -130dBc PIM level should be more than sufficient for the remaining components, see calculations below.

$$100W = 50dBm$$

*The signal is coupled by 10dB*

$$40dBm = 10W$$

*10W Signal passes through a cable or switch, resulting in PIM*

$$-130dBc \text{ PIM cable} \rightarrow -99dBm \text{ IM products}$$

*−160dBc PIM cable → −129dBm IM products*

*Signal passes through a filter with a minimum of 50dB attenuation in the stopband.*

*40dBm − 50dB → −10dBm = 0,1mW*

*0,1mW Signal passes through a cable or switch, resultning in PIM*

*−130dBc PIM switch → −149dBm IM products*

*−160dBc PIM switch → −179dBm IM products*

### **3.3.9 Size calculations**

After deciding on the components to use in the box based on technical attributes, such as IL and gain, size was taken into account. Height, width and length of all components were noted and they were regarded as blocks for the purpose of determining the total space required to fit them inside a box. At first, they were simply considered to be arranged in accordance to the visualisation in Figure 15, except with no space in-between components for air or cables.

Since all components are placed in one layer, the height is equal to the height of the tallest component, which is the switch. (See appendix B for component specifications)

*Height: 51.054mm*

For width, every stage was calculated separately and the highest value was used.

*Width switch: 51.054mm*

*Width filters: 73 + 137 + 12.7 + 19.09 + 78.76 = 320.55mm*

*Width Amplifiers and attenuators: 31.496 + 41.15 = 72.646mm*

As seen from the calculations above, the filter widths give the total width of the layer.

The length was calculated by simply adding the lengths of the longest component in every stage, resulting in:

*Length: 69.342 + 249 + 69.342 + 69.342 + 141.7 + 69.342 = 668.068mm*

As shown by the calculations, placing the components in this manner results in a box with the measurements of 51.054x320.55x668.068mm, yielding a total volume of 10,93 litres.

An existing filter box in the lab was measured to 220x450x650mm, or 64.35 litres. Since the existing box is roughly 6 times as spacious, it was assumed the chosen components would most likely fit in a similar case, even including cables and room for ventilation. Note that this configuration does not have any power supply as it had not been looked into at this point, nor does it include any controller for the switches. The existing box is mounted in a 19” rack, so keeping the width the same would allow the new box to be easily fitted in the same type of rack. Worthy of note

is that the filter box in the lab protrudes a bit though the backside of the rack, which is 600mm deep. According to Jörgen Ankarberg at Ericsson it is not a problem if the box protrudes a little, but keeping the filter box within the rack dimensions is preferable.

### **3.3.10 Filter box cost**

After establishing contact with manufacturers and distributors, the costs for the components were written down and calculated. The prices will not be documented in the report as they are considered confidential by Ericsson.

## **3.4 Agilent VEE Programming**

This part of the method chapter covers the development of the user interface for the control of the filter box. The application was written in the Agilent VEE programming language.

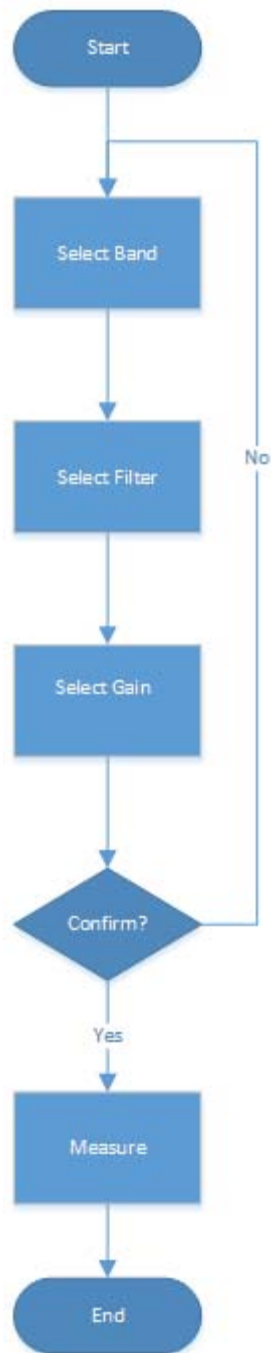
### **3.4.1 Learning the basics**

The programming language Agilent VEE was studied by reading and solving problems in the form of small exercises to teach the user how the basic functions work and what the language is capable of. Experienced programmers of VEE were consulted at Ericsson in order to further understand the language. In addition, the programming software and the exercises were provided by Ericsson.

### **3.4.2 Flowchart for the application UI**

For the programming of the user interface, a flowchart was drawn in order to understand how the flow of the application was going to work (See Figure 17). The user needs to be able to select which band that is going to be used for the configuration. Additionally, the ability to change the configuration of the filter box by choosing the signal path is necessary. This is done by selecting which filter/external component to be used along with attenuation/gain/external components. Once a configuration has been selected, the user is prompted if the configuration is correct. If confirmed, the user is able to start the measurement. Otherwise, the user can make a new selection for the configuration.





*Figure 17: Flowchart for the application*

### 3.4.3 Programming control for the filter box

With the help of the flowchart, a user interface application was developed for the filter box. However, due to the fact that no physical filters were available to be programmed, stubs were instead used. Stubs are stand-ins for not yet implemented modules in the code, which in this case would be the filters, amplifiers and switches since there were no physical components to apply the control to. In addition, a stub was used to simulate the start of a measurement. [19] The features of this program are the ability to choose which filter and amplifier to be used for the signal path for the measurement and the ability to tune the tuneable filters. All selectable components in the user interface matches the ones discussed in previous chapters.

The picture below (Figure 18) shows the application running and what options that is available for the user.

