## **Deco Planner Manual**

This document is written to support version 2.0.49

**17 November 2000** 

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## 1 About Deco Planner

Deco Planner software has been developed by a team of divers and decompression experts from around the world to model decompression for both recreational and extended range diving. The aim of the development was to produce a package which is simple to use whilst allowing more experienced divers to access to in-depth analyses of potential dive plans.

Furthermore, it is intended that Deco Planner can be used as an educational tool, by providing access to divers to extensive online reference material to allow them to improve their awareness of the theory of decompression.

Divers using this program should be aware that decompression is not an exact science and what this program does is attempt to draw a line through this scientific uncertainty whilst providing education such that the user can better understand the results being produced.

Although this program can be used to plan extensive Nitrox and Trimix dives it is NOT intended that the program becomes a shortcut to bypass formal training in these subjects.

The program Deco Planner is fully owned by its developer who retains all rights. In recognition of the input, testing, guidance and extensive help given by the others in the development team, The developer has agreed to allow Global Underwater Explorers non-exclusive rights to distribute Deco Planner exchange for a small donation to the GUE. This donation will allow GUE to continue to bring information, education and awareness to the world wide diving community and to further develop educational tools, such as this program. If you did not obtain your version of Deco Planner GUE, please contact them in order to ensure that you have the latest version and register it with them, so they can keep you informed of further developments.

If you have any questions regarding operation, usage or you have some feedback about Deco Planner please contact us via one of the following routes

#### Email

General Enquiries info@gue.com

Registered users can email technical questions to decoplan@gue.com

#### **Telephone**

1-800-762-DIVE inside the USA 904-454-0820 outside the USA 904-454-0815 (FAX)

# 2 System Requirements

Deco Planner has been tested on the following environments

Windows 95 Windows 98 Windows 2000 Windows NT4

The following files are required for operation of Deco Planner and are installed automatically if Deco Planner is being installed from the valid setup.exe program

C:\WINDOWS\SYSTEM\Msvbvm60.dll

C:\WINDOWS\SYSTEM\Olepro32.dll

C:\WINDOWS\SYSTEM\Oleaut32.dll

C:\WINDOWS\SYSTEM\asycfilt.dll

C:\WINDOWS\SYSTEM\stdole2.tlb

C:\WINDOWS\SYSTEM\comcat.dll

C:\WINDOWS\SYSTEM\Msvcrt.dll

C:\WINDOWS\SYSTEM\Msvcrt40.dll

C:\WINDOWS\SYSTEM\Mfc40.dll

C:\WINDOWS\SYSTEM\Mfc42.dll

C:\WINDOWS\SYSTEM\Spin32.ocx

C:\WINDOWS\SYSTEM\Comdlg32.ocx

C:\WINDOWS\SYSTEM\Vsocx32.ocx

C:\WINDOWS\SYSTEM\spr32x30.ocx

C:\WINDOWS\SYSTEM\Graph32.ocx

C:\WINDOWS\SYSTEM\Gswdll32.dll

C:\WINDOWS\SYSTEM\GSW32.EXE

C:\WINDOWS\SYSTEM\vsvbx.lic

\*folder\*\decoplan\decoplan.exe

\*folder\*\decoplan\decoplan.hlp

\*folder\*\decoplan\decoplan.cnt

\*folder\*\decoplan\readme.txt

\*folder\*\decoplan\install.log

# 3 Support

Deco Planner has been extensively tested during its development by a number of users under a number of system and hardware environments. However if you do encounter problems a number of options are open to you for support.

All users who purchase Deco Planner from GUE are automatically registered on an email support / discussion group called <a href="mailto:decoplan@gue.com">decoplan@gue.com</a>. If you are encountering an installation problem or operational problem, please provide as much detail as possible to enable the developers to assist you in resolution. Include, as a minimum, the following details in your email

Description of the problem: The operating system you are using: include a copy of the install.log file (which will be found in the directory in which you installed Deco Planner).

If you are struggling with operational issues or cannot find out how to complete an operation within the program, the <a href="mailto:decoplan@gue.com">decoplan@gue.com</a> email list has all the worldwide users and the developers, who can provide you assistance and advice.

For bug reports send an email to the <a href="mailto:decoplan@gue.com">decoplan@gue.com</a> list containing the following information. Detailed description of how you can recreate the bug, include all your preferences (GFIo / GFhi, Descent options, Ascent options, Imperial / Metric settings, Model used, Ascent / Descent rates, Surface pressure etc). If possible save the dive you are working on and send the DPL file as well, (this will be found in the Deco Planner directory).

If you are unable to send / receive email you can telephone/fax the following numbers.

1-800-762-DIVE inside the USA 904-454-0820 outside the USA 904-454-0815 (FAX)

## **4 About GUE**

Global Underwater Explorers was created exclusively to increase the quality and diversity of aquatic education. GUE was founded by conservationists, explorers and educators with a desire to see the mystery of the underwater world explored, studied, protected and shared. Global Underwater Explorers is prepared to redefine the nature of aquatic activity in three specific areas: education, research and exploration.

In sum, Global Underwater Explorers is a complete resource for the underwater enthusiast with a specific interest in seeing the underwater world explored, studied, protected and shared. By redefining the link between the underwater enthusiast and the scientific community GUE will be able initiate a unique age in underwater exploration. The evolving future of diving will allow thousands of people to combine their efforts in the pursuit of underwater recreation, education, research and exploration. The future of the underwater world is replete with unique opportunities; regardless of one's specific area of interest, Global Underwater Explorers has created a nexus to bring together the best of sport, technical and research diving in the service of environmental protection and understanding.

For more information on GUE, please visit the online website at <a href="http://www.gue.com/">http://www.gue.com/</a>

## 5 About the Author

The author of Deco Planner is Simon Tranmer. Simon is an experienced 'C++' and VB programmer who has worked in the computer industry for 18 years

Simon is an experienced diver and has been diving since 1995 in many locations around the world, including the Maldives, The Cayman Islands, Mauritius, Portugal, Cyprus and Scapa Flow. Most of his diving is on the wrecks of the UK south coast. Simon is a member of BSAC branch 1958 'Under Pressure'

Simon has studied diving physiology and decompression theory as a hobby and after moving to Nitrox wanted to find a quick and easy way to plan more technical dives. After looking at the commercial programs, which were available, Simon decided to produce a program, which was easier to use and tailored to those who wanted a program based on sound principles of decompression theory. To this end he was assisted greatly by information provided by Erik Baker, an expert in decompression theory, some of whose published articles appear elsewhere in this manual.

# **6 Credits**

The developers of Deco Planner would like to thank the following people for their dedication and assistance in developing the program

Simon Tranmer Erik C Baker Jarrod Jablonski Andy Kerslake Graeme Davison Keith Bellamy Sue Davison

& Numerous Others

# 7 Using The Program

#### 7.1 The Menus

Deco Planner utilizes the concept of missions and dives. A mission is a series of dives that are started as if the diver has not completed any previous dives. Once a dive is completed, the human body is loaded with inert gas, which will off gas on the surface over a period of time. It is assumed that if >24hours are spent between dives a new mission can be started.

## File Menu:FILE (alt F)

Access to the files menu which allows access to the following options

## **OPTIONS (Alt 0)**

A series of planning options which can be toggled on / off - if a tick mark is present along side the option the option is active

## TOOLS (alt T)

Provides access to two dive planning tools

## **GRAPH (Alt G)**

Provides access to a series of tissue graphs, which are used to analyse, planned dives.

#### WINDOW (Alt W)

Provides access to the standard Windows/95 window cascading, tiling facilities

#### HELP (alt H)

Contents (Alt C)

Provide access to this manual

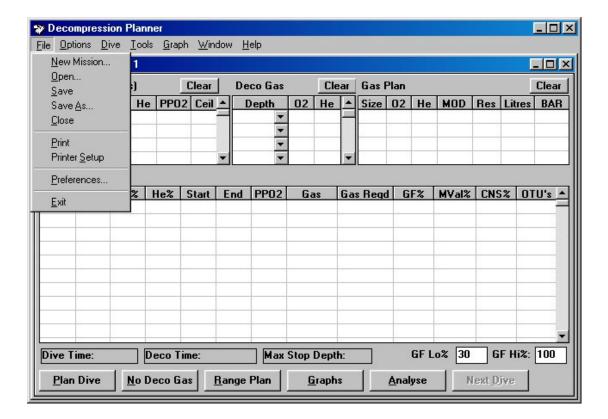
Read Me (Alt R)

Provides access to the revision history and any updates which did not make this manual

About (Alt A)

Provides access to the logon splash screen

#### 7.1.1 The File Menu



### File: New Mission (alt N)

Start a new mission consisting of a dive series - This requires the user to have experienced at least 24 hours of surface interval from any previous dive exposure.

#### File: Open (Alt O)

Loads a previously saved mission

#### File: Save (Alt S)

Saves the current dive mission, if the mission has been previously saved, the file name is kept the same. If this is a new mission, the user is prompted for the file name. By default the mission is saved in the Deco Planner directory, this can be changed if required

#### File: Save As (Alt A)

Save the current dive mission, prompting the user for a file name, by default the mission is saved as filename.dpl in the Deco Planner directory

#### File: Print

Prints the current active window to the Windows default printer.

## File: Printer Set up

Allows the user to change basic printer options such as paper size & format as well as the default printer

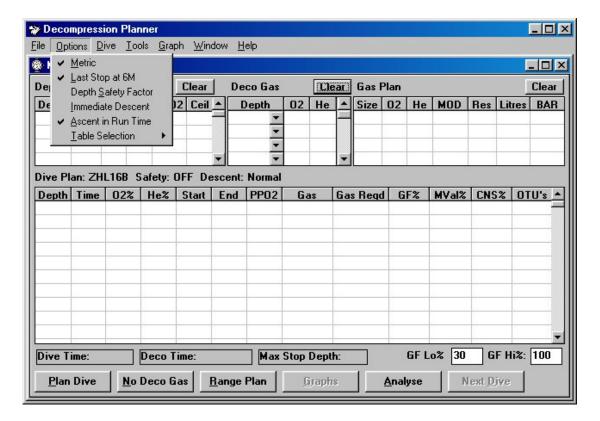
## File: Preferences (Alt P)

Gives access to a preferences screen which allows the user to set parameters used within the Deco Planner software for calculating missions & dives - See Preferences section for an explanation on the options which can be set in this section

File: Exit (Alt E)

Exit deco plan and return to windows

## 7.1.2 Options



#### Metric (alt M)

If set, Deco Planner works in meters, bars and litres. If not set, Deco Planner works in feet and cubic feet (imperial), with decompression being calculated in 10 feet increments - If a dive has been planned in metric, it is possible to convert this to feet to toggling this option - the decompression will be greyed out and can be recalculated again by hitting the plan dive button

#### Last stop at 6m (alt L)

Divers decompressing on Oxygen, often prefer to complete the last stop at the optimum depth (6m/20feet) for the optimum benefit from the oxygen window. Setting this option allows Deco Planner to recalculate the last stop to be completed at 6m (20 feet) as opposed to 3m (10 foot) as with standard Bühlmann tables. **Note** if metric is not set this option will read "Last stop at 20 feet"

#### **Depth Safety Factor (alt S)**

If set all calculations are completed as if the depth is equal to (ENTERED DEPTH \* 1.03) + 1 meter. This increasing of the inert gas fraction was an early attempt to introduce conservatism and comes from Bühlmann's work. Unfortunately the problem with this method is it produces inconsistent results. Generally, short/shallow dives will result in a large margin of safety and deep/long dives will see the margin of safety decrease to inadequate levels.

This kind of inconsistency should not be acceptable for the calculation of mixed-gas technical diving profiles. One reliable and consistent method of introducing conservatism is by controlling M-value gradients and thereby controlling Percent M-values. The Depth Safety Factor option has been included to allow users to compare Deco Planners output against other dive planning programs.

## Immediate descent (alt I)

If set it is assumed that all the descents are immediate, if not set descent time is modelled and on gassing is accurately calculated based upon descent rates set in the preferences section. Please see <u>operational issues</u> for further information to be taken into account with dive planning and this parameter.

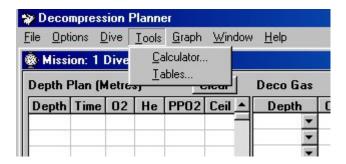
#### Ascent in Run Time (alt A)

This option causes deco stops to be calculated with the ascent time to the next stop included in the stop. This means a one minute stop is actually calculated as one minute less the ascent time to the next stop. When doing the dive this means you should plan on arriving at a stop at the start times given, NOT leaving for the next stop at the given end times. When including ascent in run times the ascent to the first stop is rounded up to the nearest minute and the extra rounding up time is considered as though it had been at depth. **NOTE** this is the methodology that Bühlmann originally used in his research.

### Table Selection (alt T)

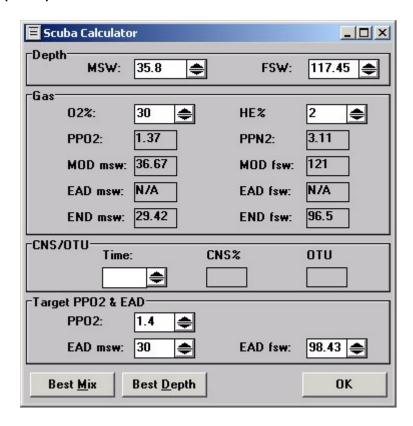
This allows access to changing which of the Algorithms is used in the Deco Planner software - currently 2 of the Bühlmann's systems are used ZHL16B and ZHL16C. ZHL16B is intended for generation of tables and dive profiles, ZHL16C is intended for minute by minute calculations such as those computed by a in water dive computer. Both models have been included as educational tools. For most dive planning it is recommended the user uses ZHL-16B.

#### 7.1.3 Tools



The tools menu gives access to a dive calculator and table generation facility

## Calculator (Alt C)



Gives access to a depth (in feet or meters) to best mix and max operating depth calculator - by entering a depth figure in either the MSW (metric) or FSW (imperial) windows, the tool can then calculate the PP02, MOD (based on the set PP02).

The tool also calculates, if the mix contains no helium, an equivalent air depth (assuming O2 is <u>not narcotic</u>) or if helium is present in the mix an Equivalent Narcosis depth is calculated.

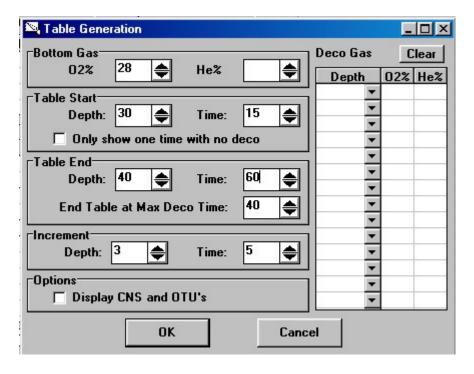
MSW to FSW calculations can also be performed.

The user can increase or decrease the depths and gas contents with the simple use of the up/down tumbler arrows to the right of the window in question.

Entering a time in the CNS/OTU section will give simple CNS% and OTU calculations for the mix in question assuming all the time is spent at the same depth.

Two Buttons are present for Best mix and Best Depth - these will calculate best mix based on the set PP02 and set EAD. Selecting these buttons will modify the relevant calculator entry in order to display the relevant answer

### Tables (Alt T)



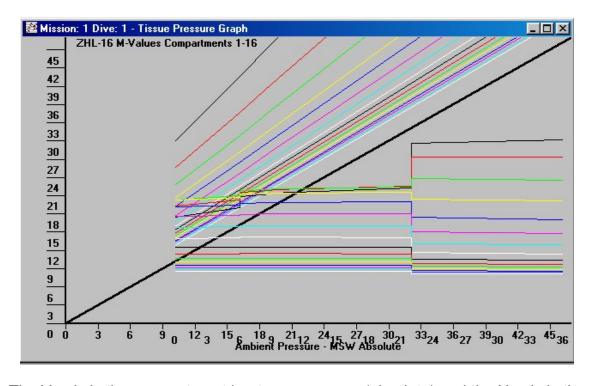
The bottom gas FO2 and FHe (in percent) are entered in the top two windows. The table start depth (i.e. the minimum planned dive depth) and the table start time (i.e. minimum planned dive time) are then entered.

Maximum planned dive depth and time are then entered in the next two windows. The object of these windows is to enter the four corners of the planning variables

Further information is presented in Dive Table Generation

## 7.1.4 Graph Analyses Tool

The pressure graph is a useful tool for analysing decompression profiles because a diver can see both the computed gas loadings and the M-values for a profile and easily visualize the general characteristics of the profile. This includes identifying when the profile is in the "decompression zone" (gas loadings above ambient pressure), identifying excessive gradients over ambient pressure, identifying stops that are "too deep," identifying a surge or "swell" of gas loadings over ambient pressure at a particular point, and identifying when individual inert gases are on-gassing and off-gassing.



The Y-axis is the compartment inert gas pressure (absolute) and the X-axis is the ambient pressure (absolute)

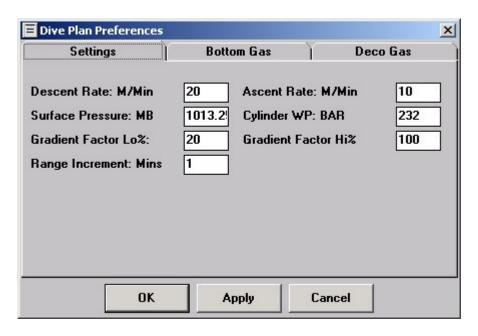
An M-value (maximum value) is the maximum tolerated partial pressure (absolute) of inert gas for a given compartment at a given ambient pressure. The range of M-values for a given compartment over the range of possible ambient pressures are shown as the upper straight lines, with the slope being equal to or less than 45 degrees on the diagram above

The ambient pressure line (APL), the thick black line, is simply a reference line on the graph with a slope of 45 degrees and passing through the origin. The APL represents all points where the compartment inert gas pressure will be equal to ambient pressure. Points plotting above the ambient pressure line will represent overpressure (or supersaturation) in the compartment(s).

The graph normally shows all 16 compartments, however it can be can be used to zoom into show individual compartment data. Whilst in graph mode, the minus key will remove all compartment lines and then each compartment can be displayed by keying its relevant number on the keyboard i.e. 1 for compartment 1, 2 for compartment 2 etc. Note as we have to deal with 16 compartments we adopt the hexadecimal numbering scheme where the A key is used for compartment 10 through to F for compartment 16. The PLUS key is used to display all 16 compartments again.

#### 7.2 Preferences

## **Settings**



#### **Descent rate**

This parameter is only used if the option for immediate descent is set. With the immediate descent option turned on this rate in meters per min (or feet per min if not in metric) will be used to calculate run times and on gassing for the descent phases of the dive plan. Otherwise it is assumed the descent from surface to the first defined dive depth is zero seconds.

#### Surface Pressure MB

This is the known ambient surface pressure, if the actual surface pressure is not known, it is recommended that this be set to 1013mb. This parameter is limited to a setting between 300mb and 1500 mb.

#### **Gradient Factor Lo %**

The % gradient factor controlling the decompression at the first decompression stops, the lower the figure entered, the deeper the first decompression stops will start. For a detailed explanation of gradient factors please see <a href="Deep Stops">Deep Stops</a> <a href="Explained by Erik Baker">Explained by Erik Baker</a>

## **Range Increments: Mins**

This value sets the increment period used in planning the variable time on the last dive segment entered

#### **Ascent rate**

This is the ascent rate used in calculating dive times in meters per min (or feet per min if running Deco Planner in feet) the recommended ascent rate is 10m/min (30 feet/min)

## Cylinder working pressure

This is the default cylinder working pressure in BARS - this value is used in both bottom gas and deco gas calculations. Note, if Deco Planner is not set to metric any value entered into this field is not used in any calculation.

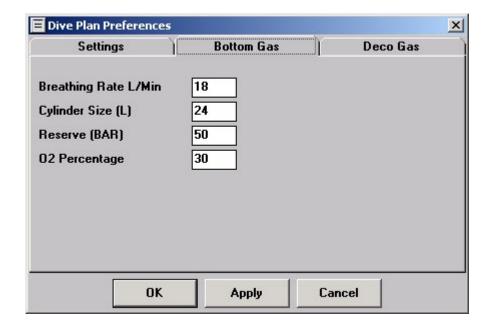
To calculate bars from PSI the following calculation is used

**BARS = PSI / 14.7** 

#### **Gradient Factor Hi %**

The % gradient factor controlling the decompression at the last decompression stop (i.e. the surface). For a detailed explanation of gradient factors please see <a href="Deep Stops Explained by Erik Baker">Deep Stops Explained by Erik Baker</a>

#### **Bottom Gas Defaults**



## **Breathing Rate L/min**

This is your breathing rate in litre's per min (or cubic feet per min if running Deco Planner in feet) this is used in calculating gas requirements for the NON decompression portion of the dive. Any figure > 0 can be added, it is left to the user to ensure that a valid figure has been entered to ensure that valid gas requirement calculations are completed.

## Cylinder size

This is the default cylinder size, in litres when working in metric or cubic feet (at cylinder rated pressure) if working in imperial. The cylinder size is used in calculating gas requirements for back gas mix.

#### Reserve (bar)

This is the reserve gas, which is not taken into account in the gas requirement calculation. It is good practice to always ensure adequate gas is available, and a reserve should always be used. A minimum figure of a third, of the initial gas, should be reserved for any dive in an overhead environment including a decompression dive.

To calculate bars from PSI the following calculation is used

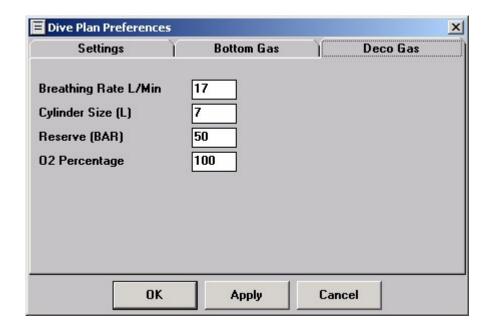
#### BARS = PSI / 14.7

#### O2 Percentage

This is the default Nitrox mix used for all bottom gas calculations, It is left to the user to ensure that PO2 levels are not exceeded when planning a dive. This can be changed within the Deco Planner page whilst entering details. Deco Planner

warns the user of excessive PO2's in the dive display by displaying PO2's greater than 1.4 in orange and PO2's greater then 1.6 in red.

#### **Deco Gas Defaults**



#### **Breathing Rate**

This is your breathing rate in Litres per min (or cubic feet per min if running Deco Planner in feet) at resting and is used in calculating gas requirements for the decompression portion of the dive. Any figure > 0 can be added, it is left to the user to ensure that a valid figure has been entered to ensure that valid gas requirement calculations are completed.

#### Cylinder size

This is the default cylinder size, in litters when working in metric or cubic feet (at cylinder rated pressure) if working in imperial. The cylinder size is used in calculating gas requirements for all decompression gas mixes. The cylinder sizes can be changed on the main dive planning screen.

#### Reserve (bar)

This is the reserve gas, which is not taken into account in the gas requirement calculation. It is good practice to always ensure adequate gas is available, and a reserve should always be used

To calculate bars from PSI the following calculation is used

**BARS = PSI / 14.7** 

#### O2 Percentage

This is the default Nitrox mix used for the last decompression gas of a dive; it is left to the user to ensure that PO2 levels are not exceeded when planning a dive. This can be changed within the Deco Planner page whilst entering details. Deco

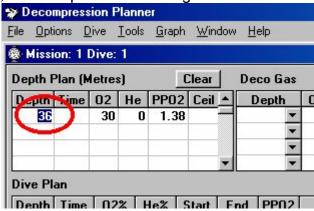
Planner warns the user of excessive PO2's in the dive display by displaying PO2's greater than 1.4 in orange and PO2's greater then 1.6 in red.

## 7.3 Planning a Dive

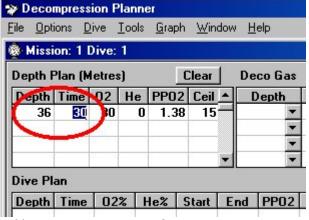
## 7.3.1 Entering basic dive information

Note: Planning dives with Deco Planner set to work in feet, follows exactly the same process as detailed below. In order to keep files sizes to a minimum only metric pictures have been included.

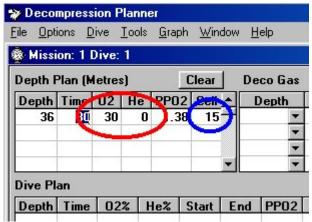
Dive planning in Deco Planner is very simple; the cursor is positioned in the depth plan section, in the depth column using the mouse.



The depth of the first portion of the dive is entered. The right cursor key is used to move across to the time column where the time at that depth is added.

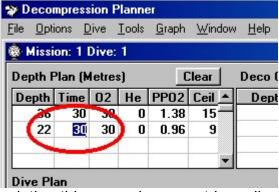


The %O2 and %He (% He is only added if using Trimix/Heliox) content of the mix can now be entered by moving to these columns with the right arrow key (the remainder to 100% is assumed to be nitrogen). In the example a bottom mix of EAN30 has appeared as this is the default bottom mix, which has been set in the dive preferences



If EAN30 was not being used for this dive, the user can edit both the %O2 and the %He at this point. It can be seen that Deco Planner has calculated that completing this dive, to 36m for 30 mins, has already produced a ceiling of 15m for decompression (shown in the blue circle). Deco Planner can now be instructed to calculate the decompression schedule or additional dive segments can be added to the dive profile.

In order to plan a multi level dive, the user moves down a row in the depth plan section and enters other depth/times. In the example shown, we have planned a second segment in the dive of 30 minutes at 22 meters.



We now see that completing this second segment has allowed some off gassing and the decompression ceiling has risen to 9 m.

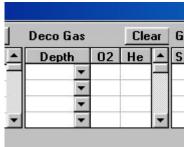
Additional segments can be added to the dive profile up to a MAXIMUM of 20 depth segments. The user simply utilizes the cursor arrow keys to navigate around the depth plan section. Whilst entering the dive segments it is possible to delete individual depth/time segments by hitting CTRL+D when the cursor is on the line to be deleted. If more than 4 segments are entered in a dive plan, the user can either use the scroll bar (to the right of the Depth plan window) to scroll up and down for review and edit or may resize the window, by placing the mouse on the bottom of the depth plan window, click and hold the mouse button and then drag the window down to make it bigger.

If the user wishes to delete all the dive depth and time segments entered, they can simply click on the clear button which is above the depth plan window

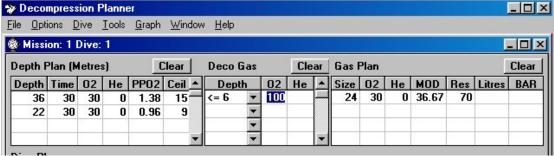
**Note:** After entering depth and breathing gas information, it is possible to have Deco Planner calculate the no decompression time limit for a dive to that depth by keying a? whilst the cursor is in the time cell (if a figure of zero is returned, the dive is a decompression dive)

### **Entering Deco gas information**

Once the dive segments have been entered the user either TABS across to the deco gas window or clicks with the mouse in the window to enter the chosen decompression mixes.



In the deco gas window, the user can enter the decompression mix, which is to be used from each depth. To the right of the depth window is a menu pull down which allows gas switch points to be chosen down to a maximum depth of 90m. To access this menu the user simple left click with the cursor and then uses the scroll bar to enter the gas switch depth. In the example shown we have chosen to complete all decompression at <=6m on 100% O2.



Multiple decompression mixes can be used upto a maximum of 20 different mixes. Note no checking is undertaken regarding max PO2 decompression gases and it is possible to call up 100 % O2 for 60m - which is NOT recommended. As with the depth plan, it is possible to delete individual lines within the Deco gas window by hitting CTRL+D when the cursor is on the line to be deleted

If the user wishes to delete all the decompression gases used, they can simply click on the clear button which is above the deco gas window

#### Gas Plan

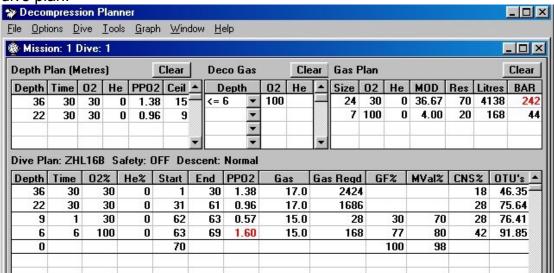
The only columns that can be changed are the Size & Reserve columns. When working in metric, the BAR column indicates how many bar is needed (inc. the reserve) to complete the dive. If this figure is in RED it is exceeding the maximum cylinder pressure set in the preferences, increase the cylinder size used for the dive - note it is good practice to always ensure adequate gas is available, and a reserve should always be used. NOTE full gas plan information is only available once the dives has been planned

When working in Imperial, the user can change the cylinder size presented in the gas plan window, the figure given in the cubic feet column is the free gas required to complete the dive including the reserve.

If the user wishes to delete the contents of the gas plan window, they can simply click on the clear button which is above the gas plan window

#### PLAN DIVE BUTTON

This button calculates the dive decompression and gas requirements. All relevant decompression mixes programmed into Deco Planner are used in the dive plan.



In the above diagram, the decompression requirement for this dive is shown. The details show that a 1 minute stop at 9m and 6 min stop (on Oxygen) is required. In addition the pressure in the 24l cylinders is shown in red, this is because the calculated fill pressure needed to complete the dive, exceeds the cylinder working pressure set in the preferences.

#### **NO DECO GAS BUTTON**

This button calculates the dive decompression and gas requirements assuming ALL decompression mixes have been lost and the dive is to be conducted only on the Depth Plan information

Depth	Time	02%	He%	Start	End	PP02	Gas	Gas Regd	GF%	MVal%	CNS%	OTU's
36	30	30	0	1	30	1.38	17.0	2424			18	46.35
22	30	30	0	31	61	0.96	17.0	1686		1	28	75.64
9	1	30	0	62	63	0.57	15.0	28	30	70	28	76.41
6	14	30	0	63	77	0.48	15.0	360	77	80	28	76.43
0	- 1			78			- 1		100	99		

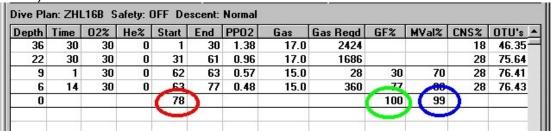
As can be seen in the above example the previous calculated 6 min at 6m stop has been increased to 14 mins.

#### THE DIVEPLAN WINDOW

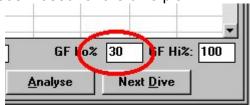
The Deco Planner window gives detailed information of the depth plan entered (above the first dark black line) and decompression calculated.

Full run time information giving starting and ending times for all the stops is included. The display also shows CNS % and OTU's, which are cumulative as the dive progresses (as such the %CNS and OTU's for the end of the dive are shown in the last row). The Mval% display shows the maximum M value during the dive, this figure will rise as the diver ascends and arrives at the next depth in the dive plan (including the decompression stops).

Between the bottom two black lines a summary of some important surfacing details are shown: namely, the surfacing run time (red circle), the MAXIMUM surfacing Gradient Factor (green circle) and MAXIMUM surfacing M Value (blue circle).



If the diver decides that the surfacing M value is too great, the Gradient factor low (GF Lo%) and Gradient factor high valves (GF Hi%) can be modified, as shown, to change the conservatism used for the dive plan.



For details on how to use Gradient factors to control dive conservatism please read the section on dive analysis

If any details in the depth plan window are changed, the details in the Deco Planner window are greyed out to show they are now longer valid, hit either the Plan Dive or the No Deco Gas buttons to replan the decompression obligation again.

#### RANGE PLAN BUTTON

Gives access to a simple dive range planning tool, This tool will calculate the decompression obligation (using all the defined gases) whilst varying the last dive segment time from zero to the entered time in the time interval which was set in the Dive preferences.

If only one dive segment has been entered and the user is using Deco Planner to calculate a set of dive tables, Deco Planner offers a much more feature rich facility in the <u>table generation option</u>.