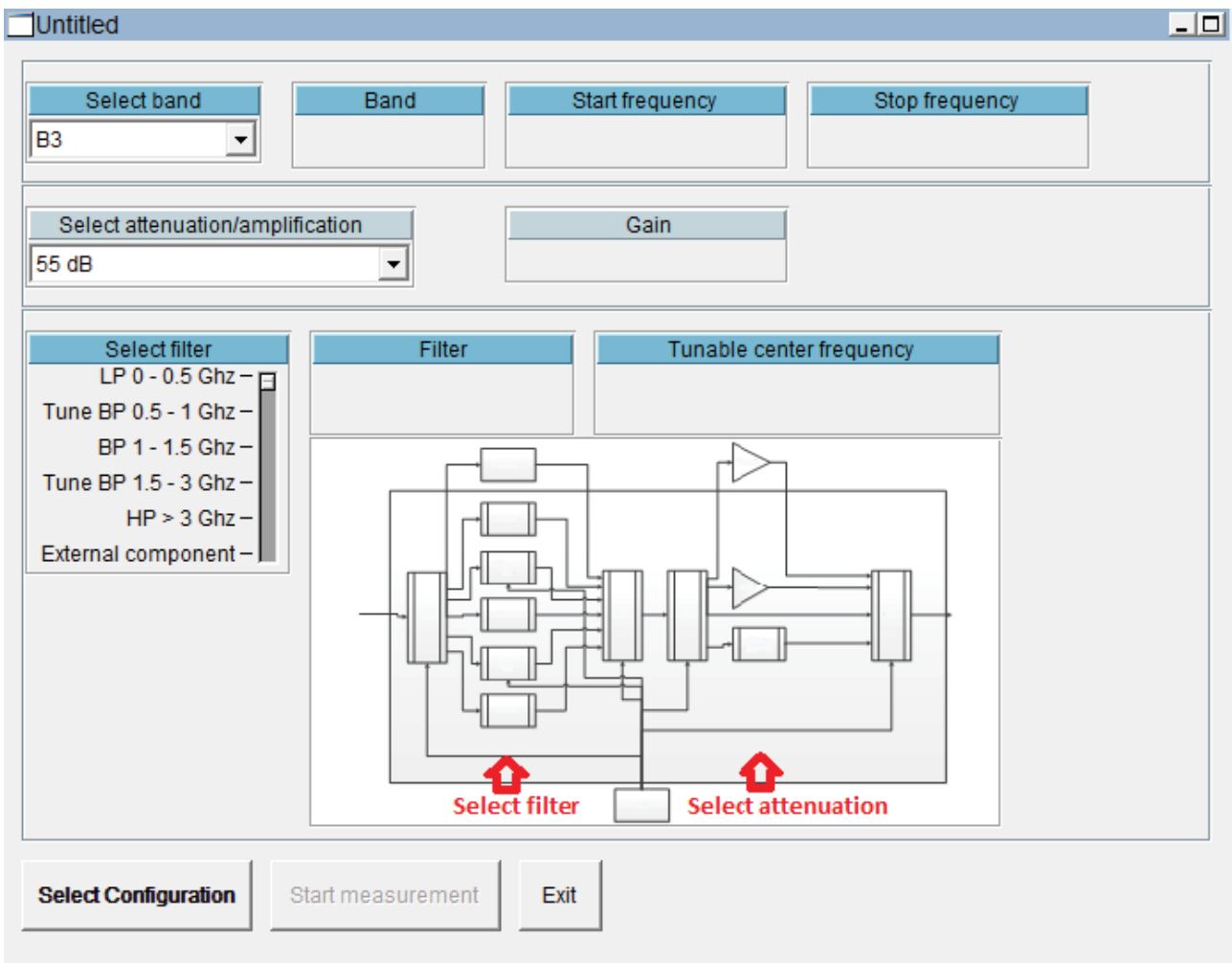


Figure 18: Filter box control interface

In the program, the user is able to select what band, filter and attenuation he wants to use for the measurement from three dropdown menus. Compared to the flowchart in the previous section, these options do not need to be chosen in a specific order. A picture with components, representing the inside of the filter box, is used to inform the user where his selections take place in the filter box marked with red arrows. To start a measurement, the user must have selected a band, a filter and attenuation, if any, followed by pressing the “Select Configuration” button to confirm his choices. When pressed, all options selected will be displayed in their respective labelled windows. The selected band along with its start and stop frequency will be displayed in “Band”, “Start frequency” and “Stop Frequency”. The selected filter will be displayed in the “Filter” window along with, if the filter is tuneable, its tuneable centre frequency. Finally, the chosen attenuation or amplification will be displayed in the “Gain” labelled window. The user is then prompted to confirm his selected options for the measurement. If the user made a mistake or wishes to change the selection, selecting “no” in the prompt allows the user to make new choices and then press “Select Configuration” again. If the user is content with his selection; he selects “yes” and the “Start measurement” button becomes activated, allowing the user to press it. The picture below (Figure 19) displays an example of a user confirming a selected configuration.

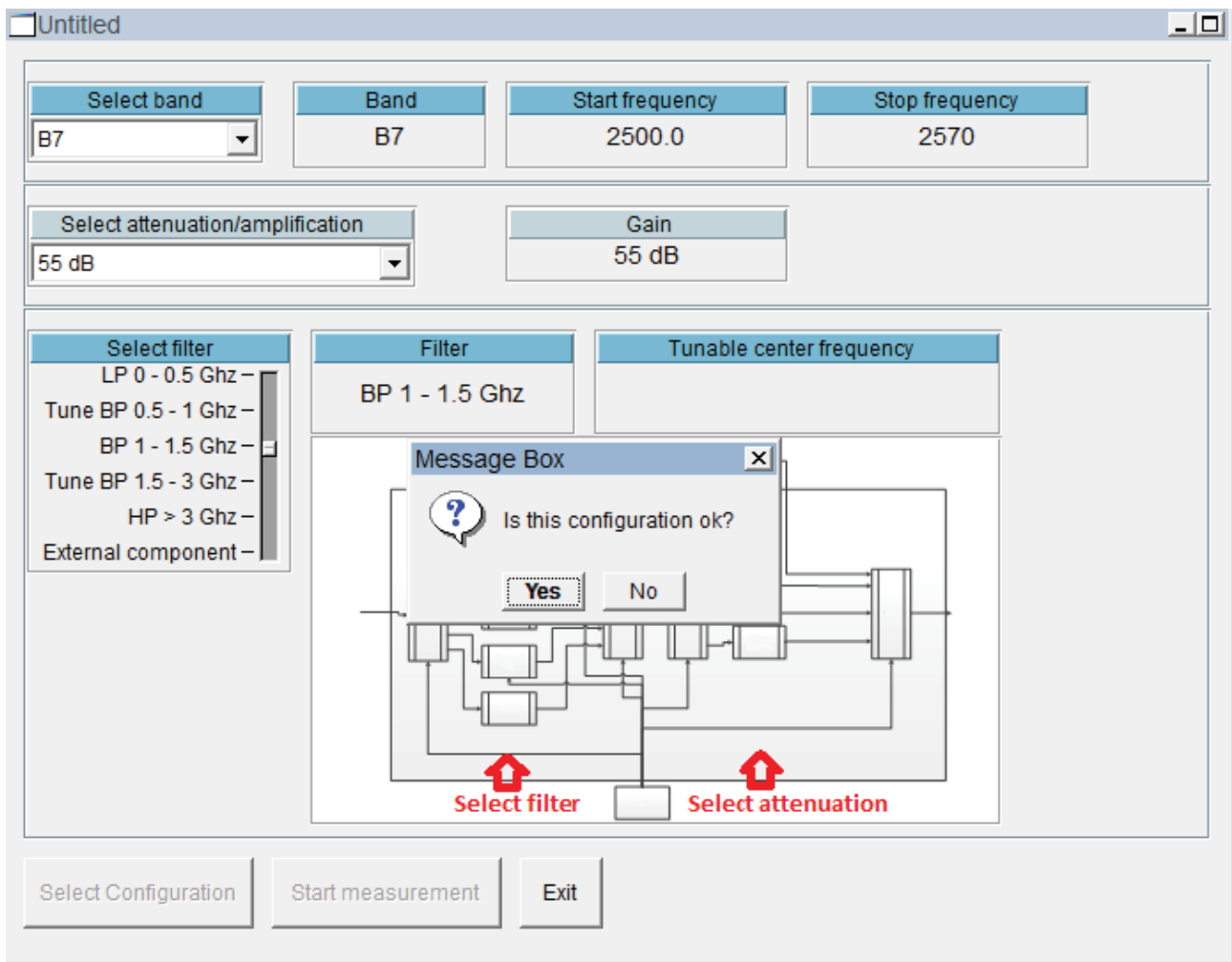
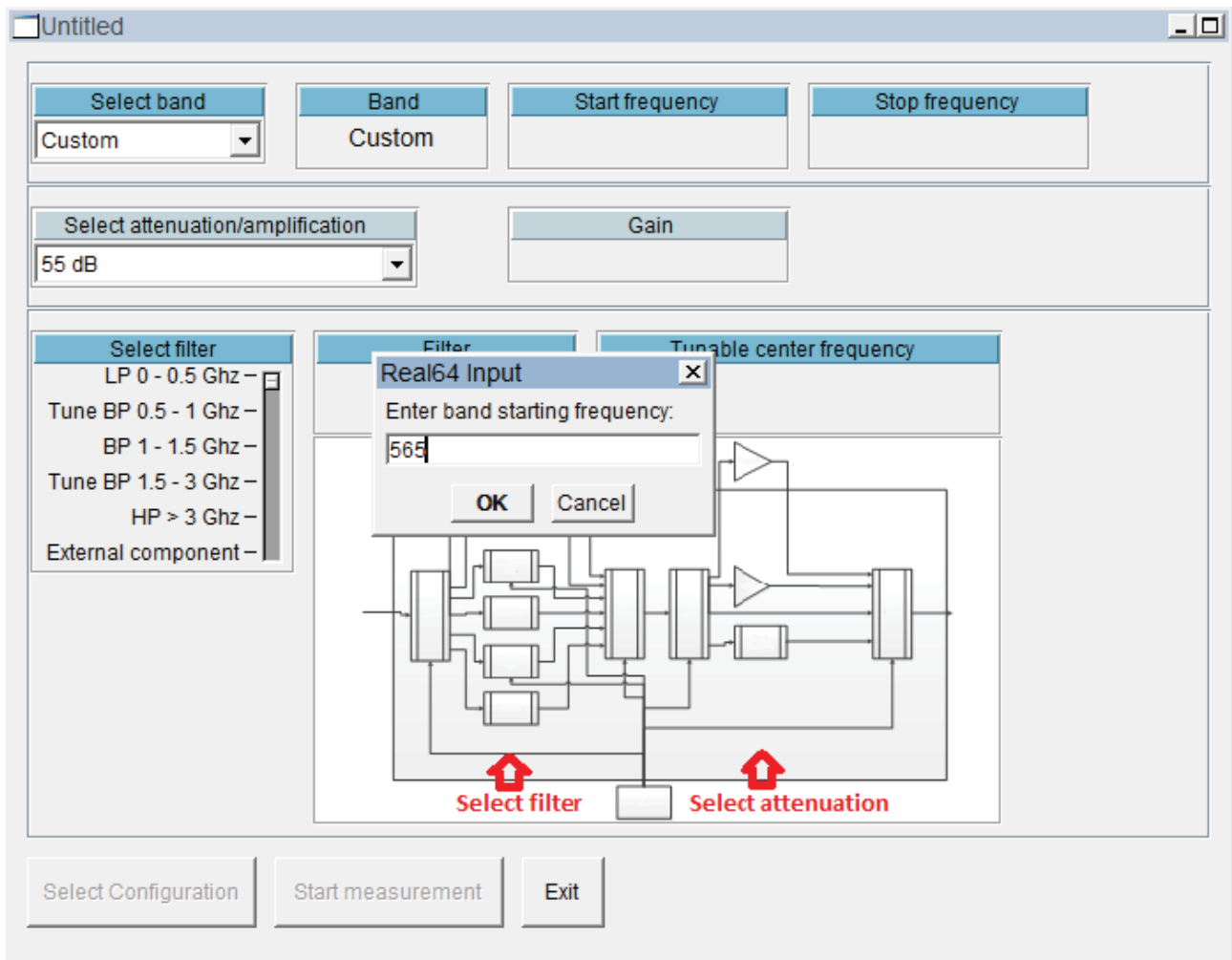