#### **GRAPHS**

Gives access to a series of in-depth dive analysis graphs

#### **ANALYZE**

Provides access to a detailed dive analysis tool

#### **NEXT DIVE**

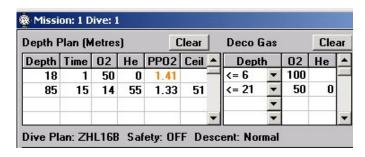
This allows the planning of repetitive dives.

## 7.3.2 Planning a dive using a travel gas for descent

When planning a dive with non immediate descent set, Deco Planner makes some assumptions on which gas is used whilst modelling each separate descent. The first descent (i.e. from the surface) is always completed on the gas entered for the first dive segment. The next descent to the next depth / time segment is completed on the same gas UNLESS the PO2 would exceed 1.6 in which case the descent is completed on the gas entered for the next depth / time segment.

This logic attempts to differentiate from a dive where the diver is descending on a travel gas and a dive where the early part of the dive is a multi level profile followed by a travel gas switch.

For instance a Diver is planning a dive to 85 m on bottom mix of 14/55. As this mix is Hypoxic at the surface the diver intends to drop to 18m on his first deco mix (EAN50). The diagram below shows the details entered into Deco Planner and the subsequent analysis chart showing the gases used in modelling the descent. The diver has assumed a 1 min pause at 18m for the gas switch (by entering a time of 2 minutes, the dive has modelled approx one minute for descent and 1 minutes for gas switch).



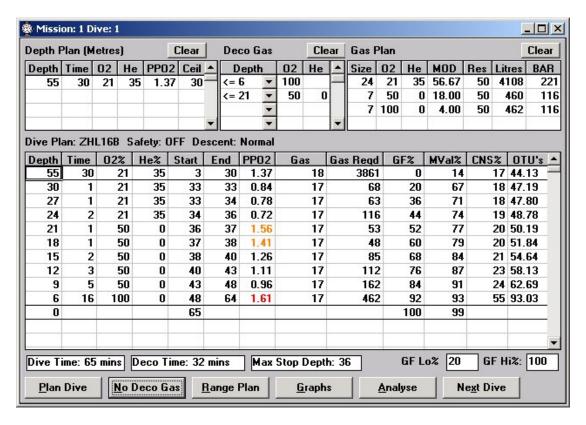
Looking to the analysis on the right, the gas used in the computation are shown (highlighted in green). Segment one (initial descent) is completed on EAN50. The diver holds at 18m for one minute (actually 1.1 minutes) completing the gas switch and then descends on the Trimix 14/55 from 18m to 85m

If the Diver had planned this dive dropping on EAN 50 to a depth at which the PO2 is greater than 1.6, Deco Planner will indicate the PO2 in red and immediately gas switch to the next gas for the next descent.

Mission: 1 Dive	1 - Ana	ysis			
SEG: 1	DESC	9.			
START DEPTH	0				
FINAL DEPTH	18	PHe+			
RATE	20	%Amb			
SEG TIME	.9	He (			
DIIN TIME	q	N2 (			
MIX 02	50%	M-V			
MIX He	0%	%M-V			
		%М-V (			
SEG: 2	STOP				
CONST DEPTH	18				
PO2 ATA	1.39	PHe+			
SEG TIME	1.1	%Amb			
RIIN TIME	2 በ	He (			
MIX 02	50%	N2 (			
MIX He	0%	M-V			
		%M-V			
	%M-V				
SEG: 3	DESC				
START DEPTH	18				
FINAL DEPTH	85	PHe+			
RATE	20	%Amb			
SEG TIME	3.4	He (			
RIIN TIME	54	N2 (			
MIX 02	14%	M-V			
MIX He	55%	%M-V			
		у <b>ы</b> 17 (			

## 7.3.3 Modifying gas switches / decompression times

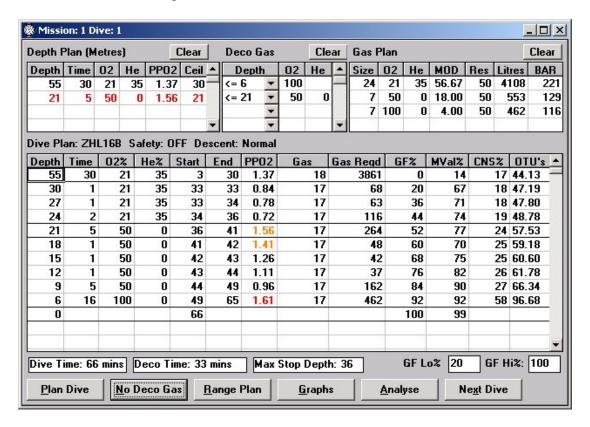
In the following example a user has planned a dive of 30 minutes to a depth of 55m, decompressing with EAN50 from 21m and Oxygen from 6m.



Research has shown that it is advantageous to extend a gas switch decompression stop (to around 5 minutes) to gain benefit from the Oxygen window and to account for the delay in transport of oxygen around the body by the blood system. The user in this example has therefore elected to extend the 21m stop on EAN50 to 5 minutes. This is simply done by entering this information into Deco Planner, as normal. A warning is generated, informing the user that this dive segment is shallower than the calculated ceiling and decompression stops will be added.



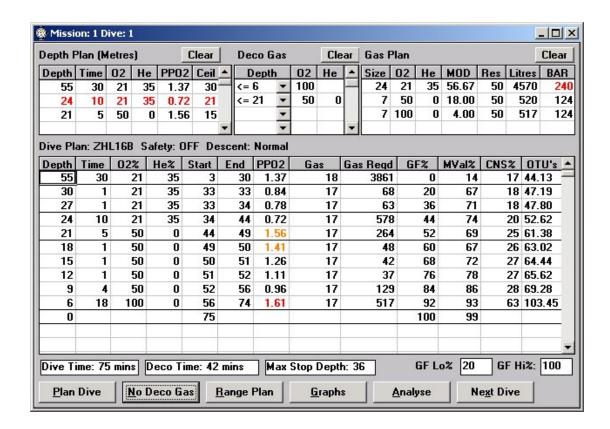
Upon accepting this warning, the 21m segment is shown in red on the dive plan window and when decompression is calculated, Deco Planner will calculate the decompression stops as before, extending the 21m time to 5 minutes. As can be seen in the diagram below, the stops shallower than 21m have been modified to account for the benefit gained at 21m



If the user attempts to modify a stop time with a time shorter than the required time, Deco Planner will account for this as shown below. A user has selected a 21m stop of 5 minutes, however the profile in question required a 21m stop in excess of this, as such Deco Planner automatically ensure the extra time is calculated and shown.

🏽 Missi	on: 1 D	ive: 1		
Depth F	Plan (M	etres	;)	
Depth	Time	02	Н	
55	100	21	3	
21	21 5 50			
Dive Pl	an: 74	I 16E	S	
			-	
Depth	Time	02	%	
		02	-	
Depth 55	Time 100	02	% 21	
Depth 55	Time 100	02	% 21 21	
Depth 55 36 33	Time 100 1	02	% 21 21 21	
Depth 55 36 33 30	Time 100 1 3	02	% 21 21 21 21 21	
Depth 55 36 33 30 27	Time 100 1 3 6 7	02	% 21 21 21 21 21 21	
Depth 55 36 33 30 27 24	Time 100 1 3 6 7	02	% 21 21 21 21 21 21	
Depth 55 36 33 30 27 24 21	Time 100 1 3 6 7 9	02	% 21 21 21 21 21 21 50	

This facility can also be very useful in cave diving where the cave profile may lengthen sections of the decompression forcing longer stops than planned. In the following example a dive is being planned in which a section of cave, at 24m, is part of the cave exit. This depth is in our decompression zone, and the user know that it will take us 10 minutes to traverse this cave section. The user enters details as before, including the 10 minutes at 24m that they will be forced to undertake. In addition the user wishes to extend the21m stop on EAN50 (as before), so this is also entered. Deco Planner takes these modifications to the previously calculated decompression into account and recalculates the decompression whilst still taking into account the user Gflo / GfHi settings.



## 7.3.4 Planning dives at Altitude

Deco Planner can be used to plan dives at altitude by using the surface pressure parameter in the <u>Dive Plan Preferences</u>. This parameter takes into account, altitude as well as the ambient surface pressure due to the current weather system.

The correct option is to take a calibrated barometer to the dive site, which will actually measure the ambient pressure and thus take both weather and altitude into account.

If this is not possible and the altitude and sea level ambient pressure is known, the pressure at altitude can be calculated from the following equation.

$$p(z) = po * exp(-Mgz/RT)$$

Where po = 1013.25 mbar M = 28.8 g/mol = 0.0288 Kg/mol g = 9.81 m/s^2 R = 8.314 S.I.

T = temperature in Kelvin's (to convert degrees Celsius to Kelvin's add 273)

This formula can be simplified as follows (assuming the temperature is 15C)

$$p(z) = 1013.25 * exp(-z/8475)$$

Don't forget that 'z' must be in meters (not in feet or kilometres). The following tables assumes sea water surface pressure = 1013.25 and temperature at altitude is 15 C

Altitude (m)	Pressure (mb)
500	955
1000	900
1500	849
2000	800

## 7.4 Dive Analysis

The Deco Planner Analysis Display provides detailed information about tissue pressures in all compartments for each segment of the dive.

## **Dive Segments**

For analysis purposes any dive is broken down into segments. Each segment is either a constant depth segment or a continuous ascent/descent segment. For example a dive to 30m / 100ft might consist of 5 segments as follows;

A descent segment (assuming immediate descent is switched off)
A constant depth segment for the bottom time at 30m / 100ft
An ascent segment from the bottom to the 6m / 10ft stop
A constant depth segment for the deco stop
An ascent segment for the ascent from the deco stop to the surface

## Ascent or Descent segment Information

The first two columns of the Analysis chart (as shown in the red rectangle) give information about the segments as follows;

Decompression Planner - [Mission: 1 Dive: 1 - Analysis]											
File Options !	<u>D</u> ive <u>I</u> o	ols <u>G</u> raph	<u>W</u> indow	<u>H</u> elp							
			Cpt 1	Cpt 2	Cpt 3	Cpt 4	Cpt 5	Cpt 6	Cpt 7	Cpt 8	Cpt 9
SEG: 1	DESC	PHe	.0	.0	.0	.0	.0	.0	.0	.0	.0
START DEPTH	0	PN2	9.4	8.7	8.3	8.1	7.9	7.8	7.7	7.7	7.6
FINAL DEPTH	36	PHe+PN2	9.4	8.7	8.3	8.1	7.9	7.8	7.7	7.7	7.6
RATE	30	%Ambient	20.4	18.9	18.0	17.5	17.2	16.9	16.8	16.7	16.6
SEG TIME	1.2	He Grad	.0	.0	.0	.0	.0	.0	.0	.0	.0
RUN TIME	1.2	N2 Grad	22.5	23.2	23.6	23.8	24.0	24.1	24.2	24.2	24.2
MIX 02	30%	M-Value	94.4	80.8	72.5	66.5	63.4	60.3	58.0	56.3	54.9
MIX He	0%	%M-Value	10.0	10.8	11.5	12.1	12.5	13.0	13.3	13.7	13.9
		%M-V Grad	-76.1	-107.8	-143.4	-186.7	-220.8	-270.5	-323.1	-379.1	-437.6

SEG:1	The segment number. Segments count from 1 upward. The segment is either ASC or DESC for an ascent or descent segment
START DEPTH	The starting depth for the ascent or descent
FINAL DEPTH	The final depth for the ascent or descent
RATE	The ascent or descent rate used for this segment (These rates are set from the preferences option on the File menu)
SEG TIME	The duration of this segment in minutes
RUN TIME	The total accumulated dive time at the end of the segment
MIX 02	The percentage of Oxygen in the breathing gas during this segment
MIX He	The percentage of Helium in the breathing gas during this segment

### **Constant Depth or Decompression stop segment Information**

**SEG:2** The segment number. The segment is shown as a STOP

segment

**CONST DEPTH** The constant depth for this segment

**PO2 ATA** The partial pressure of Oxygen at this depth (in ATA)

**SEG TIME** The duration of this segment in minutes

**RUN TIME** The total accumulated dive time at the end of the segment

MIX 02 The percentage of Oxygen in the breathing gas during this

segment

MIX He The percentage of Helium in the breathing gas during this

segment

## **Compartment Information**

<u>File</u> Options <u>I</u>	<u>D</u> ive <u>I</u> o	ols <u>G</u> raph	<u>W</u> indow	<u>H</u> elp				
			Cpt 1	Cpt 2	Cpt 3	Cpt 4	Cpt 5	Cpt 6
SEG: 9	ASC	PHe	.0	.0	.0	.0	.0	.1
START DEPTH	9	PN2	24.3	25.6	24.9	22.8	20.2	17.
FINAL DEPTH	6	PHe+PN2	24.3	25.6	24.9	22.8	20.2	17.
RATE	10	%Ambient	150.5	158.6	154.2	141.5	125.2	109.
SEG TIME	.3	He Grad	.0	.0	.0	.0	.0	
RUN TIME	35.3	N2 Grad	-24.3	-25.6	-24.9	-22.8	-20.2	-17.
MIX 02	100%	M-Value	40.6	34.8	31.0	28.2	26.5	24.
MIX He	0%	%M-Value	59.8	73.6	80.4	81.0	76.2	71.
GF Used	86	%M-V Grad	33.3	50.8	59.0	55.6	39.2	18.
SEG: 10	STOP	PHe	.0	.0	.0	.0	.0	
CONST DEPTH	6	PN2	15.4	19.2	20.7	20.2	18.6	16.
PO2 ATA	1.59	PHe+PN2	15.4	19.2	20.7	20.2	18.6	16.
SEG TIME	2.7	%Ambient	95.3	119.2	128.4	125.1	115.1	103.
RUN TIME	38.0	He Grad	.0	.0	.0	.0	.0	
MIX 02	100%	N2 Grad	-15.4	-19.2	-20.7	-20.2	-18.6	-16.
MIX He	0%	M-Value	40.6	34.8	31.0	28.2	26.5	24.
		%M-Value	37.8	55.3	66.9	71.6	70.0	67.
		%M-V Grad	-3.1	16.6	30.9	33.6	23.4	6.

The remaining columns of the analysis show information for each of the 16 theoretical tissue compartments. The column headings are from 'Cpt 1', (the fastest tissue, shown in the red rectangle above) to 'Cpt 16', (the slowest tissue). Each segment has 9 rows of data for each compartment as follows;

**PHe** The pressure of Helium in the compartment measured in

MSW (Meters of sea water) or FSW (Feet of sea water)

**PN2** The pressure of Nitrogen in the compartment measured in

MSW (Meters of sea water) or FSW (Feet of sea water)

PHe+PN2 The sum of the pressures of Helium and Nitrogen in the

compartment as given in the previous two rows

**%Ambient** The percentage of the inert gas pressures in the

compartment, as compared to the ambient pressure.

He Grad

The Helium gradient shows the difference in pressure between the current compartment helium pressure and the fully saturated compartment helium pressure. Once the tissue is fully saturated this value will show zero. A positive value means the compartment has a gradient driving the gas into it. In other words the compartment is on-gassing. A negative value means the compartment has a gradient driving the gas out of it. In other words the compartment is off-gassing

N2 Grad

The Nitrogen gradient shows the difference in pressure between the current compartment nitrogen pressure and the fully saturated compartment nitrogen pressure. As with the H2 Gradient; Once the tissue is fully saturated this value will show zero. A positive value means the compartment has a gradient driving the gas into it. In other words the compartment is on-gassing. A negative value means the compartment has a gradient driving the gas out of it. In other words the compartment is off-gassing

M-Value

The M-Value shows the maximum allowed compartment pressure. This value is a combined value for N2 and He. To see how close to the M-Value a compartment is, compare this value to the PHe+PN2 row

%M-Value

This value shows the percentage of the M value reached by the compartment. This value is calculated by comparing the PHe+PN2 value to the M-Value. It is a measure of how close to the M-Value the inert gas pressure is. A value of 100 would mean that the compartment pressure has reached it's maximum possible theoretical tolerance

%M-V Grad

This value shows how far into the decompression zone the compartment is. The percentage is a measure of the compartment insert gas pressure as compared with the difference between the M-Value and the ambient pressure. A negative value here means that the compartment pressure is below ambient and is therefore still on-gassing. A positive value here means that the compartment pressure is above ambient (in the decompression zone) and is therefore offgassing. A value of 100 would mean that the compartment pressure has reached it's maximum possible theoretical tolerance

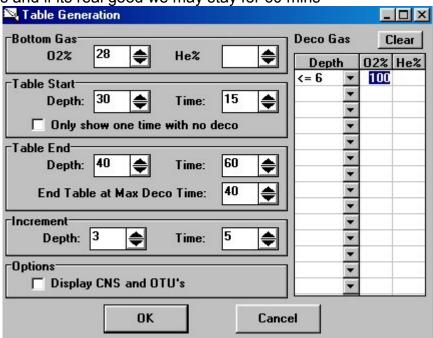
The values in each of the compartments are compared to determine the highest value and this value is shown in blue. This allows you to see immediately the leading tissue compartment for each segment.

### 7.5 Dive Table Generation

Note: Dive table generation with Deco Planner set to work in feet, follows exactly the same process as detailed below. In order to keep files sizes to a minimum only metric pictures have been included.

The diagram below shows the table set up for a dive. In the example we are planning a wreck dive where the depth is unknown, but is thought to be between 30 and 40m. The planned dive is 40 minutes however we may call the dive after

15 minutes and if its real good we may stay for 60 mins



The next entry is the depth increments that are to be planned i.e. in the example shown above, Deco Planner will calculate a table every 3 m between table start depth and table end depth

The last entry is the time increments that are to be planned i.e. in the example shown, Deco Planner will calculate a table every 5mins between table start time and table end time

To reduce the number of tables calculated the option of "only show one time with no deco" can be set - if the depth/time tables being calculated will result in a lot of no decompression dives, Deco Planner will only show the No decompression limits and not output any dive that is less than this.

As well as choosing the dive bottom mix (in the example a 28% EAN mix is used), the user can choose to use multiple decompression mixes, the diagram above, shows that all decompression less than and equal to 6m is to be completed on 100 % Oxygen (in blue).

Upon hitting the OK button Deco Planner will start calculating the dive tables requested.

Time	15	20	25	30	35	40	45	50	55	60	28%	2 0	
12	1.0			1	1	1	1	1	2	3	28%		1
9	1	1	1	1	1	1	1	3	3	3	28%		1 1
6	1	1	1	1	2	3	5	6	8	9	100%		
otal	2	2	2	3	4	5	7	10	<13>	<15>			
33M	Table	: ZHL	.16B 9	afety:	OFF	Desce	ent: N	ormal	GF Lo	%: 30	GF Hi%	: 100	
Time	15	20	25	30	35	40	45	50	55	60	28%		
15						1	1	1	1	1	28%		1 1
12	1	1	1	1	1	1	1	1	2	3	28%		
9	1	1	1	1	1	1	2	4	4	4	28%		
6	1	1	1	2	4	5	7	9	10	12	100%		
otal	2	3	3	4	6	8	11	<15>	<17>	<20>			
_					1								

In the diagram above it is seen that some of the information is in a red box with <> signs around the number. This is to indicate that the user does not have enough gas to complete the dive based upon cylinder size, reserves and breathing parameter settings set in the user <u>preferences section</u>.

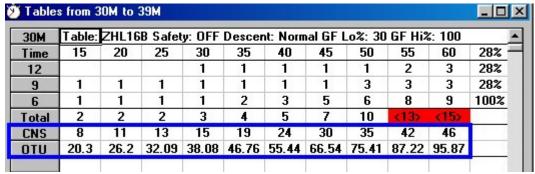
The dive table contains a lot of additional information to assist in dive planning. In the following diagram, sections have been highlighted to assist in the description of the output

Time	15	20	25	30	35	40	45	50	55	60	28%		T	
12	1.0			1	1	1	1	1	2	3	28%			-
9	1	1	1	1	1	1	1	3	3	3	28%			1
6	1	1	1	1	2	3	5	6	8	9	100%			-
Total	2	2	2	3	4	5	7	10	<13>	<15×				
33M	Table	: ZHL	.16B 9	afety:	OFF	Desce	ent: N	ormal	GF Lo	%: 30	GF Hi%	: 100		
Time	15	20	25	30	35	40	45	50	55	60	28%			Ī
15	Ü					1	1	1	1	1	28%			Ī
12		1	1	1	1	1	1	1	2	3	28%			
9	1	1	1	1	1	1	2	4	4	4	28%			
6	1	1	1	2	4	5	7	9	10	12	100%			
Total	2	3	3	4	6	8	11	<15>	<17>	<20>				I
														1

The pink section details the preferences set in calculating the dive table (i.e. which model used gradient factors etc)

The yellow section indicates which gas is being breathed at which depth

The green section shows the total DECOMPRESSION time for each dive time



The diagram above shows the same dive planned, however this time the user selected the option in the table generator window to display oxygen information as well shown in blue.

# 7.6 Repetitive dives

Deco Planner allows the user to plan repetitive dives over any period. The theory behind repetitive dives is based on Bühlmann's pulmonary shunt model. During a surface interval, the elimination of gas is delayed due to the pulmonary shunt mechanism and the gas loading remain higher than a normal set of calculations would conventionally calculate. Accordingly, on repetitive profiles, it will mean either less no-stop time or longer deco time.

Deco Planner runs gas loading calculations for all the compartments on a CONTINUOUS basis which may cover days or even weeks! The gas loading are calculated and updated within a MISSION and are calculated dependent on what the diver is doing (surface interval or diving)

At the end of the first dive of a mission (i.e. after all decompression) each compartment will have a certain loading of helium and nitrogen. Generally, after oxygen decompression, the fast compartments will be completely empty of helium and nitrogen and they will ON-GAS with nitrogen during the surface interval! The slowest compartment, 635 min for nitrogen, takes over 2-1/2 days to completely off-gas so any repetitive dive will halt that process.

Until a better implementation of the pulmonary shunt model is developed, Deco Planner behaves as if the surface interval is at one meter breathing 21 % (i.e. Air) as such the tissues never clear completely, as such once a surface interval of 3-4 hours is exceeded the penalty on the subsequent dive is the same whether the diver waits 4 or 24 hours

# **8 Decompression Theory**

We are please to be able to reproduce a number of articles from experts around the globe as part of this manual. This software package would not have been possible, without these articles and the guidance provided by their authors.

Erik C. Baker is an electrical engineer with an architecture/engineering firm in Pennsylvania. He pursues research into decompression and diving physiology as a hobby, and has developed several FORTRAN computer programs for decompression calculation and analysis. Erik is a certified cave diver and trimix diver.

**Understanding M Values : Erik C Baker** 

**Deep Stops Explained : Erik C Baker** 

# 8.1 Understanding M Values : Erik C Baker

In conjunction with an array of hypothetical "tissue" compartments, gas loading calculations and M-values compose the major elements of the dissolved gas or "Haldanian" decompression model. Through the use of widely-available desktop computer programs, technical divers rely on this model for their decompression safety. A good understanding of M-values can help divers to determine appropriate conservatism factors and evaluate the adequacy of various decompression profiles for a particular dive.

What are M-values? The term "M-value" was coined by Robert D. Workman in the mid-1960's when he was doing decompression research for the U.S. Navy Experimental Diving Unit (NEDU). Workman was a medical doctor with the rank of Captain in the Medical Corps of the U.S. Navy.

The "M" in M-value stands for "Maximum." For a given ambient pressure, an M-value is defined as the maximum value of inert gas pressure (absolute) that a hypothetical "tissue" compartment can "tolerate" without presenting overt symptoms of decompression sickness (DCS). M-values are representative limits for the tolerated gradient between inert gas pressure and ambient pressure in each compartment. Other terms used for M-values are "limits for tolerated overpressure," "critical tensions," and "supersaturation limits." The term M- value is commonly used by decompression modelers.

### HISTORICAL BACKGROUND

In the dissolved gas or "Haldanian" decompression model, gas loading calculations for each hypothetical "tissue" compartment are compared against "ascent limiting criteria" to determine the safe profile for ascent. In the early years of the model, including the method developed by John S. Haldane in 1908, the ascent limiting criteria was in the form of "supersaturation ratios." For example, Haldane found that a diver whose "tissues" were saturated by breathing air at a depth of 33 fsw could ascend directly to the surface (sea level) without experiencing symptoms of DCS. Because the ambient pressure at 33 fsw depth is twice that at sea level, Haldane concluded that a ratio of 2:1 for tolerated overpressure above ambient could be used as the ascent limiting criteria. This approximate ratio was used by Haldane to develop the first decompression tables. In later years, and up until the 1960's, other ratios were used by various modelers for the different half-time compartments. Most of the U.S. Navy decompression tables were calculated using this supersaturation ratio method.

However, there was a problem. Many of the tables produced by this method were deficient when it came to deeper and longer dives. Robert Workman began a systematic review of the decompression model including previous research that had been performed by the U.S. Navy. He arrived at some important conclusions. First of all, he recognized that Haldane's original ratio of 2:1 (based

on air) was really a ratio of 1.58:1 if you considered only the partial pressure of the inert gas in air nitrogen. [By that time in decompression research it was known that oxygen was not a significant factor in DCS; it was the inert gases like nitrogen and helium that were the culprits.] In his review of the research data, Workman found that the "tissue ratios" for tolerated overpressure varied by half-time compartment and by depth. The data showed that the faster half-time compartments tolerated a greater overpressure ratio than the slower compartments, and that for all compartments the tolerated ratios became less with increasing depth. Then, instead of using ratios, Workman described the maximum tolerated partial pressure of nitrogen and helium for each compartment at each depth as the "M-value." Next, he made a "linear projection" of these M-values as a function of depth and found that it was a reasonably close match to the actual data. He made the observation that "a linear projection of M-values is useful for computer programming as well."

### THE WORKMAN M-VALUES

Workman's presentation of M-values in the form of a linear equation was a significant step in the evolution of the dissolved gas decompression model. His M-values established the concept of a linear relationship between depth pressure [or ambient pressure] and the tolerated inert gas pressure in each "tissue" compartment. This concept is an important element of the present-day dissolved gas model as applied by a variety of modelers.

Workman expressed his M-values in the slope-intercept form of a linear equation (see Figure 1). His surfacing value was designated Mo [pronounced "M naught"]. This was the intercept value in the linear equation at zero depth pressure (gauge) at sea level. The slope in the linear equation was designated M [pronounced "delta M"] and represented the change in M-value with change in depth pressure.

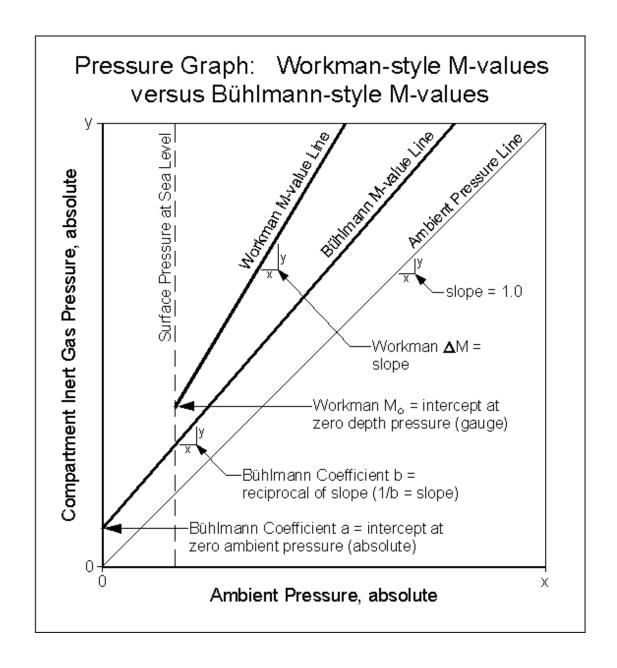
### THE BUHLMANN M-VALUES

Professor Albert A. Bühlmann, M.D., began doing decompression research in 1959 in the Laboratory of Hyperbaric Physiology at the University Hospital in Zurich, Switzerland. Bühlmann continued his research for over thirty years and made a number of important contributions to decompression science. In 1983 he published the first edition (in German) of a successful book entitled Decompression Decompression Sickness. An English translation of the book was published in 1984. Bühlmann's book was the first nearly complete reference on making decompression calculations that was widely-available to the diving public. As a result, the "Bühlmann algorithm" became the basis for most of the world's in-water decompression computers and do-it-yourself desktop computer programs. Three more editions of the book were published in German in 1990, 1993, and 1995 under the name Tauchmedizin or "Diving Medicine." [An English translation of the 4th Edition of the book (1995) is in preparation for publication].

Bühlmann's method for decompression calculations was similar to the one that Workman had prescribed. This included M-values which expressed a linear relationship between ambient pressure and tolerated inert gas pressure in the hypothetical "tissue" compartments. The major difference between the two approaches was that Workman's M-values were based on depth pressure (i.e. diving from sea level) and Bühlmann's M-values were based on absolute pressure (i.e. for diving at altitude). This makes sense, of course, since Workman was concerned with the diving activities of the U.S. Navy (presumably performed at sea level) while Bühlmann was concerned with diving activities in the high mountain lakes of Switzerland.

Bühlmann published two sets of M-values which have become well-known in diving circles; the ZH-L12 set from the 1983 book, and the ZH-L16 set(s) from the 1990 book (and later editions). The "ZH" in these designations stands for "Zurich" (named after his hometown), the "L" stands for "limits," and the "12" or "16" represents the number of pairs of coefficients (M-values) for the array of half-time compartments for helium and nitrogen. The ZH-L12 set has twelve pairs of coefficients for sixteen half-time compartments and these M-values were determined empirically (i.e. with actual decompression trials). The ZH-L16A set has sixteen pairs of coefficients for sixteen half-time compartments and these Mvalues were mathematically-derived from the half-times based on the tolerated surplus volumes and solubilities of the inert gases. The ZH-L16A set of M-values for nitrogen is further divided into subsets B and C because the mathematicallyderived set A was found empirically not to be conservative enough in the middle compartments. The modified set B (slightly more conservative) is suggested for table calculations and the modified set C (somewhat more conservative) is suggested for use with in water decompression computers which calculate in real-time.

Similar to the Workman M-values, the Bühlmann M-values are expressed in the slope-intercept form of a linear equation (see Figure 1). The Coefficient a is the intercept at zero ambient pressure (absolute) and the Coefficient b is the reciprocal of the slope. [Note: the Coefficient a does not imply that humans can withstand zero absolute pressure! This is simply a mathematical requirement for the equation. The lower limit for ambient pressure in the application of the Bühlmann M-values is on the order of 0.5 atm/bar.]



## Workman Definitions:

M = tolerated inert gas pressure (absolute) in hypothetical "tissue" compartment

Depth = depth pressure (gauge) measured from surface at sea level

Tolerated Depth = tolerated depth pressure (gauge) measured from surface at sea level

M<sub>o</sub> = intercept at zero depth pressure (gauge); surfacing M-value at sea level

▲M = slope of M-value line.

## Bühlmann Definitions:

P<sub>t.tol.</sub>i.g. = tolerated inert gas pressure (absolute) in hypothetical "tissue" compartment

P<sub>t</sub>i.g. = inert gas pressure (absolute) in hypothetical "tissue" compartment

P<sub>amb.</sub> = ambient pressure (absolute)

P<sub>amb.tol.</sub>= tolerated ambient pressure (absolute)

a = intercept at zero ambient pressure (absolute)

b = reciprocal of slope of M-value line

atics
x = (y - b) / m format
Tolerated Depth = (M - $M_{\circ}$ ) / $\Delta$ M
$P_{amb.tol.} = (P_{t.}i.g a) \cdot b$
Bühlmann to Workman
$M_o = a + P_{amb. (surface at sea level)} / b$
△M = 1 / b

#### DCAP AND DSAT M-VALUES

Many technical divers will recognize the 11F6 set of M-values used by Hamilton Research's Decompression Computation and Analysis Program (DCAP). This set or "matrix" of M-values was determined by Dr. Bill Hamilton and colleagues during development of new air decompression tables for the Swedish Navy. In addition to air diving, the 11F6 M-values have worked well for trimix diving and are the basis for many custom decompression tables in use by technical divers.