Figure 19: Confirming a configuration

The different selections and options will now be explained in more detail. From the “Select Band” dropdown menu, the user is able to choose between predetermined bands or if the user does not find the choice he is looking for, he can select the “Custom” option from the dropdown menu, allowing him to specify the start and stop frequency for the band he wants to measure. After pressing the “Select Configuration” after selecting the “Custom” option, the user gets a prompt where he first enters the starting frequency of the band, followed by a prompt for the stop frequency. The picture below (Figure 20) shows an example of the user entering a start frequency for the custom band selection.



*Figure 20: Entering a custom band*

The “Select attenuation/amplification” menu allows the user to choose between using an amplifier of 55 dB, an attenuator of 40 dB, a straight signal line or simply an external component such as a different amplifier or attenuator.

For the selection of filters, a vertical slider is used to let the user choose what filter that is going to be used for the measurement. Two of the selectable filters are tuneable, when either is chosen and confirmed with the “Select Configuration” button, the program will prompt the user to enter a value, which sets the centre frequency for the tuneable filter. The picture below (Figure 21) shows a user entering a value for the selected tuneable filter.

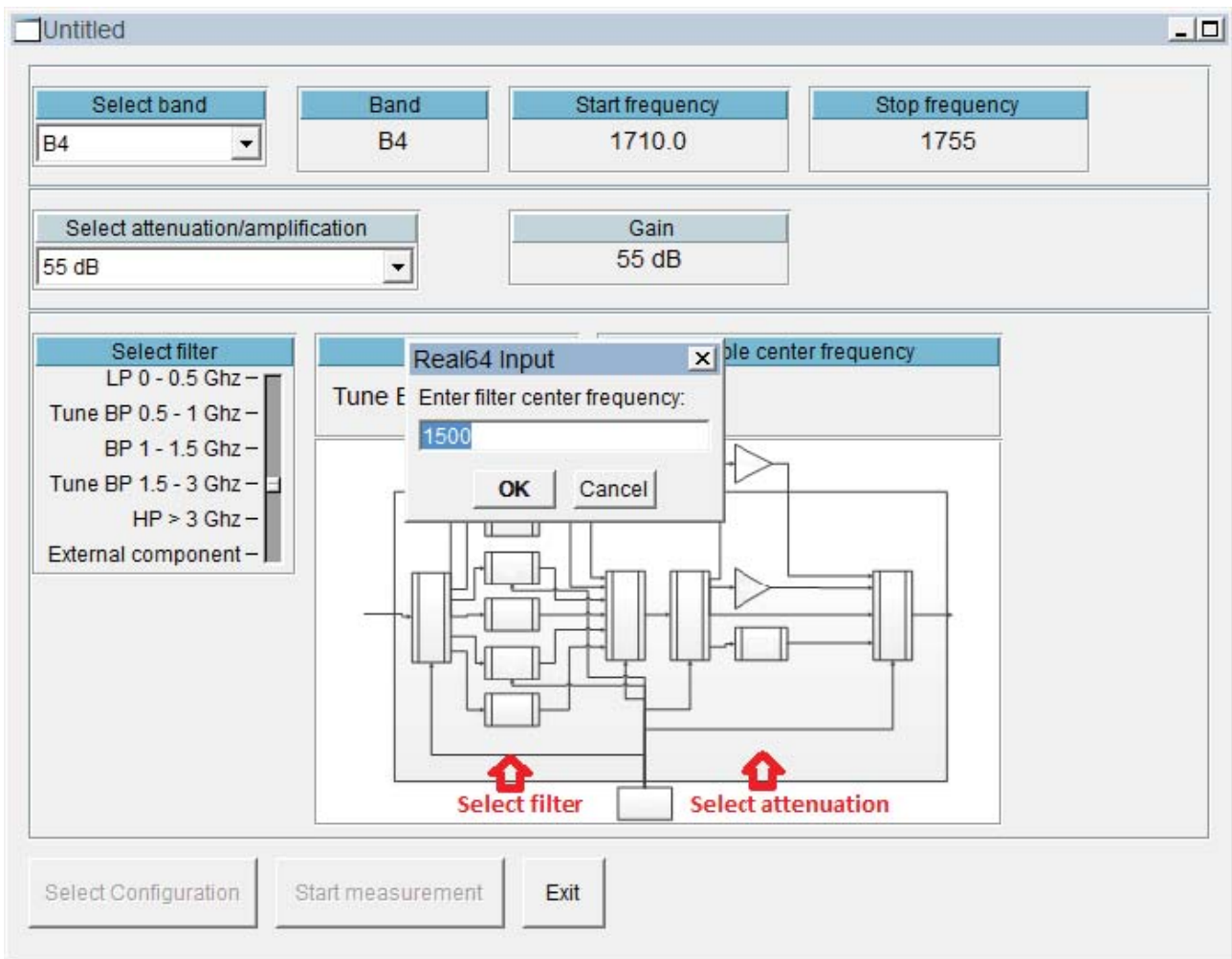


Figure 21: Selecting filter centre frequency

The "Start measurement" button as of currently only shows a message box, informing the user that the measurement will now start.