Many sport divers are familiar with the Recreational Dive Planner (RDP) distributed by the Professional Association of Diving Instructors (PADI). The M-values used for the RDP were developed and tested by Dr. Raymond E. Rogers, Dr. Michael R. Powell, and colleagues with Diving Science and Technology Corp. (DSAT), a corporate affiliate of PADI. The DSAT M-values were empirically verified with extensive in-water diver testing and Doppler monitoring.

### COMPARISON OF M-VALUES

Tables 1 thru 4 present a comparison of M-values for nitrogen and helium between the various Haldanian decompression algorithms discussed in this article. All M-values are presented in Workman-style format. An evolution or refinement in the M-values is evident from Workman (1965) to Bühlmann (1990).

	UUo	rkmar	1	Т	Bühlm	ann Zh	<u>Vmerican</u> I-L		SAT				MP118		,,,,		Bühlm	ian n ZH-	L16	
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				5	26.5	63.5	1.1834	4	30	59.74	3	25	62.3	1.08	5	27.0	62.3	62.3	60.8	1.23
4	40	56	1.4	6	37	57.3	1.1628	5	40	55.73					6	38.3	58.5	57.4	55.6	1.18
				7	53	53.2	1.1494	6	60	51.44	4	55	48.6	1.06	7	54.3	55.2	54.1	52.3	1.15
5_	80	54	1.3	8	79	51.9	1.1236	7	80	49.21					8	77.0	52.3	51.7	50.1	1.12
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_				13	304	42.6	1.0395	<del>  </del>			8	285	44.0	1.0	13	305	44.5	44.1	44.1	1.05
				14	397	42.6	1.0395	13	360	43.81	9	385	44.0	1.0	14	390	43.5	43.5	43.1	1.04
				15	503	42.6	1.0395	14	480	43.40	10	520	44.0	1.0	15	498	42.6	42.6	42.4	1.04
				16	635	42.6	1.0395								16	635	41.8	41.8	41.8	1.03
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pt   1   2   5   6	Table 1000 1000 1000 1000 1000 1000 1000 10	e 2: rkmar es (19 Mo msw 31.7 26.8 21.9 17.0	Comp 1 965) AM slope 1.8 1.6 1.5 1.4	Cpt No. 1 2 3 4 5 6 7 8	Bühlm M-val HT min 2.65 7.94 12.2 18.5 26.5 37 53 79 1114	Eu ann 2 (19)  Mo msw 34.2  27.2  22.9  21.0  19.3  17.4  16.2  15.8	Alue s for repear S (14 m) (15	or Ni y stem D M-0 Cpt No. 1 2 3 4 5 6 7 8 9	troge   1 of Pri   1 o	en Betressure L RDP (1987) Mo msw 30.42 25.37 20.54 18.34 17.11 15.79 15.11 14.69	Oleerinits - Cpt No.	n Va - mete DCAP M-vali HT min 5 10 25 55	mous rous rous rous rous rous rous rous r	Halda a water F6 88)  AM slope  1.30 1.05  1.06 1.04	Cpt No. 1 1 5 6 7 8 9	HT min  4.0 5.0 12.5 18.5 27.0 38.3 77.0 109	Bühim M-va A M o msw 32.4 29.6 25.4 22.5 20.3 19.0 17.8 16.8 15.9 15.2	ssion sann 2H- lues (199 B Mo msw 32.4 29.6 25.4 22.5 20.3 19.0 17.5 16.5 15.7	Agoriti L16 90) C Mo ssw 32.4 29.6 25.4 22.5 20.3 18.5 16.9 15.2 14.7	1.90 1.38 1.38 1.27 1.23 1.18 1.15 1.12
pt lo. 5	Table 1000 1000 1000 1000 1000 1000 1000 10	e 2: rkmar es(19 Mo msw 31.7 26.8 21.9 17.0 16.4 15.8 15.5	Comp 1 1065) AM 5lope 1.8 1.6 1.5 1.4 1.3	Cpt No. 1 2 3 4 4 5 6 7 8 9 10	7.94 12.2 18.5 26.5 37 53 79 114	Mo msw 34.2 27.2 22.9 21.0 19.3 17.4 16.2 15.8 15.8 15.8 15.8	alue s for repear S (HL 12) (12) (13) (14) (15) (15) (15) (15) (15) (15) (15) (15	or No. Opt No.	troge to of Pri SAT labes HT min 5 10 20 30 40 60 80 100 120	en Betressure URDP (1987)  Momsw  30.42 25.37  20.54 18.34 17.11 15.79 15.11 14.69 14.41	Oleen Inits - Cpt No.	n Va - mete DCAP M-vali HT min 5 10 25 55	mous roots of se MM11 roots (19 Mm msw 19.04 ft 14.78 ft 13.92 ft 13.66	Halida a water F6 (888)	Cpt No.  1 1b 2 3 4 5 6 7 8 9 10	HT min  4.0 5.0 12.5 18.5 27.0 38.3 54.3 77.0 109	Bühim M-va A Momsw 32.4 29.6 25.4 22.5 20.3 19.0 17.8 16.8 15.9 15.2	ssion  sann 2H- lues (19:  B	Agoriti L16 90) C Momsw 32.4 29.6 25.4 22.5 20.3 18.5 16.9 15.9 14.7	1.90 1.79 1.53 1.38 1.27 1.23 1.18 1.15 1.12
pt 10.	1000 000 000 000 000 000 000 000 000 00	e 2: rkmar es(19 Mo msw 31.7 26.8 21.9 17.0 16.4 15.8 15.5 15.5	Com	Cpt No. 1 2 3 4 5 6 6 7 8 9 10 11	Bühlm M-val HT min 2.65 7.94 12.2 18.5 26.5 79 114 146 185	Mo msw 34.2 27.2 22.9 21.0 19.3 17.4 16.2 15.8 15.3 15.3 15.3	alue s for ropean S (H. 1) (1883)  AM slope 1.2195 1.2121 1.1976 1.1834 1.1236 1.1236 1.1236 1.10707 1.0707	or No.  Cpt No.  1 2 3 4 5 6 7 8 9 10 111	troge to of Pri SAT labes HT min 20 30 40 60 80 100 120 200	en Betriessure L RDP (1987) Momsw 30,42 25,37 20,54 18,34 17,11 15,79 15,11 14,69 14,41 14,06	Oleerinits - Cpt No.	n Va - mete DCAP M-vali HT min 5 10 25 55	mous rous rous rous rous rous rous rous r	Halda a water F6 88)  AM slope  1.30 1.05  1.06 1.04	Cpt No. 1 1 5 6 7 8 9 10 11	HT min  4.0 5.0 12.5 18.5 27.0 38.3 54.3 77.0 109	Bühim M-va A M o msw 32.4 29.6 25.4 22.5 19.0 17.8 16.8 15.9 15.2 14.6 14.2	SSION  Tann 2H-  Jues (19:  B  Mo msw  \$2.4  29.6  25.4  22.5  20.3  19.0  17.5  16.5  15.7  15.2  14.6  14.2	Ago ritl L16 90) C Mo msw 32.4 29.6 25.4 22.5 20.3 18.5 16.9 15.9 15.2 14.7	1.90 1.79 1.53 1.38 1.12 1.13 1.15 1.12 1.09
pt 10.	Table 1000 1000 1000 1000 1000 1000 1000 10	e 2: rkmar es(19 Mo msw 31.7 26.8 21.9 17.0 16.4 15.8 15.5	Comp 1 1065) AM 5lope 1.8 1.6 1.5 1.4 1.3	Cpt No. 1 2 3 4 5 6 6 7 8 9 10 111 12	Bühlm M-val HT min 2.65 7.94 12.2 18.5 26.5 79 114 146 185 238	Mo msw 34.2  27.2 22.9 21.0 19.3 17.4 16.2 15.8 15.3 14.4	alue s for ropean S (H. 17) (183)  AM slope 1.2195 1.2195 1.2121 1.1976 1.1834 1.1628 1.1494 1.1236 1.1236 1.10707 1.00707 1.00593	or No. Opt No.	troge to of Pri SAT labes HT min 5 10 20 30 40 60 80 100 120	en Betressure URDP (1987)  Momsw  30.42 25.37  20.54 18.34 17.11 15.79 15.11 14.69 14.41	Oleen Inits - 1	n Va mete DCAP M-vali HT min 5 10 25 55 95 145 200	mous (19 Mo msw 19.04	Halda a water F6 888)  AM Slope 1.08 1.06 1.04 1.02 1.01	Cpt No.  1 1b 2 3 4 5 6 7 8 9 10 11 12	HT min  4.0 5.0 8.0 12.5 27.0 38.3 77.0 109 146 187 239	Bühim M-va A Momsw 32.4 29.6 25.4 22.5 20.3 19.0 17.8 16.8 15.9 15.2	ssion 24- lues (19: 8 Mo msw 32.4 29.6 25.4 22.5 20.3 19.0 17.5 16.5 15.7 15.2	Agoriti L16 100) C M <sub>0</sub> msw 32.4 29.6 22.5 20.3 118.5 16.9 15.9 15.2 14.7 14.3 14.0 13.7	1.90 1.79 1.53 1.38 1.27 1.23 1.18 1.15 1.12 1.09
pt lo. 1 2 3 4 5 6 7 8	1000 000 000 000 000 000 000 000 000 00	e 2: rkmar es(19 Mo msw 31.7 26.8 21.9 17.0 16.4 15.8 15.5 15.5	Com	Cpt No. 1 2 3 4 5 6 7 8 9 10 11 12 13	### REPART OF THE PART OF THE	F M-W Eu	alue s for ropean S III 13	or Ni ystem 0 M-0 Cpt No. 1 2 3 4 5 6 7 8 9 10 11 12	trogs of Prosent sealures HT min 5 10 20 30 40 60 80 100 120 160 200 240	en Beti essure t RDP (1987) Mo msw 30.42 25.37 20.54 18.34 17.11 14.69 14.41 14.06 13.84 13.84	Oleen Inits -	n Vanmete DCAP M-vali HT min 5 10 25 55 95 145 200	mous (19 mou	Halda water F6 888)  AM 50000  1.30 1.08 1.06 1.04 1.02 1.01	Cpt No. 1 1 5 6 7 8 9 10 11 12 13	HT min  4.0 5.0 8.0 12.5 27.0 38.3 77.0 109 146 187 239 305	Bühim M-ua A M o msw 32.4 29.6 25.4 22.5 19.0 17.8 16.8 15.2 14.6 14.2 13.9 13.5	ssion	Ago ritt L16 B0) C Mo msw 32.4 29.6 20.3 18.5 16.9 15.9 14.7 14.3 14.0 13.7	1.90 1.79 1.53 1.38 1.27 1.23 1.18 1.15 1.12 1.09
pt 10.	1000 000 000 000 000 000 000 000 000 00	e 2: rkmar es(19 Mo msw 31.7 26.8 21.9 17.0 16.4 15.8 15.5 15.5	Com	Cpt No. 1 2 3 4 5 6 7 8 9 10 11 12 13 14	7.94 12.2 18.5 26.5 37 53 79 114 146 148 288 304 397	F M-W Eu ann ZF Eu ues (19 Mo msw 34.2 22.9 21.0 19.3 15.8 15.8 15.3 15.3 15.3 12.9 12.9 12.9 12.9	Alue s for ropean S III 1883)  AM slope 1.2195 1.2195 1.2195 1.1976 1.1834 1.1628 1.1494 1.1236 1.1236 1.0707 1.0707 1.0593 1.0395 1.0395	or No.  Cpt No.  1 2 3 4 5 6 7 8 9 10 111	troge to of Pri SAT labes HT min 20 30 40 60 80 100 120 200	en Beti essure t RDP (1987) Mo msw 30.42 25.37 20.54 17.11 15.79 15.11 14.06 13.84 13.69	Oleen Inits - 1	n Vanmete DCAP M-vali HT min 5 10 25 55 95 145 200 285 385	mous rs of se MM11 res (19 M m msw 19.04 11.78 11.90 11.78 11.90 11.78 11.50 11.50 11.50	Halida as water F6 888) AM slope 1.30 1.05 1.04 1.04 1.02 1.01	Cpt No. 1 1 5 6 7 8 9 10 11 12 13 14	HT min  4.0 5.0 8.0 12.5 27.0 38.3 77.0 109 146 187 239	Bühim M-ua A M o msw 32.4 22.5 25.4 22.5 15.9 15.2 14.6 14.2 13.9 13.5 13.2	ssion 24- lues (19:  B  Mo msw  32.4 29.6 25.4 22.5 20.3 19.0 17.5 16.5 15.7 15.2 14.6 14.2 13.2	L16 B00 C M <sub>0</sub> msw 32.4 22.5 20.3 18.5 16.9 15.9 14.7 14.3 14.0 13.7 13.4	1.90 1.79 1.53 1.38 1.27 1.23 1.15 1.15 1.10 1.09
,	1000 000 000 000 000 000 000 000 000 00	e 2: rkmar es(19 Mo msw 31.7 26.8 21.9 17.0 16.4 15.8 15.5 15.5	Com	Cpt No. 1 2 3 4 5 6 7 8 9 10 11 12 13	### REPART OF THE PART OF THE	F M-W Eu	alue s for ropean S III 13	or Ni y stem D M-v (Cpt No	######################################	en Beti essure t RDP (1987) Mo msw 30.42 25.37 20.54 18.34 17.11 14.69 14.41 14.06 13.84 13.84	Neer   Ne	n Vanmete DCAP M-vali HT min 5 10 25 55 95 145 200	mous (19 mou	Halda water F6 888)  AM 50000  1.30 1.08 1.06 1.04 1.02 1.01	Cpt No. 1 1 5 6 7 8 9 10 11 12 13	HT min  4.0 5.0 8.0 12.5 18.5 27.0 38.3 77.0 109 146 187 239 305 390	Bühim M-ua A M o msw 32.4 29.6 25.4 22.5 19.0 17.8 16.8 15.2 14.6 14.2 13.9 13.5	ssion	Ago ritt L16 B0) C Mo msw 32.4 29.6 20.3 18.5 16.9 15.9 14.7 14.3 14.0 13.7	