### 3.4.4 Outline for measurement algorithm

In addition of coding a basic user interface for the planned filter box, an outline for an automatic switching during measurement algorithm was created. The purpose of this algorithm is to plan future functionality for the application in VEE by allowing the program to control the tuneable filters and the switching of signal paths in the filter box. If the application has an automatic measurement function, it would allow the user to save time by allowing the program to do the majority of the switching of components. As of currently, the application would require the user to make several measurements while studying the spectral analyser and power meter to investigate whether attenuation or amplification is required. This algorithm is planned to be used only when the tuneable filters are used for a measurement. The picture below (Figure 22) depicts a flowchart of how the measurement algorithm could work

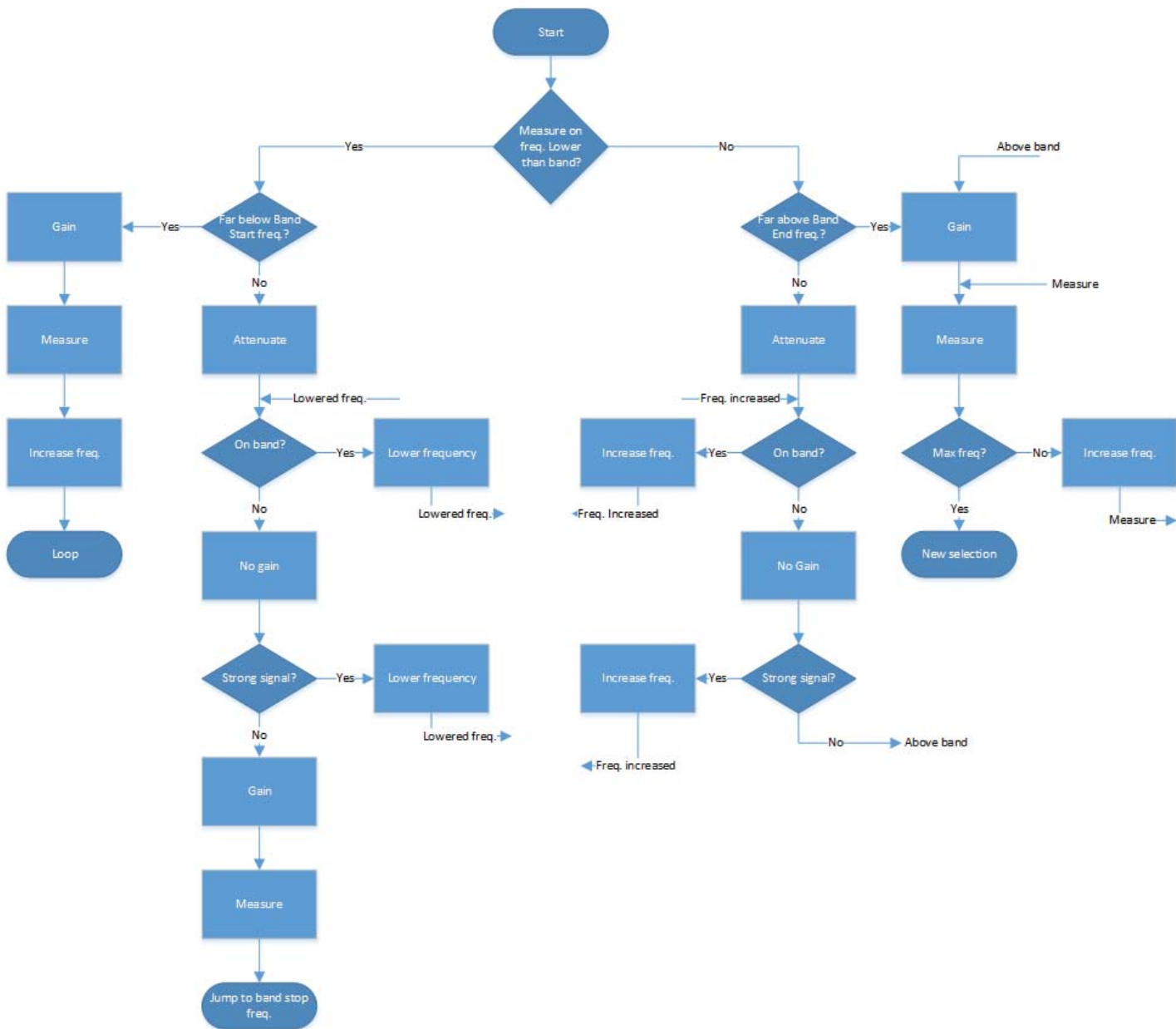


Figure 22: Outline for measurement algorithm

In general, this algorithm is meant to ensure that the measurement for spurious emissions with the filter box proceeds without breaking any of the equipment used for the measurement. This includes switching on the attenuator or amplifier where it is needed during the measurement. Furthermore, the algorithm makes sure measurement is conducted for all frequencies below and above the selected band. The algorithm consists of two main branches, one where the tuned filter frequency is below the start frequency of the band (Shown to the left in the picture) and one where the tuned filter frequency is above the stop frequency of the band (Shown to the right in the picture).

When the tuned filter frequency is below the centre frequency of the band, the algorithm works in the following way. First a test checks if the tuned filter frequency is close to the start of the band. If it is not, it is determined safe to use the amplifier, then measure and lastly the tuneable filter increases its frequency and repeats the test until the frequency is considered close to the band.

Once considered close to the band, the attenuator is switched to, circumventing the risk of breaking the spectrum analyser should the tuned frequency be in-band. Following this, the algorithm reads

the current frequency to determine if it is in-band or not. If it is, the frequency is repeatedly lowered until it is no longer in-band. The algorithm then switches to an empty signal path and the strength of the signal is read, then it either lowers the frequency until it is no longer considered strong, or switches on the amplifier and measures at the frequency if the signal is considered weak. Finally the filter tunes to the band stop frequency. At this point the other main branch of the algorithm will start running.

When the other branch of the algorithm starts running, the frequency of the filter is above the band and a test checks whether or not the tuned frequency is close to the band from the upper side. If it is, attenuation is switched on and another test keeps checking if the frequency is in-band and increases the frequency until it is no longer within the band. Following this, the filter box switches to an empty signal path and checks if the signal is strong or not. If it is, the frequency is increased until the signal is no longer considered strong otherwise the algorithm jumps back to the check which determines if the frequency is close to the band or not.

If the filter is tuned to a frequency far above the band, the filter box switches on the amplifier and measures. Afterwards a test checks if the filter has tuned to its max frequency. If it has not, the frequency is increased and measured until the test validates the frequency as max. Otherwise, the measurement ends and the user make a new selection for the application.

## 4. RESULTS AND CONCLUSIONS

Presented in this chapter are the results of the research and work outlined in the process chapter. The conclusions made are also included, as is the difficulties that were encountered during the project. Possible future plans for development are also present in this chapter.

### 4.1 Result

The theoretical outline of a more general filter box with tuneable filters was designed. The filter box, based on the choice of filters, is able to support spurious emission measurements for bands B1, B3, B4, B12 and B13. However, for B8 only RX is supported due to the bandpass filter having an inadequate lower stopband. Furthermore, because the highpass filter could not meet the requirements for stopband frequency, support for B7 will require an external filter. From the noise calculations the box is able to handle the requirement of a 5dB signal-to-noise ratio, even in a worst case scenario. The calculations of the size proved that the box would be of acceptable size for placement in a 19" rack.

When it comes to the cost of all so far established components, i.e. cables, switches, filters, attenuator and amplifier, the price seems reasonable compared to the guidelines received from Ericsson.

A basic user interface in Agilent VEE has been created which simulates the behavior of switching between components and bands to measure. In addition, the outline of an algorithm for automatic control during measurement using tuneable filters has been created.

## 4.2 Discussion

This section covers the discussion of the result and interesting topics.

It is possible that more environmental friendly components exist for creating this filter box but it was not a matter we investigated very deeply. It is uncertain if these components would have sufficient requirements. However, it can be something to investigate for future work.

Since the drawback from using tuneable filters results in worse shape factor, it might not be possible to measure as close to the carrier as desired. Working around it by attenuating the signal more results in worse SNR, which in many cases would make the SEM undistinguishable from the noise.

However, it is questionable if using non-tuneable filters for the box would be better. Since they are not tuneable, a large amount of filters would need to be used if the same amount of bands is going to be covered. And a higher amount of filters is guaranteed to increase the price and size of the filter box. If more filters are the answer, using the existing filter boxes for separate bands is probably better than building a bigger box with all filters.

Another problem is that it is hard to account for all passive intermodulation without having components to test. PIM needs to be measured on a real system since it is dependent on how clean connectors are and if they are thoroughly connected. In addition, only the switches and cables have specified levels of PIM, consequently, intermodulation of the other components are unaccounted for and would have to be investigated before purchase.

The dynamic range of a spectrum analyser can prevent measurements on the most extreme cases, 50dBm carrier and -115dBm SEM. Even with the carrier attenuated by 50dB down to 0dBm the difference is 115dB, which might be too much for spectrum analysers to handle. Using filters with better stopband attenuation alleviates this problem.

It is hard to determine how difficult it is to implement the automatic measurement algorithm in Agilent VEE. It is possible the algorithm can be improved and adjusted and is likely to be changed because of the shape factor issue.

Given more time it is possible that other component choices exist which fulfils the requirements and are cheaper than the ones we have picked. Maybe it is possible to adjust the parameters of the tuneable filters further, thus circumventing the shape factor issue.

## 4.3 Future Work

Investigate other components to provide support for B7 and TX of B8.

Further development of the Agilent VEE user interface application. Prepare its integration with physical components and solve possible bugs.

Write a manual for the Agilent VEE user interface application.

Investigate if there are cheaper and/or better alternatives to components.



Investigate if there are better tuneable filters with better shape factor.

Investigate the intermodulation of the components.

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## **Personal references**

20. Jörgen Ankarberg, Ericsson

21. Samir Kilim, Ericsson

22. Martin Hedin, Ericsson

## APPENDICES

### Appendix A: Filter box requirement specification

This appendix contains the requirements for the filter box

#### Interfaces

The switches and tuneable filters in the box will be controlled by a PC connected by GPIB. The box will have extra ports for connecting external components for other measurements to increase flexibility. An output port for connecting a spectrum analyser to measure signals.

1.	Original	GPIB for communication between filter box and PC.	Base
2.	Original	Ports for connecting external modules	Base
3.	Original	Port for spectrum analyser	Base

#### Functional requirements for filter box

The filter box has to be able to measure TX OOB spurious emissions on bands B1, B3, B4, B7 and B8. Support for band B12 and B13 is desired and, if possible, support for other bands as well. Ideally the filters will be digitally tuneable to keep the number of filters needed low. In order for the signal to be distinguishable, it is necessary for the PIM level generated by the components to be -130 dBm or less with a 40dBm carrier. This requirement makes it possible to measure signals at -115 dBm, which is the strictest requirement for OOB measurements, with a SNR of at least 5dB. To cover all desired measurements, the ability to handle a constant wave of 10W is required. For signals to be measurable by the spectrum analyser, the carrier needs to be attenuated by at least 50 dB by the filters. Otherwise the spectrum analyser will in all likelihood break due to the carrier power. The filter box needs to be of reasonable size and cost if it is going to be of interest for future development. A necessary amount of switches to accommodate the filters is required.

4.	Original	Support for bands: B1, B3, B4, B7 and B8	Base
5.	Original	Support for Band B12 and B13	Wanted
6.	Original	Support for other bands	Extra
7.	Original	Digitally tuneable filters	Wanted
8.	Original	One port for output	Base
9.	Original	External component support (filters etc.)	Base
10.	Original	Support for measuring down to -115dBm SEM level	Base
11.	Original	SNR greater than 5 dB	Base
12.	Original	Support for up to 10W CW	Base
13.	Original	Reasonable size	Base
14.	Original	Reasonable cost	Wanted

15.	Original	Support for TX OOB spurious emission measurements	Base
16.	Original	Support for RX OOB spurious emission measurements	Wanted
17.	Original	Support for other measurements	Extra
18.	Original	Switches for switching between filters/amplifiers	Base
19.	Original	Support for switching to a signal path with high attenuation.	Base

## Software requirements

The application will be written in Agilent VEE. The application will need to be able to select what filters that are going to be used for the measurement. The ability to switch between different amplifiers in the application is also required. The addition of preset configurations for different band is desired, to simplify usage of the application. A graphical representation of the current configuration would further increase user friendliness. A descriptive user manual is important so the user can understand how the application works.

21.	Original	Adjustable frequency range (by switching and/or tuning filter)	Base
22.	Original	Adjustable amplification (by switching amplifier)	Base
23.	Original	Preset for bands: B1, B3, B4, B7 and B8	Wanted
24.	Original	Preset for Band B12 and B13	Extra
25.	Original	Preset for other bands	Extra
26.	Original	Easy to use interface	Base
27.	Original	Graphical representation of settings	Wanted
28.	Original	User Manual	Wanted
29.	Original	Application written in Agilent VEE	Base

## Appendix B: Components and datasheets

The following list is a compilation of the components that was chosen to match the requirements laid out in the filter box design chapter, as well as their datasheets if available. The filter specifications were provided by Peter Perman, consequently no proper datasheets are included.