		Tab	le 3:	Con	npari	son o	FM-vali	ues:	for Hel	ium						
	Betw	jeen	Vario	us F	Halda	nian	Decom	pres	sion A	lgorith	nms					
_	1016	rkm an					Inits -fee		ea water Bühlman		100					
١.						iann ZH										
-	A-valu	_		0.00	M-Vai	ues (19				es (199	_					
Cpt No.		M <sub>o</sub> fsw	<u>∆</u> M slope	No.		M <sub>o</sub> fsw	<u>∆</u> M slope	Cpt No.	HT min	M o fsw	<u>A</u> M slope					
				1	1.0	111.9	1.2195	1	1.51	134.5	2.3557					
$\vdash$				<del>'</del>				10	1.88	121.9	2.0964					
$\vdash$				2	3.0	89.1	1.2195	2	3.02	102.5	1.7400					
1	5	86	1.5	3	4.6	75.2	1,2121	3	4.72	89.4	1.5 321					
Ė				4	7.0	68.8	1.1976	4	6,99	79.7	1.3845					
2	10	74	1.4	5	10	63.5	1,1834	5	10.21	73.6	1.3189					
Ť				6	14	57.3	1.1 628	6	14.48	68.2	1.2568					
3	20	66	1.3	7	20	53.2	1.1 494	7	20.53	63.7	1.2079					
$\vdash$				8	30	51.9	1.1 236	8	29.11	59.8	1.1 692					
4	40	60	1.2	9	43	51.9	1.1 236	9	41.20	57.1	1.1 419					
Ė				10	55	52.4	1.0799	10	55.19	55.1	1.1 232					
5	80	56	1.2	11	70	52.4	1.0799	11	70.69	54.0	1.1115					
Ė				12	90	52.4	1.0799	12	90.34	53.3	1.1 022					
6	120	54	1.2	13	115	52.4	1.0799	13	115.29	53.1	1.0963					
7	160	54	1.1	14	150	52.4	1.0799	14	147.42	52.8	1.0904					
8	200	53	1.0	15	190	52.4	1.0799	15	188.24	52.6	1.0850					
9	240	53	1.0	16	240	52.4	1.0799	16	240.03	52.3	1.0791					
Cpt = Compartment HT = Half-time <u>A</u> M = slope of M-value line																
	. Me	Տ= Տա	rfacing I	M-val	ue (se	a level	= 1 atm =	Mo= Surfacing M-value (sea level = 1 atm = 33 fsw = 1.01325 bar)								
Г																
	Table 4: Comparison of M-values for Helium															
Between Various Haldanian Decompression Algorithms									for Hel	ium						
		jeen	Vario	us F	Halda	nian	FM-vali Decom	ues: pres	for Hel sion A	ium Igoritk	nms					
	E	Jeen Urope	Vario an Syst	us F em o	Halda F Pres	nian sure Un	FM-vali Decom its-mete	ues pres os of	for Hel sion A sea wate	ium Igoritk :r(msw	nms )					
_	UVo	Jeen Urope rkman	Vario an Syst I	us F em o	dalda FPres Bühlm	nian sure Un iann ZH	M-valu Decomp its-mete I-L <sub>in</sub>	ues pres os of	for Hel sion A sea wate Bühlman	ium Igoritk :r(msw :n ZH-L	1MS ) 16A					
-	E VVo VI-valu	Jeen urope rkman es (19	Vario an Syst 1 165)	us F em o	dalda F Pres Bühlm M-val	nian sure Un lann ZH lues (19	M-valu Decomp its - mete I-L <sub>is</sub> iss)	ues pres is of	for Hel sion A sea wate Bühlman	ium Igorith :r(msw :n ZH-L es (199	nms ) 16A 10)					
Cpt	UVo	Jeen Grope Okman es (19 Mo	Vario an Syst (65) <u>AM</u>	us H em o Cpt	dalda f Pres Bühlm M-val HT	nian sure Un iann ZH	M-vali Decomi its - mete I-L <sub>is</sub> 88) <b>∆M</b>	ues pres os of	for Hel sion A sea wate Bühlman M-valu	ium Igoritk :r(msw :n ZH-L	nms ) 16A (0)					
Cpt	E VVo VI-valu HT	Jeen Grope Okman es (19 Mo	Vario an Syst 1 165)	us F em o	dalda f Pres Bühlm M-val HT	nian sure Un lann ZH lues (19 Mo	M-valu Decomp its - mete I-L <sub>is</sub> iss)	ues pres rs of Cpt	for Hel sion A sea wate Bühlman M-valu HT	ium Igoritk r(msw In ZH-L es (199 Mo	nms ) 16A 10)					
Cpt	E VVo VI-valu HT	Jeen Grope Okman es (19 Mo	Vario an Syst (65) <u>AM</u>	us h em o Cpt No.	dalda f Pres Bühlm M-val HT min	nian sure Un lann ZH lues (19 Mo msw	M-vali Decom its - mete I-L <sub>13</sub> 88) <b>AM</b> slope	pres rs of Cpt No.	for Hel sion A sea wate Bühlman M-valu HT min	ium Igorith Ir (msw In ZH-L es (199 Mo msw 41.0	nms ) 16A 10) AM slope 2.3557					
Cpt	E VVo VI-valu HT	Jeen Grope Okman es (19 Mo	Vario an Syst (65) <u>AM</u>	us h em o Cpt No.	dalda f Pres Bühlm M-val HT min	nian sure Un lann ZH lues (19 Mo msw	M-vali Decom its - mete I-L <sub>13</sub> 88) <b>AM</b> slope	ues pres is of Cpt No.	for Hel sion A sea wate Bühlman M-valu HT min	ium Igorith Ir (msw In ZH-L es (199 Mo msw	nms ) 16A 10) AM slope					
Cpt	E VVo VI-valu HT min	Jeen Urope rkman es (19 Mo msw	Vario an Syst I 165) AM slope	us F em o Cpt No.	Halda F Pres Bühlm M-val HT min 1.0	nian sure Un lann 2H lues (19 Mo msw 34.2	F M-vali Decomplits - mete I-L m (88) AM slope 1.2195	pres pres cof Cpt No.	for Hel sion A sea wate Bühlman M-valu HT min 1.51	ium Igorith Ir (msw In ZH-L es (199 Mo msw 41.0 37.2	nms ) 16A 100)					
Cpt No.	E VVo VI-valu HT	Jeen Grope Okman es (19 Mo	Vario an Syst (65) <u>AM</u>	us h em o Cpt No. 1	Halda F Pres Bühlm M-val HT min 1.0	nian sure Uniann ZH lues (19 Momsw 34.2 27.2	F M-vali Decomits - mete I-L <sub>13</sub> 1883) AM Slope 1.2195	pres pres cpt No. 1 1b	for Hel sion A sea wate Bühlman M-valu HT min 1.51 1.88 3.02	ium Igorith Ir (msw In ZH-L es (199 Mo msw 41.0 37.2	nms ) 16A 10) AM slope 2.3557 2.0964 1.7400					
Cpt No.	E VVo VI-valu HT min	Jeen urope rkman es (19 Mo msw	Vario an Syst I 165) AM slope	us hem o	Halda F Pres Bühlm M-val HT min 1.0 3.0	mian sure Uniann ZH ues (19 Momsw 34.2 22.9 21.0	M-vali Decomits - mete I-L 10 883) AM slope 1.2195 1.2195 1.2121 1.1976	pres rs of Cpt No. 1 1b 2	for Hell sion A sea wate Bühlman M-valu HT min 1.51 1.88 3.02 4.72	ium Igorith Ir (msw In ZH-L es (199 Mo msw 41.0 37.2 31.2	nms ) 16A 10)					
Cpt No.	E VVo VI-valu HT min	Jeen Urope rkman es (19 Mo msw	Vario an Syst 1 165) AM slope	us Hem of Cpt No.	Halda F Pres Bühlm M-val HT min 1.0 3.0 4.6 7.0	nian sure Uniann ZH lues (19 Momsw 34.2 27.2	F M-vali Decomits - mete I-L m 883) AM slope 1.2195 1.2195	pres rs of Cpt No. 1 1b 2 3	for Hell sion A sea wate Bühlman M-valu HT min 1.51 1.88 3.02 4.72 6.99	ium Igorith (msw in ZH-L es (199 M <sub>o</sub> msw 41.0 37.2 31.2 27.2	nms ) 16A, 10) AM slope 2.3557 2.0964 1.7400 1.5321					
Cpt No.	E VVo VI-valu HT min	Jeen urope rkman es (19 Mo msw	Vario an Syst 1 165) AM slope	us hem o	Halda F Pres Bühlm M-val HT min 1.0 3.0 4.6 7.0	nian sure Un lann ZH ues (19 Mo msw 34.2 27.2 22.9 21.0	M-vali Decomits - mete -L m 883) AM slope 1.2195 1.2195 1.2121 1.1976 1.1884	pres rs of Cpt No. 1 1b 2 3 4	for Hel sion A sea wate Bühlman M-valu HT min 1.51 1.88 3.02 4.72 6.99	ium lg o rith r (msw in ZH-L es (199 Mo msw 41.0 37.2 31.2 27.2 24.3 22.4	nms ) 16A 10)  AM slope 2.3557 2.0964 1.7400 1.5321 1.3845 1.3189					
Cpt No.	E (Wo M-valu HT min	Jeen Jurope Ikman es (19 Mo msw 26.2	Vario an Syst  1665)  AM slope  1.5	US  - em o Cpt No. 1 2 3 4 5	Halda f Pres Bühlm M-val HT min 1.0 3.0 4.6 7.0 10	mian sure Unian n ZH sure Unian n ZH sure (19 Momsw 34.2 22.9 21.0 19.3 17.4	M-valid Decominates - meter - L 13	pres rs of Cpt No. 1 1b 2 3 4 5	for Hel sion A sea wate Bühlman M-valu HT min 1.51 1.88 3.02 4.72 6.99 10.21	ium lg o rith r (msw in ZH-L es (199 Mo msw 41.0 37.2 27.2 24.3 22.4 20.8	nms ) 16A 100  AM slope 2.3557 2.0964 1.7400 1.5321 1.3845 1.3189 1.2568					
Cpt No.	E (Wo M-valu HT min	Jeen Jurope Ikman es (19 Mo msw 26.2	Vario an Syst  1.665)  AM slope  1.5  1.4	us l- em o  Cpt No. 1 2 3 4 5 6	Talda   F Pres   Büh Im   M-val   HT   min   1.0   3.0   4.6   7.0   10   14   20	mian sure Unian n ZH ues (19 Momsw 34.2 22.9 21.0 19.3 17.4 16.2	M-valid Decominates - meter - Linus - meter -	pres pres cof No. 1 1b 2 3 4 5	for Hel sion A sea wate Bühlman M-valu HT min 1.51 1.88 3.02 4.72 6.99 10.21 14.48 20.53	ium Jg o rith r (msw in ZH-L es (199 Mo msw 41.0 37.2 31.2 27.2 24.3 22.4 20.8 19.4	100 mms   100 mm					
Cpt No.	E Vilo vi-valu HT min  5	Jeen urope rkman es (19 Mo msw 26.2 22.5	Vario an Syst  1665)  AM slope  1.5	us F em o Cpt No. 1 2 3 4 5 6 7	Halda f Pres Bühlm M-val HT min 1.0 3.0 4.6 7.0 10 14 20 30	mian sure Uni lann ZH wes (19 Mo msw 34.2 27.2 22.9 21.0 19.3 17.4 16.2 15.8	M-vali Decomilits - mete I-L 12 883)	pressiss of Cpt No. 1 1b 2 3 4 5 6 7 8	for Hel sion A sea wate Bühlman M-valu HT min 1.51 1.88 3.02 4.72 6.99 10.21 14.48 20.53 29.11	ium Jg o rith r (msw in ZH-L es (199 Mo msw 41.0 37.2 27.2 24.3 22.4 20.8 19.4 18.2	nms ) 16A (10)					
Cpt No.	E Vilo vi-valu HT min  5	Jeen urope rkman es (19 Mo msw 26.2 22.5	Vario an Syst  1.665)  AM slope  1.5  1.4	us   Cpt   No. 1   2   3   4   5   6   7   8   9	Halda F Pres Bühlm M-val HT min 1.0 3.0 4.6 7.0 10 14 20 30 43	mian sure Un lann ZH ues (19 Mo msw 34.2 27.2 22.9 21.0 19.3 17.4 16.2 15.8	M-vali Decomi its - mete I-L m 883)  △M slope 1.2195  1.2195  1.11976 1.1834 1.1628 1.1494 1.1236 1.1236	pres rs of Cpt No. 1 1 1 5 6 7 8 9 9	for Hellsion A sea wate Bühlman M-valu HT min 1.51 1.88 3.02 4.72 4.79 10.21 14.48 20.53 29.11 41.20	ium lg o rith r (msw in ZH-L es (199 Mo msw 41.0 37.2 27.2 24.3 22.4 20.8 19.4 18.2	nms) 16A 100)  AM slope 2.3557 2.0964 1.7400 1.5321 1.3189 1.2568 1.2079 1.1692 1.1419					
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The general trend has been to become slightly more conservative. This trend reflects a more intensive validation process (empirical testing) and includes the use of Doppler ultrasound monitoring for the presence and quantity of "silent bubbles" (bubbles which are detectable in the circulation but are not associated with overt symptoms of decompression sickness).

### **CONSISTENCY OF M-VALUES**

One observation that can be made about the comparison between the M-values of the various algorithms is that there is not a great difference between them. In other words, there appears to be a certain consistency between the values determined by various independent researchers around the globe. This is a good

sign as it indicates that the science has determined a relatively consistent threshold for symptoms of decompression sickness across the human population.

#### FORMAT FOR M-VALUES

M-values are often expressed in the form of a linear equation as in the Workmanstyle or the Style-style. This format is ideal for computer programming since it allows the M-values to be calculated "on-the-fly" as they are needed. The linear format permits the display of M-value lines on the pressure graph as well.

M-values can also be expressed in the form of a matrix or table. This is simply where the M-values for each half-time compartment and each stop depth are precalculated and arranged in columns and rows. This format is useful for detailed comparisons and analysis. Some of the early dive computers and desktop computer programs used the table format to "look up" M-values for each stop during the calculation process.

#### M-VALUE CHARACTERISTICS

M-value sets can be classified into two categories, no-decompression sets and decompression sets. No-decompression M-values are surfacing values only. The DSAT RDP M-values are an example. No-stop dive profiles are designed so that the calculated gas loadings in the compartments do not exceed the surfacing M- values. This allows for direct ascent to the surface at any time during the dive. Some no-decompression algorithms account for ascent and descent rates in the calculations.

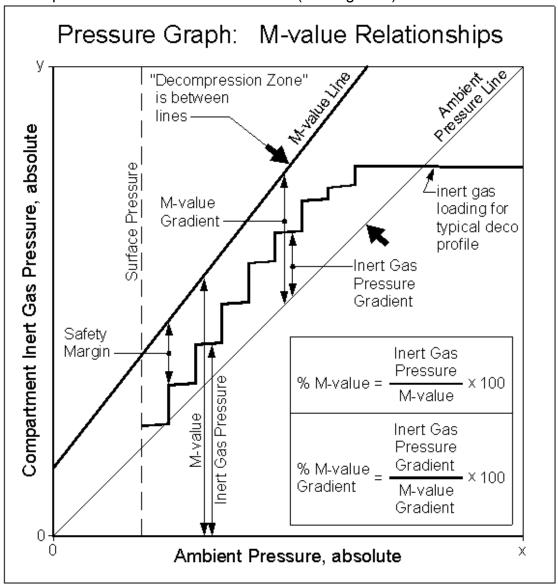
Decompression M-values are characterized by having a slope parameter which determines the change in M-value with change in ambient pressure. The value of the slope parameter will vary depending on the half-time of the hypothetical "tissue" compartment. Generally, faster half-time compartments will have a greater slope than slower half-time compartments. This reflects the observation that faster compartments tolerate greater overpressure than slower compartments. If the slope is greater than 1.0 then the M-value line "expands" on the pressure graph and that compartment will tolerate greater overpressure gradients with increasing depth. A fixed slope of 1.0 means that the compartment will tolerate the same overpressure gradient regardless of depth. In all cases, the value of the slope can never be less than 1.0. Otherwise, the M-value line would cross under the ambient pressure line at some point and this would represent an illogical situation whereby the compartment could not tolerate even the ambient pressure.

### THE AMBIENT PRESSURE LINE

The ambient pressure line is an all-important reference line on the pressure graph. Passing through the origin, it has a slope of 1.0 and simply represents the collection of points where the compartment inert gas loading will be equal to ambient pressure. This is important because when the inert gas loading in a compartment goes above the ambient pressure line, an overpressure gradient is created. An M-value line represents the established limit for tolerated overpressure gradient above the ambient pressure line.

### THE DECOMPRESSION ZONE

The "decompression zone" is the region on the pressure graph between the ambient pressure line and the M-value line (see Figure 3).



Within the context of the dissolved gas model, this zone represents the functional area in which decompression should take place. In theory, a positive gradient above ambient pressure of some magnitude is required in order for a

compartment to "off-gas" or "decompress" in an optimum manner. Depending on the fraction of oxygen in the mix, a compartment may still be able to off-gas even though the total inert gas partial pressure is less than ambient pressure. However, an "efficient" decompression profile is characterized by leading compartment gas loadings which plot within the decompression zone. The gas loadings for various half-time compartments will cross into and then out of the decompression zone during the decompression profile depending upon which compartment is "leading" or "controlling" at the time. Generally, the faster compartments will cross into the decompression zone first and be leading (gas loadings closest to M-value lines) and then the rest of the decompression profile will be controlled by the slower compartments in sequence.

### **MULTIPLE INERT GASES**

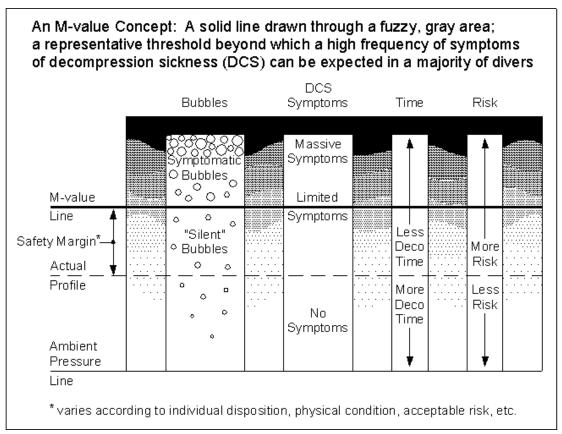
Present-day dissolved gas models employ a concept for multiple inert gases which states that the total inert gas pressure in a hypothetical "tissue" compartment is the sum of the partial pressures of the inert gases present in the compartment, even though the various inert gases each have a different half-time for that compartment.