Component type	Product name	Manufacturer
Lowpass filter	7L120-510/T1500-O/O	K&L Microwave
Highpass filter	11SH10-3000/T13000-O/O	K&L Microwave
Bandpass filter	13ED50-1250/T500-O/O	K&L Microwave
Tuneable bandpass filter	5BT-500/1000-5-N/N	K&L Microwave
Tuneable bandpass filter	5BT-1500/3000-5-N/N	K&L Microwave
Amplifier	AMF-7D-00101800-30-10P	Miteq
Attenuator	47-40-33	Aeroflex/Weinschel
Switch-6port	H6P-140138	Charter Engineering
Switch-6port	H6P-140139	Charter Engineering
Switch-4port	H4P-140139	Charter Engineering
Switch-4port	H4P-140139	Charter Engineering
Cables	SUCUFORM_141_CU	Huber+Suhner

Lowpass filter: 7L120-510/T1500-O/O

3.0 dB Cut-off Frequency	510 MHz
Passband Insertion Loss (1-500 MHz)	0.9 dB
Stopband Attenuation (650-3000 MHz)	53 dB
Return Loss	14.0 dB (1.5:1 VSWR)
Filter Size	116.84 x 12.70 x 12.70 mm
Input Connector Type	SMA Female
Output Connector Type	SMA Female

Highpass filter: 11SH10-3000/T13000-O/O

3.0 dB Cut-off Frequency	3000 MHz
Passband Insertion Loss (3000-13000 MHz)	2.0 dB
Stopband Attenuation (2500 MHz)	50 dB
Return Loss	9.54 dB (2.0:1 VSWR)
Filter Size	44.45 x 25.40 x 12.70 mm
Input Connector Type	SMA Female
Output Connector Type	SMA Female

Bandpass filter: 13ED50-1250/T500-O/O

Centre Frequency	1250 MHz
3.0 dB Bandwidth	500 MHz
Insertion Loss	0.3 dB
Stopband Atten. (DC - 920 MHz):	50 dB
Stopband Atten. (1600 - 3000 MHz):	50 dB
Return Loss	11.7 dB (1.7:1 VSWR)
Filter Size	138.27 x 78.76 x 19.02 mm
Input Connector Type	SMA Female
Output Connector Type	SMA Female

Tuneable Band Pass Filter: D5BT-500/1000-5-O/O-GRI-LP

Passband (500-1000MHZ)	2 dB
Bandwidth	5% of $f_{center}$
Lower Stopband (0-450MHZ)	50 dB
Upper Stopband(1200-3000MHZ):	50 dB
Size	249 x 137 x 50 mm
Input Connector Type	SMA Female
Output Connector Type	SMA Female
G	GPIB Digital Interface
R	24 VDC
I	Tuning By Infrared Sensor

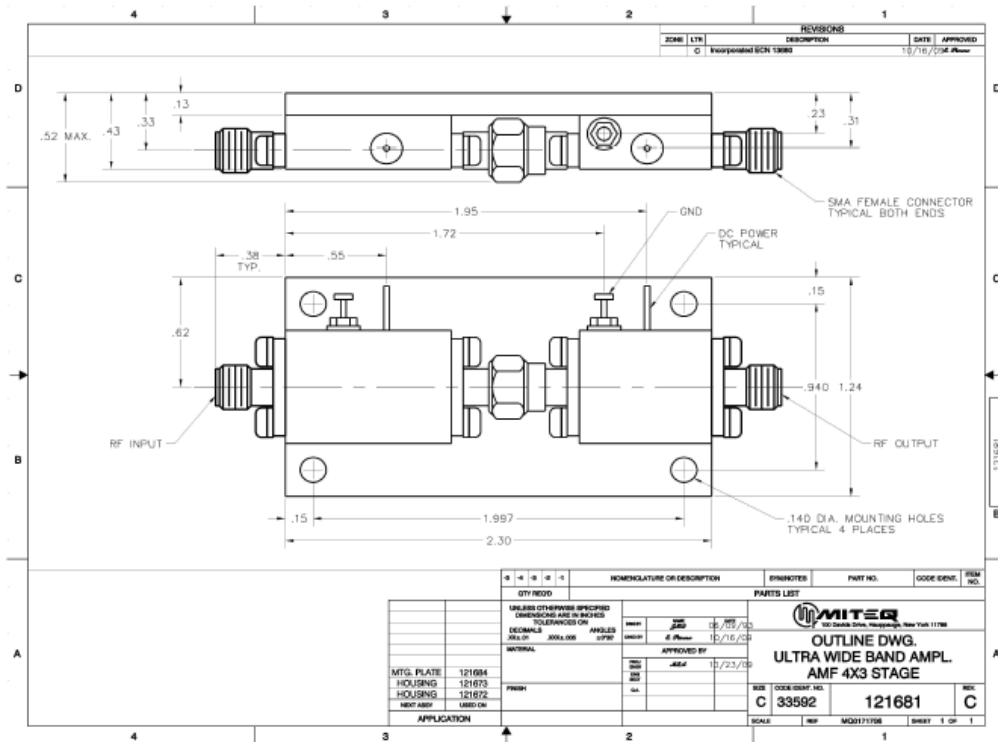
Tuneable Band Pass Filter: D5BT-1500/3000-2-O/O-GRI-LP

Passband (1500-3000MHZ)	2.7 dB
Bandwidth	2% of $f_{center}$
Lower Stopband (0-1450MHZ)	50 dB
Upper Stopband(3105-6000MHZ):	50 dB
Size	187 x 73 x 50 mm
Input Connector Type	SMA Female
Output Connector Type	SMA Female
G	GPIB Digital Interface
R	24 VDC
I	Tuning By Infrared Sensor

Amplifier: AMF-7D-00101800-30-10P

Specifications at 23 °C	
Frequency	0.1 to 18 GHz
Gain	55 dB min
Gain Flatness:	2 dB+/- max.
Noise Figure:	3 dB max.
Noise Temperature:	288.6 K max.
VSWR In	2.2:1 max
VSWR Out	2.2:1 max
P1dB Out:	10 dBm min.
Voltage:	15 V nom.
Current:	425 mA nom.
Outline Drawing:	121681
Operating Temp:	-40 to 75 °C

**Current Revision**  
As of 10/26/2009 7:47:32 AM



Attenuator: 47-40-33

## Fixed Coaxial Attenuators



### Model 47 Medium Power, N or 3.5mm Connectors

dc to 18.0 GHz  
50 Watts



#### Features

- Designed to meet environmental requirements of MIL-DTL-3933.
- Rugged injection molded connectors.

#### Specifications

NOMINAL IMPEDANCE: 50 Ω  
FREQUENCY RANGE: dc to 18.0 GHz

MAXIMUM DEVIATION OVER FREQUENCY:	
Nominal ATTN (dB)	Deviation (dB)
3, 6	± 0.75
10, 20	± 0.75
30, 40	± 1.00

MAXIMUM SWR:			
Frequency (GHz)	3, 6 dB	10, 20, 30, 40 dB	
dc - 8	1.25	1.20	
8 - 12.4	1.35	1.25	
12.4 - 18	1.45	1.35	

**POWER RATING** (mounted horizontally): 50 watts average (unidirectional) to 25°C ambient temperature, derated linearly to 5 watts @ 125°C. Note: 3 dB model can handle 100 Watts average (unidirectional). 1 kilowatt peak (5 μsec pulse width; 2.5% duty cycle). Maximum power rating into output port is 10 Watts average.

**POWER COEFFICIENT:** <0.0003 dB/dB/watt  
**TEMPERATURE COEFFICIENT:** <0.0004 dB/dB/°C  
**TEMPERATURE RANGE:** -55°C to 125°C

**TEST DATA:** Swept data plots of attenuation and SWR from 50 MHz to 18 GHz.

**CONNECTORS:** Type N connectors per MIL-STD-348 interface dimensions - mate nondestructively with MIL-C-39012 connectors.