Mixed gas decompression algorithms must deal with more than one inert gas in the breathing mix, such as helium and nitrogen in trimix. M-values for this situation are handled differently by the various algorithms. Some methodologies use the same M-values for both nitrogen and helium; usually they are based on the M-values for nitrogen. In the Style algorithm, an intermediate M-value is calculated which is an adjustment between the separate M-values for nitrogen and helium based on the proportion of these inert gases present in the compartment. In the M-value linear equation, the Coefficient a (He+N2) and the Coefficient b (He+N2) are computed in accordance with the partial pressures of helium (PHe) and nitrogen (PN2) as follows:

```
a (He+N2) = [a (He) PHe + a (N2)*PN2] / [PHe + PN2];
b (He+N2) = [b (He) PHe + b (N2)*PN2] / [PHe + PN2].
```

### WHAT DO M-VALUES REPRESENT?

A misconception among some divers is that M-values represent a hard line between "getting the bends" and "not getting the bends." This might explain why some divers routinely push the limits of their tables or dive computer. The experience of diving medicine has shown that the established limits (M- values) are sometimes inadequate. The degree of inadequacy is seen to vary with the individual and the situation. Accordingly, it may be more appropriate to describe an M-value as "a solid line drawn through a fuzzy, gray area" (see Figure 2).



The reasons for this lack of definitude involve complex human physiology, variations among individuals, and predisposing factors for decompression sickness.

Overall, the dissolved gas model has worked well for divers and the knowledge base has continued to grow. For example, it was originally presumed that all inert gas had to remain dissolved in solution and that any bubbles were indicative of DCS. However, we now know that silent bubbles are present even during symptom-free dives. Thus, the reality is that there is a combination of two conditions during a dive most of the inert gas presumably in solution and some of the inert gas out of solution as bubbles. An M-value, therefore, represents not only a tolerable overpressure gradient, but a tolerable amount of bubbles as well.

M-values are empirically verified, meaning that actual decompression trials are carried out with human subjects. These tests are conducted with a relatively small number of subjects intended to represent the much larger population of divers. Even though good data is obtained about the approximate threshold for symptoms of decompression sickness (M-values), this process cannot accurately predict or guarantee an absolute threshold for everyone. Also, we know from experience that certain factors are predisposing for decompression sickness: lack of physical conditioning, fattiness, fatigue, drugs/alcohol, dehydration, over-exertion, very cold water, open patent foramen ovale (PFO), etc. Individual susceptibility can vary on a daily basis as well.

### M-VALUES AND CONSERVATISM

Limited symptoms, if any, and a reasonably low level of risk are associated with M-values. This criteria, however, may not be entirely acceptable to all divers. Many divers would like to be in the range of "no symptoms" and "very low level of risk" when it comes to their decompression profiles.

Fortunately, it is well understood among decompression modelers and programmers that calculations based on the established M-values alone cannot produce sufficiently reliable decompression tables for all individuals and all scenarios. This is why decompression programs provide for a means of introducing conservatism into the calculations.

Some of the methodologies include increasing the inert gas fractions used in the calculations, applying a depth safety factor which calculates for a deeper-than-actual dive depth, calculating for a longer-than-actual bottom time, and adjusting the half-times to be asymmetrical during off-gassing (slower). Some programs use more than one of these methods combined. These methodologies for conservatism are effective when properly applied. The degree of "effectiveness" is usually gauged by divers in terms of how much longer and deeper the decompression profiles become, and through individual experience with the outcome of the profiles.

#### M-VALUE RELATIONSHIPS

Some fundamental relationships involving M-values and decompression calculations are indicated on the pressure graph in Figure 3. The Percent M-value calculation has been used by various decompression modelers over the years. Professor Style, for example, evaluated many of his decompression trials on a Percent M-value basis and reported the data as such in his book(s)

The Percent M-value Gradient calculation is a measure of how far a decompression profile has entered into the decompression zone. 0% M-value Gradient is at the ambient pressure line and represents the bottom of the decompression zone. 100% M-value Gradient is at the M-value line and represents the top of the decompression zone.

### ANALYSIS OF PROFILES

Many divers would like to know precisely what the effect is of the conservatism factors in their desktop decompression program(s). They realize that longer and deeper profiles are generated with increasing conservatism factors, but more fundamental information is desired.

Both the Percent M-value and Percent M-value Gradient relationships are useful for the analysis and evaluation of decompression profiles. Using a standard set of reference M-values, different profiles can be evaluated on a consistent basis. This includes comparison of profiles generated by entirely different programs, algorithms, and decompression models.

#### UNIVERSAL REFERENCE VALUES

The Style ZH-L16 M-values are employed in most, if not all, of the desktop decompression programs in use by technical divers. These M-values were developed and tested for a broad range of ambient pressure exposures; from high altitude diving to deep sea diving. When used with appropriate conservatism, they have proven to be "reliable" for technical diving (to the extent that something can be reliable in an inexact science). They have become the de facto world-wide standard that can serve as universal reference values for the comparison and evaluation of decompression profiles.

It is a relatively easy task for programmers to include Percent M-value and Percent M-value Gradient calculations in summary form with the decompression profiles.

Table	Table 5: Effect of Conservatism Factors in a Commercially-Available Program on Decompression Profiles Referenced to Bühlmann ZH-L16 M-values (ZH-L16A Helium, ZH-L16B Nitrogen)											
		Referenced	l to Bühlma	nn ZH	L16 M	-values (ZH	FL16A Heliu	ım, ZH	-L16B	Nitrogen)		
	15/40	Trimix Dive (1	5% O <sub>2</sub> / 40% F	te) to 250	Ofsw for:	30 min. Deco	mixes - Nitrox 3	36% at 1	10 fsw, 10	00% O <sub>2</sub> at 20 fs	3W	
(	0% Cor	ıservatism F	actor	50% Conservatism Factor					100% Conservatism Factor			
			Maximum *				Maximum *				Maximum *	
Deco	Run	Maximum *	% M-value	Deco	Run	Maximum *	% M-value	Deco	Run	Maximum *	% M-value	
Stop	Time	% M-value	Gradient	Stop	Time	% M-value	Gradient	Stop	Time	% M-value	Gradient	
(fsw)	(min)	(Cpt No.)	(Cpt No.)	(fsw)	(min)	(Cpt No.)	(Cpt No.)	(fsw)	(min)	(Cpt No.)	(Cpt No.)	
								140	35	74.3% (4)	29.3% (3)	
								130	37	76.0% (4)	31.0% (3)	
				120	35	81.6% (4)	47.0% (3)	120	40	77.4% (4)	33.9% (4)	
110	36	85.8% (4)	59.4% (4)	110	38	84.5% (4)	55.7% (4)	110	43	77.6% (4)	35.5% (4)	
				100	39	79.0% (5)	39.4% (4)	100	45	75.4% (5)	22.6% (4)	
90	38	89.0% (4)	69.3% (4)	90	41	82.1% (5)	46.0% (4)	90	49	76.5% (6)	26.3% (5)	
80	41	89.5% (5)	69.1% (4)	80	45	83.2% (5)	49.1% (5)	80	53	76.3% (6)	20.3% (5)	
70	44	88.3% (5)	65.6% (5)	70	49	82.2% (6)	42.5% (5)	70	58	77.0% (6)	22.1% (6)	
60	48	89.8% (6)	67.2% (6)	60	55	83.2% (6)	45.1% (6)	60	68	78.2% (7)	24.9% (6)	
50	55	91.1% (6)	72.2% (6)	50	64	83.1% (7)	44.1% (6)	50	78	76.9% (7)	17.6% (7)	
40	64	90.3% (7)	67.7% (7)	40	75	83.1% (7)	42.8% (7)	40	96	78.4% (8)	22.5% (7)	
30	79	90.7% (7)	70.7% (7)	30	95	84.5% (8)	46.0% (7)	30	124	78.3% (8)	22.4% (8)	
20	94	90.9% (8)	70.7% (8)	20	113	84.2% (9)	47.1% (8)	20	147	78.9% (9)	24.4% (9)	
10	119	91.1% (9)	72.2% (9)	10	144	85.8% (10)	51.7% (10)	10	189	81.2% (11)	32.6% (10)	
0	120	93.6% (11)	80.2% (11)	0	145	88.6% (12)	62.6% (12)	0	190	84.9% (13)	46.6% (13)	
* Upon	Arrival at	t the Stop										

Table 5 is an example of this and shows the effect of conservatism factors used in a commercially-available desktop decompression program.

At 0% Conservatism Factor, the decompression profile is in the 90% M-value range and has entered approximately 70% into the decompression zone (70% M-value Gradient). It is evident that this program employs a level of baseline conservatism since none of the values reaches 100%. At 50% Conservatism Factor (which is recommended in the user's manual), the profile is in the 85% M-value range and has entered approximately 40-50% into the decompression

zone. At 100% Conservatism Factor, the profile is in the 77% M-value range and has entered approximately 20-35% into the decompression zone. Note that the values given in Table 5 are upon arrival the respective stops which is the worst-case condition. This correlates with the edges of the "stair-steps" in the gas loading profile on the pressure graph (see example in Figure 3). The highest values across all profiles are calculated upon arrival at the surface which illustrates why a very slow final ascent from the last decompression stop to the surface is always prudent.

### **MARGIN OF SAFETY**

Using the M-value relationships and a standard set of reference M-values, divers can determine personal decompression limits which are both well-defined and transportable. The margin of safety selected will depend on individual disposition and prior experience with profiles. An honest assessment of one's fitness for decompression diving is always in order. For example, this author/diver (an office worker) has chosen a personal limit of 85% M-value and 50-60% M-value Gradient for typical trimix dives. To ensure a fixed margin of safety, a decompression profile can be calculated directly to a predetermined percentage of the M-value Gradient. The advantage of this approach is complete consistency across the entire ambient pressure range and precise control over the resultant profile.

### **About the Author**

Erik C. Baker is an electrical engineer with an architecture/engineering firm in Pennsylvania. He pursues research into decompression and diving physiology as a hobby, and has developed several FORTRAN computer programs for decompression calculation and analysis. Erik is a certified cave diver and trimix diver.

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# 8.2 Deep Stops Explained : Erik C Baker

The old adage, "an ounce of prevention is worth a pound of cure," is certainly applicable to the various symptoms of decompression sickness (DCS). The best treatment of all for these maladies is to complete a sufficient decompression profile in the first place. Technical divers have observed that many ailments can be avoided by including "deep stops" in their profiles. A closer examination of the decompression model reveals that this practice serves to reduce or eliminate excessive overpressure gradients. Knowing this, the model can be modified to provide precise control of gradients and stops can be calculated within the decompression zone to the depth of the "deepest possible decompression stop."

Note: For further explanation of the decompression concepts and terminology discussed herein, readers are referred to a previous article by the author, "Understanding M-values," Immersed, Vol. 3, No. 3, Fall 1998.

Many technical divers have observed that they feel fatigue, malaise, or drowsiness after completing certain types of decompression dives. The "bounce dive," which is characterized as being relatively deep with a short bottom time, often produces such symptoms. Conventional implementation of the dissolved gas decompression model for this kind of dive will generate a first stop in the decompression profile that is much shallower than the bottom depth. Several divers have reported that if they add some "deep stops" in their profiles, i.e., deeper than what the conventional calculation calls for, then post-dive symptoms are dramatically reduced or eliminated. Issues of confusion and controversy among technical divers are the questions of how deep these "deep stops" should be and how many such stops should be performed.

The empirical observations of divers have led to the development of arbitrary methods for introducing deep stops. Many of these methods involve individual judgement and discretion rather than having a basis in the decompression calculations. Analysis of complete decompression profiles that utilize arbitrary deep stops reveals that there are potential problems. These include stops that are made too deep and inadequate extension of decompression time at the shallow stops to compensate for the increased gas loading caused by the deep stops.

### **CONVENTIONAL CALCULATION**

In decompression application and theory, there is a trade-off between sufficient decompression (no symptoms of DCS) and economic decompression (minimum amount of time, gas supplies, exposure, etc.). Conventional dissolved gas algorithms, such as those developed by Robert D. Workman and Albert A. Bühlmann, seek to optimize the decompression by allowing the diver to ascend

to the shallowest depth or "ceiling" based on the ascent limiting M-values for the hypothetical "tissue" compartments. The economics of this are two-fold: inert gas elimination in the faster compartments is accelerated while inert gas uptake in the slower compartments is minimized during decompression. In practice, divers have traditionally been instructed to "get off the bottom" and ascend to the first stop in a timely manner.

For a typical bounce dive, the conventional calculation will permit a relatively long ascent from the bottom to the first stop. In this scenario, the inert gas loadings in the fastest compartments can be at or near saturation at the bottom depth while the slowest compartments are only partially loaded. This means that the fastest compartments will control the initial ascent since their inert gas loadings will be closer to M-values well before the slower compartments. The first stop is determined when the inert gas loading in the leading compartment is equal to or near its M-value.

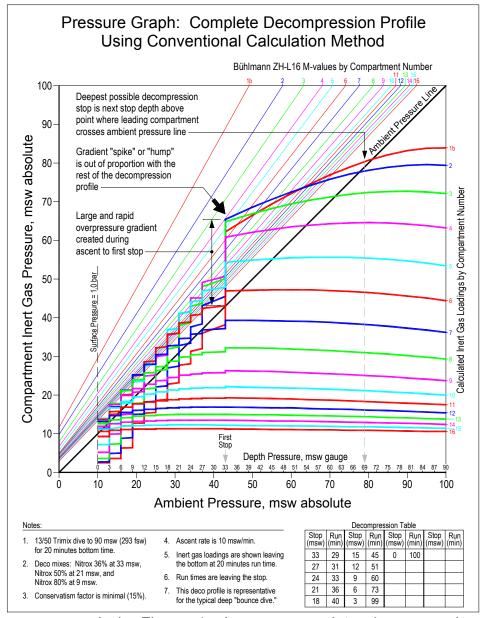
### **BUBBLES AND GRADIENTS**

When the concept of M-values was first presented in 1965 by decompression researcher Robert D. Workman, an assumption was made that inert gas would not come out of solution as bubbles in a diver's tissues until an M-value was exceeded. This theory was somewhat controversial at the time, however it was recognized that future technology would be able to give better information about the presence and behavior of bubbles in diver's bodies. Workman acknowledged that "ultrasonic methods of bubble detection in vivo and in vitro are being explored to permit better definition of decompression adequacy, but this is still in its early stages."

Since then, Doppler ultrasound technology was developed and it has been used extensively in decompression research around the world. This research has shown that bubbles are present in the body's circulation during and after many kinds of dives, including those with no symptoms of DCS. In other words, a diver does not have to exceed an M-value in order to generate bubbles. This fact has been acknowledged in decompression science, but the mechanisms for bubble formation and growth in the human body are neither well understood nor precisely defined.

The laws of physics and many bubble models predict that greater numbers and sizes of bubbles can be expected with increasing overpressure gradients. In the dissolved gas model, this means that more bubbling can be expected as the compartment inert gas loadings plot farther above the ambient pressure line on the pressure graph.