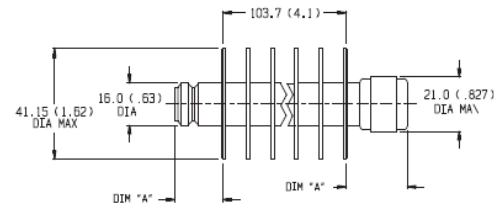
3.5mm Connectors - mate nondestructively with SMA per MIL-C-39012, 2.92mm and other 3.5mm connectors.

Options	Description	Options	Description
1	3.5mm Female	3	Type N Female
2	3.5mm Male	4	Type N Male

**CONSTRUCTION:** Black, finned aluminum body, stainless steel connectors with gold plated beryllium copper contacts.

**WEIGHT:** 175 g (6 oz.) maximum

#### PHYSICAL DIMENSIONS:

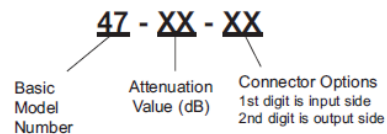


Connector	DIM A	Connector	DIM A
N Male	24.1 (0.95)	3.5mm Female	14.0 (0.55)
N Female	19.0 (0.75)	3.5mm Male	13.2 (0.52)

NOTE: All dimensions are given in mm (inches) and are maximum, unless otherwise specified.

#### MODEL NUMBER DESCRIPTION:

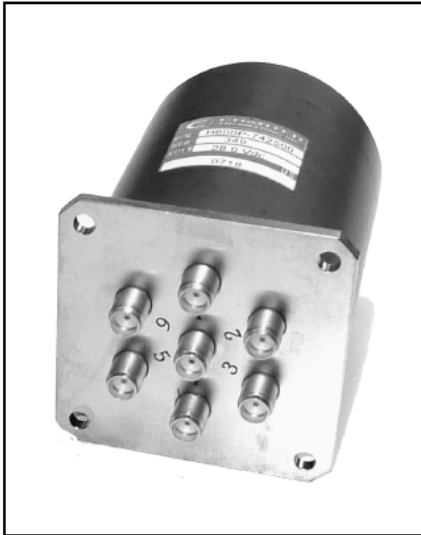
Example:



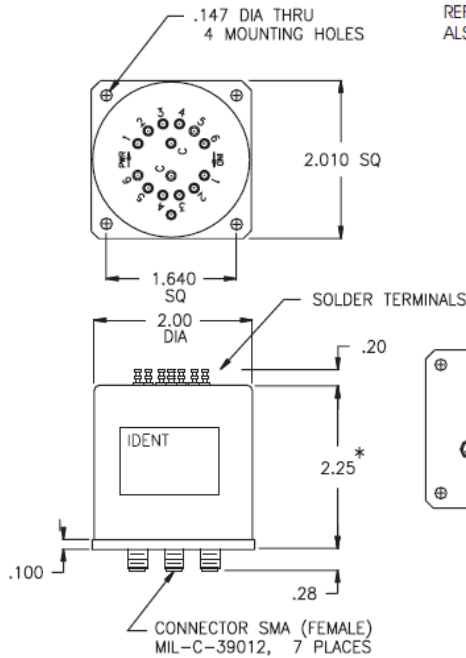


Switches: H6P-140138, H6P-140139 and H4P-140139

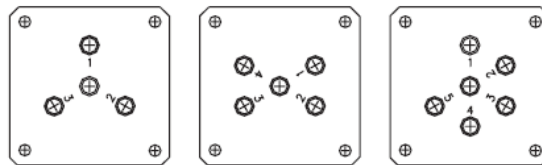
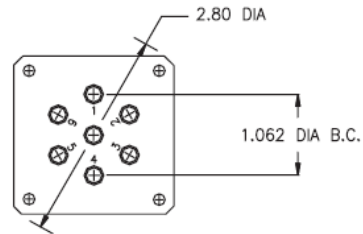
# H3 - H6 SERIES SP3T - SP6T DC - 26.5 GHz



<b>FREQUENCY:</b> GHz	DC - 2.0	2.0 - 4.0	4.0 - 8.0	8.0 - 12.4	12.4 - 18.0	18.0 - 26.5
<b>VSWR (MAX.)</b>	1.20:1	1.25:1	1.30:1	1.40:1	1.50:1	1.65:1
<b>INSERTION LOSS (MAX.)</b>	0.20	0.25	0.30	0.40	0.50	0.70
<b>ISOLATION (MIN.)</b>	90	80	80	70	60	50
<b>IMPEDANCE</b>	50 Ohms					
<b>MECHANICAL</b>						
CONTACT	:	BREAK BEFORE MAKE				
ACTUATOR	:	FAILSAFE, LATCHING, MOMENTARY				
SWITCHING SPEED	:	20 mSEC MAX.				
<b>ELECTRICAL</b>						
ACTUATOR VOLTAGE	:	28.0, 12.0, 15.0, 24.0 Vdc				
ACTUATOR CURRENT	:	CONTACT CEI				
POWER HANDLING	:	200 WCW @ 1.0 GHz (STANDARD) 300 WCW @ 1.0 GHz (OPT. /P)				
<b>ENVIRONMENTAL</b>						
OPERATING TEMP	:	-40 DEG. C TO 90 DEG. C (STANDARD)				
SINE VIBRATION	:	-54 DEG. C TO 90 DEG. C (OPT. /MS) **				
RANDOM VIBRATION	:	20 G'S/ms				
LIFE	:	1,000,000 CYCLES				
<b>FINISH</b>						
RF CAVITY	:	ALUMINUM ELECTROLESS NICKEL PLATED PER MIL-C-26074, CLASS 4 (EXCEPT LOW OR ULTRA LOW IM MODELS)				
ENCLOSURE	:	ALUMINUM, BLUE				
CONTACT	:	BERYLLIUM COPPER, GOLD PLATED PER MIL-G-45204				
CONNECTOR SHELL	:	CRES. PASSIVATED PER QQ-P-35 OR BRASS, ELECTROLESS NICKEL PLATED PER MIL-C-26074				
<b>AVAILABLE OPTIONS</b>						
INDICATOR CIRCUITRY	:	CUT OFF POWER CIRCUIT				
SUPPRESSION DIODE	:	D'SUB MINIATURE SERIES				
TTL LOGIC	:	MS CONNECTOR OR EQUIV. (MIL-SPEC)				
LOW, ULTRA LOW, AND SUPERIOR INTERMODULATION (IM)						



REFERENCE FOR DIMENSIONS ONLY  
ALSO AVAILABLE WITH A D'SUB OR MS CONECTOR



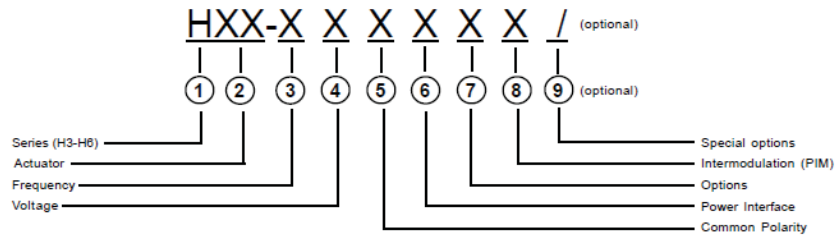
H3

H4

H5

\* SWITCH WITH TTL LOGIC OR PWR.CONNECTOR  
THIS DIMENSION TO BE 2.60 MAXIMUM.

## H3-H6 SERIES PART NUMBER &amp; ORDERING INFORMATION



<b>1 - Switch Series</b>			
H3	SP3T SMA		
H4	SP4T SMA		
H5	SP5T SMA		
H6	SP6T SMA		
<b>2 - Actuator</b>			
F	FAILSAFE	R	MOMENTARY
G	FAILSAFE WITH SUPPRESSION DIODE	S	MOMENTARY WITH SUPPRESSION DIODE
H	FAILSAFE WITH INDICATOR	T	MOMENTARY WITH INDICATOR
J	FAILSAFE WITH SUPPRESSION DIODE AND INDICATOR	U	MOMENTARY WITH SUPPRESSION DIODE AND INDICATOR
L	LATCHING	Y	OTHER (SPECIFY)
M	LATCHING WITH SUPPRESSION DIODE		
N	LATCHING WITH INDICATOR		
P	LATCHING WITH SUPPRESSION DIODE AND INDICATOR		
<b>3 - Frequency Bandwidth</b>			
1	DC - 13.0 GHz	6	DC - 6.0 GHz
2	DC - 2.0 GHz	7	DC - 26.5 GHz
3	DC - 12.4 GHz	8	DC - 20.0 GHz
4	DC - 4.0 GHz	0	OTHER (SPECIFY)
5	DC - 18.0 GHz		
<b>4 - Voltage</b>			
1	10 - 14 Vdc (12.0 NOMINAL)	4	24 - 32 Vdc (28.0 NOMINAL)
2	13 - 18 Vdc (15.0 NOMINAL)	5	OTHER
3	20 - 30 Vdc (24.0 NOMINAL)	0	NOT REQUIRED
<b>5 - Common Polarity</b>			
1	POSITIVE (+) COMMON		
2	NEGATIVE (-) OR RETURN Vdc COMMON		
0	NOT REQUIRED		
<b>6 - Power Interface</b>			
1	SOLDER TERMINAL (TOP OF SWITCH)	5	D' SUB MINIATURE SERIES (TOP OF SWITCH)
3	CONN MS3112E-XX-XXP OR EQUIV. (TOP OF SWITCH)	8	OTHER
<b>7 - Options</b>			
1	CUT OFF POWER CIRCUIT (LATCHING ONLY)	8	OTHER (SPECIFY)
2	TTL LOGIC	9	CUSTOM (ORDER)
3	CUT OFF PWR CIRCUIT & TTL LOGIC (LATCHING ONLY)	0	NO OTHER OPTIONS REQUIRED
<b>8 - Intermodulation</b>			
7	LOW PASSIVE INTERMODULATION	9	ULTRA LOW PASSIVE INTERMODULATION
8	SUPERIOR PASSIVE INTERMODULATION	0	STANDARD SWITCH
<b>9 - Special Options (optional - leave blank if not required)</b>			
/P	HIGH TEMP, HIGH POWER CONNECTOR		
/MS	EXTENDED TEMP RANGE -54 DEG C TO + 90 DEG		
/MSP	HIGH TEMP, HIGH POWER CONNECTOR AND EXTENDED TEMP RANGE		

## Cables: SUCOFORM\_141\_CU

## SUCOFORM\_141\_CU / \_141\_CU\_PE

## Cable design



Fig. 1: SUCOFORM\_141\_CU

Fig. 2: SUCOFORM\_141\_CU\_PE

	Description	Diameter
1. Centre conductor	Solid silver-plated copper wire	0.95 mm
2. Dielectric	Solid PTFE	2.95 mm
3. Outer conductor	Tin soaked copper braid	3.58 mm

SUCOFORM

## Electrical cable data

Impedance	50 Ohm
Operating frequency	33 GHz
Capacitance	92 pF/m
Velocity of propagation	71 %
Time delay	4.7 ns/m
Nom. attenuation*	coefficient a 0.3631      coefficient b 0.0377
Max. attenuation*	coefficient a 0.3995      coefficient b 0.0415
Max. operating voltage	1.9 kVrms
Min. screening effectiveness up to 18 GHz	100 dB

\*Attenuation calculation  $\alpha_{25} = a\sqrt{f} \text{ (GHz)} + b \cdot f \text{ (GHz)} \text{ (dB/m)}$

## General cable data

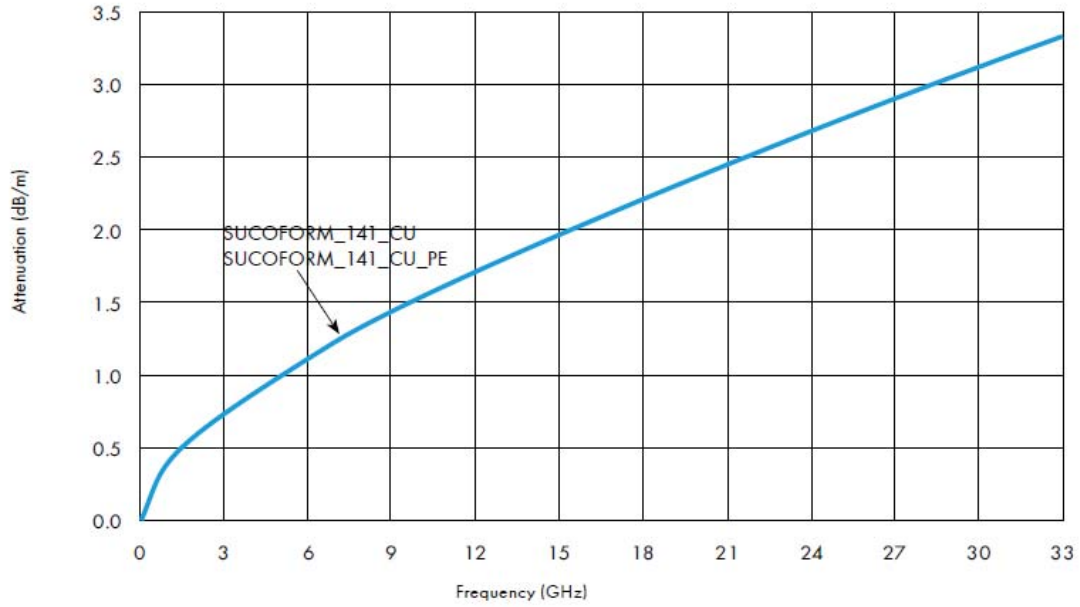
	SUCOFORM_141_CU	SUCOFORM_141_CU_PE
Item number	22511635	22511639
Additional jacket	–	PE
Colour	–	red
Diameter	3.58 mm	4.60 mm
Weight	4.0 kg/100m	4.7 kg/100m
Temperature range	- 65 ... + 165 °C	- 40 ... + 85 °C
Flammability, passed	IEC 60332-1, UL 1581-§1080 (VW-1)	–
Min. bending radius, static	8 mm	8 mm
Min. bending radius, repeated	40 mm	40 mm
Suitable connectors, cable group	Y12	Y12
Drawing	see Fig. 1	see Fig. 2

Suitable connectors see cable group Y12 (please refer to page 59 ff)

## SUCOFORM\_141\_CU / \_141\_CU\_PE

### Cable attenuation

Nominal values @ +25 °C ambient temperature



### Power Handling

Maximum values @ +40 °C ambient temperature and sea level