### ILLUSTRATING THE PROBLEM



The pressure graph in Figure 1 shows a complete decompression profile calculated by the conventional method. In this profile, the fastest compartments have the greatest gas loadings during the initial ascent and are leading. The M-values for these fast compartments permit large overpressure gradients relative to the slower compartments. Consequently, a large and rapid overpressure gradient is created during the ascent to the first stop. This is out of proportion with the smaller overpressure gradients permitted during the rest of the decompression profile when slower compartments are controlling. Presumably, many bubbles could be generated during the initial ascent to the first stop. In this case, the calculated gradient is 22.4 meters of seawater (msw) ÷ 73 feet of seawater (fsw) ÷ 2.2 atmospheres. For comparison, when a can of soda is

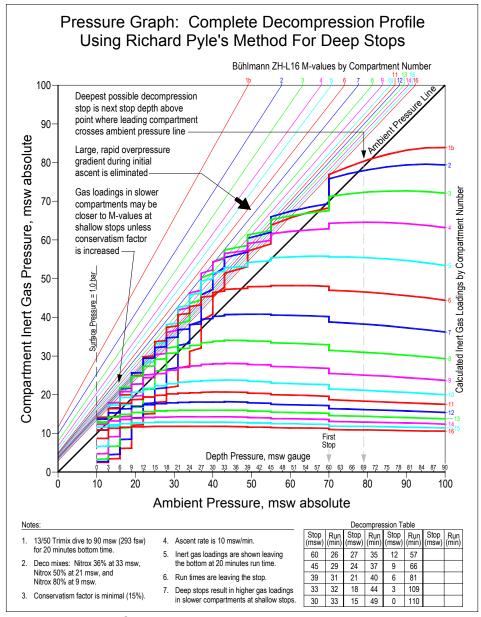
opened, the pressure gradient between the dissolved carbon dioxide and the air is in the range of 3.1 to 3.4 atmospheres.

Although an M-value is not exceeded in the decompression profile of Figure 1, a diver could experience symptoms of fatigue, malaise, or drowsiness after this dive. Explanations for this include theories of bubble migration within the body and delayed off-gassing caused by accumulation of bubbles in the pulmonary capillaries. In any case, it is possible to associate a cause and effect relationship between large overpressure gradients during the dive and post-dive symptoms. Mild or vague symptoms such as fatigue and malaise, which normally do not receive medical treatment, may fall within a category of decompression stress, a lesser variant of DCS.

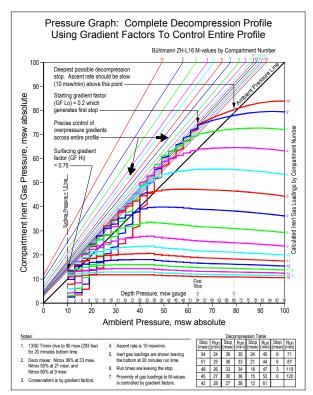
### SOLUTIONS TO THE PROBLEM

Large and/or rapid overpressure gradients in a decompression profile presumably create more bubbling which leads to decompression stress or DCS. The obvious solution to this problem is to limit the magnitude of overpressure gradients. Information within the dissolved gas decompression model can be used to address the issue.

First, there is a limit to how deep a "deep stop" can be. The leading compartment inert gas loading associated with a "decompression stop" should not be below the decompression zone. In general, an overpressure gradient of some magnitude is required for efficient off- gassing. It is also important to minimize the extent of on-gassing in the slower compartments during the decompression.



Within the context of the dissolved gas model, the "deepest possible decompression stop" for a given profile can be defined as the next standard stop depth above the point where the gas loading for the leading compartment crosses the ambient pressure line (see Figures 1 thru 3). The deepest possible stop depth is easily calculated in a decompression program and it will vary depending on the ascent rate from the bottom and the gas mix being used.

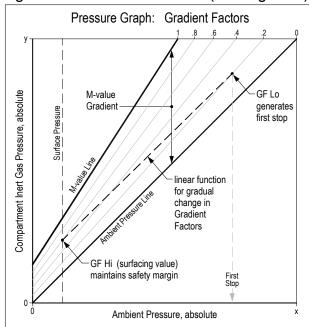


A decompression profile does not necessarily need to have a first stop at the deepest possible stop depth. This depth simply represents the point where at least one compartment will be in the decompression zone. For many decompression profiles, stops that start a few standard stop depths above the deepest possible stop should be adequate to control excessive overpressure gradients. However, the deepest possible stop depth is valuable information for the diver as it represents the beginning of the decompression zone. When reaching this point during the ascent from the bottom, the diver should slow the ascent to the decompression zone rate of 10 msw/min (30 fsw/min) or less. This practice will help to reduce rapid changes in overpressure gradients which presumably promote bubbling.

Next, there is the issue of introducing deep stops. One empirically-derived method for deep stops was published by diver and marine biologist Richard L. Pyle. It is used in conjunction with a desktop decompression program with multilevel capabilities. A complete decompression profile using Richard Pyle's method for deep stops is shown on the pressure graph in Figure 2. The graph indicates that this method is effective in reducing or eliminating excessive overpressure gradients when compared to the conventionally calculated profile. There are, however, potential difficulties with this approach. Depending on the decompression program being used and its method for conservatism, the gas loadings in the slower compartments may be closer to the M-values at the shallow stops due to the increased uptake caused by the deep stops. The program will compensate for the deep stops, but unless the conservatism factor is increased, it may not provide the same margin of safety at the shallow stops as when running a conventional profile. A good way to evaluate this is to calculate

the maximum Percent M-values and Percent M-Value Gradients across all compartments at each stop.

The pressure graph in Figure 3 shows a complete decompression profile calculated using Gradient Factors to control the overpressure gradients across the entire profile. Gradient Factors provide a consistent approach to conservatism in decompression calculations. They can be used to generate deep stops within the decompression zone, control overpressure gradients, and ensure a fixed margin of safety from the M-values across the entire decompression profile. A Gradient Factor is simply a decimal fraction or percentage of the M-value Gradient (see Figure 4).



A Gradient Factor is simply a decimal fraction (or percentage) of the M-value Gradient.

Gradient Factors (GF) are defined between zero and one,  $0 \le GF \le 1$ .

A Gradient Factor of 0 represents the ambient pressure line.

A Gradient Factor of 1 represents the M-value line.

Gradient Factors modify the original M-value equations for conservatism within the decompression zone.

The lower Gradient Factor value (GF Lo) determines the depth of the first stop. Used to generate deep stops to the depth of the "deepest possible deco stop."

M-value equations modified for use with Gradient Factors (GF)

#### Workman Equations:

$$M = Depth \cdot (\Delta M \cdot GF - GF + 1) + GF \cdot M_0$$

Tol. Depth = 
$$(M - GF \cdot M_{\circ}) / (\Delta M \cdot GF - GF + 1)$$

Bühlmann Equations:

$$P_{t.tol}$$
i.g. =  $P_{amb}$ • (GF/b - GF + 1) + GF•a

$$P_{amb,tol.} = (P_t i.g. - GF \cdot a) / (GF/b - GF + 1)$$

Gradient Factors can be applied manually for each stop or they can be applied in an automated mode. A simple linear function will permit a gradual change in the Gradient Factor from the GF Lo value to the GF Hi value:

$$\mathsf{GF} \ \mathsf{slope} = \frac{\mathsf{GF} \ \mathsf{Hi} \ \mathsf{-} \ \mathsf{GF} \ \mathsf{Lo}}{\mathsf{Final} \ \mathsf{Stop} \ \mathsf{Depth} \ \mathsf{-} \ \mathsf{First} \ \mathsf{Stop} \ \mathsf{Depth}}$$

GF = GF slope • Current Stop Depth + GF Hi

#### Advantages of Gradient Factor Method for Conservatism

- Can be used to generate deep stops to the depth of the "deepest possible decompression stop"
- . Decompression stops, including deep stops, will always be within the decompression zone
- · Permits precise control of overpressure gradients including a gradual change in gradients from first stop to the surface
- Minor modification to the familiar Haldanian decompression model easy to understand and apply
- Flexible Gradient Factors can be applied to deal with individual physiology as well as various types of dive profiles

## **ADDENDUM**

Eric Baker recently discovered that the above diagram has a small mistake in the modified Workman equation. The Workman-style M-value equations are a function of depth pressure (not ambient pressure as in the Style-style). As such everything is "shifted" on the pressure graph by the value of the surface barometric pressure.

The incorrect modified Workman Equations are shown as:

$$M = Depth^*(DM^*GF - GF + 1) + GF^*Mo$$

The correct modified Workman Equations for use with Gradient Factors are as follows:

$$M = Depth^*(DM^*GF - GF + 1) + (Psb + GF^*(Mo - Psb))$$

Tol. Depth = 
$$[P - (Psb + GF*(Mo - Psb))]/(DM*GF - GF + 1)$$

where P = compartment inert gas pressure, absolute

Psb = surface barometric pressure, absolute

### **END ADDENDUM**

The addition of deep stops in a profile will generally increase the time required at the shallow stops as well as the overall decompression time. However, if truly "sufficient decompression" is the result, then the concept of "economic decompression" is not really compromised.

The pressure graph is an excellent tool for divers to evaluate decompression profiles. Even a quick review can identify potential problem areas such as large overpressure gradients. Decompression modelers and programmers are encouraged to include this feature in their programs.

Finally, the example decompression profiles used for the pressure graphs in this article were calculated with minimal conservatism and are intended for comparison purposes only.

Erik C. Baker is an electrical engineer with an architecture/engineering firm in Pennsylvania who has developed several computer programs to improve the safety of his cave and trimix diving.

#### References:

Baker EC. 1998. Understanding M-values. Immersed. Vol. 3, No. 3.

Bennett PB, Elliott DH, eds. 1993. The Physiology and Medicine of Diving. London: WB Saunders.

Bühlmann, AA. 1984. Decompression-Decompression Sickness. Berlin: Springer-Verlag.

Bühlmann, AA. 1995. Tauchmedizin. Berlin: Springer-Verlag.

Hamilton RW, Rogers RE, Powell MR, Vann RD. 1994. Development and validation of no-stop decompression procedures for recreational diving: The DSAT Recreational Dive Planner. Santa Ana, CA: Diving Science and Technology Corp.

Pyle RL. 1996. The importance of deep safety stops: Rethinking ascent patterns from decompression dives. DeepTech. 5:64; Cave Diving Group Newsletter. 121:2-5.

Schreiner HR. 1968. Safe ascent after deep dives. Rev. Subaquat. Physiol. Hyperbar. Med. 1:28-37.

Schreiner HR, Kelley PL. 1971. A pragmatic view of decompression. In: Lambertsen CJ, ed. Underwater Physiology IV. New York: Academic Press.

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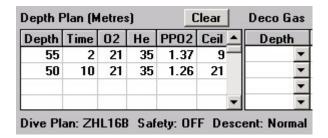
Workman RD. 1965. Calculation of decompression schedules for nitrogenoxygen and helium-oxygen dives. Research Report 6-65. Washington: Navy Experimental Diving Unit.

# 9 Operational Issues and User Workarounds

# 9.1 Deep short dives with non immediate descents

When <u>modelling descents</u> on deep short dives it is possible that the descent will take longer than the segment time. In the current version of Deco Planner, it is left to the user to ensure that the first entered depth/time segment is longer than the descent time, this can be confirmed by viewing the analysis sheet

In the example below a diver has planned a 2 min dive to 55m, the descent rate was set to 20m / min.



In the analysis sheet we see that the first segment the descent has a calculated time of 2.8 minutes (red box) and the second segment at 55m has a time of MINUS 0.8 minutes (green box)

			Cpt 1
SEG: 1	DESC	PHe	9.3
START DEPTH	0	PN2	10.6
FINAL DEPTH	55	PHe+PN2	19.9
RATE	20	%Ambient	30.5
SEG TIME	2.8	He Grad	13.3
RUN TIME	2.8	N2 Grad	17.8
MIX 02	21%	M-Value	139.0
MIX He	35%	%M-Value	14.3
		%M-V Grad	-61.3
SEG: 2	STOP	PHe	5.0
CONST DEPTH	55	PN2	8.6
PN2 ATA	1.35	PHe+PN2	13.7
SEG TIME	8	%Ambient	21.0
RUN TIME	2.0	He Grad	17.6
MIX 02	21%	N2 Grad	19.8
E315.7.1.1	25%	M W-1	120.7

The current workaround is to either turn on immediate descent, or to increase the entered time "at" 55m to include the descent time.

### 9.2 Multi level dives with immediate descent turned on

When planning multi level dives with the options set to immediate descent, only the first descent is completed immediately, all other descents are modelled using the descent rate entered in the <u>Dive Plan Preferences</u>.

This can be seen in the example analysis sheet below, the descent from surface to 36m (the green box) shows the descent being immediate. However the 36m to 55m descent (the blue box), is not immediate as the calculated segment time (of 1.3 mins) has been added to the run time.

Mission: 1 Dive			). n	
			Cpt 1	Cpt 2
SEG: 1	DESC	PHe	.0	.0
START DEPTH	0	PN2	7.6	7.6
FINAL DEPTH	30	PHe+PN2	7.6	7.6
RATE	20	%Ambient	18.8	18.8
CEC TIME	1.5	He Grad	13.8	13.8
RUN TIME	.0	N2 Grad	9.9	9.9
MIA UZ	21%	M-Value	83.6	71.6
MIX He	35%	%M-Value	9.0	10.6
		%M-V Grad	-74.9	-103.5
SEG: 2	STOP	PHe	13.5	12.5
CONST DEPTH	30	PN2	14.9	13.3
PO2 ATA	.83	PHe+PN2	28.4	25.7
SEG TIME	10.0	%Ambient	70.9	64.1
RUN TIME	10.0	He Grad	.3	1.4
MIX 02	21%	N2 Grad	2.5	4.1
MIX He	35%	M-Value	91.1	77.2
MIX He		%M-Value	31.2	33.3
		%M-V Grad	-22.9	-38.9
SEG: 3	DESC	PHe	15.4	13.9
START DEPTH	30	PN2	16.2	14.3
FINAL DEPTH	55	PHe+PN2	31.6	28.2
DATE	20	%Ambient	48.5	43.3
SEG TIME	1.3	He Grad	7.2	8.7
RUN TIME	11.3	N2 Grad	12.2	14.1
MIA UZ	4140	M-Value	139.5	118.1
MIX He	35%	%M-Value	22.7	23.9
		%M.V Grad	.45.1	.69.6

The current workaround for those divers not modelling the descents is to set the descent rate to the maximum allowed which is 100m/min.

# 9.3 Narcotic properties of Oxygen

The <u>dive tool calculator</u> assumes oxygen is **NOT** narcotic in its narcotic calculations. If the mix contains no helium, an equivalent air depth is calculated. If the mix does contain helium, an Equivalent Narcosis depth is calculated. There is no current workaround available in Deco Planner

# 9.4 Gas Calculations when working in Imperial

Currently a user can enter personal SAC rates, cylinder sizes and working pressures. However when working in imperial all that is calculated is the free cubic footage of the gas required to complete the dive, this is based purely on SAC rate, depth and times. The intent is to enhance this feature in a future release of Deco Planner.

# 9.5 Surface pressure setting

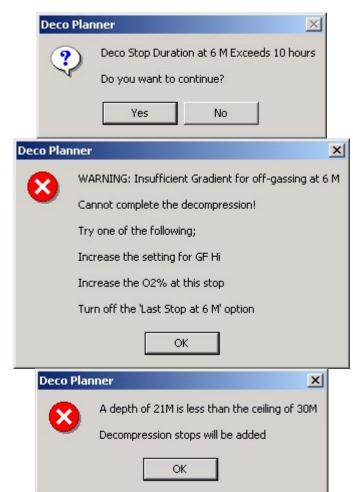
The default for a new install of Deco Planner for surface pressure is 1013.25 mb, as this is the standard setting for surface pressure. If this is changed, the user cannot enter a decimal point and therefore cannot reset the surface pressure parameter back to 1013.25. The closest setting that can be entered is 1013 mb.

# 10 Warnings and Errors

This warning is in order to prevent calculations tying up the PC, in the event of the user entering wrong or no decompression gas

This warning will appear if Deco Planner detects that due to in correct parameter choices by the user, the user is about to plan a dive from which it is impossible to dive

This warning occurs when a user enters a depth / time segment which is shallower that the calculated ceiling. See Modifying gas switches / decompression times



# 11 Support Material

## 11.1 Suggested Reading List

Bennett PB, Elliott DH, eds. 1993. The Physiology and Medicine of Diving. London: WB Saunders.

Bühlmann, AA. 1984. Decompression-Decompression Sickness. Berlin: Springer-Verlag.

Bühlmann, AA. 1995. Tauchmedizin. Berlin: Springer-Verlag.

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Wienke BR. 1994. Basic diving physics and applications. Flagstaff, AZ: Best.

Workman RD. 1965. Calculation of decompression schedules for nitrogenoxygen and helium-oxygen dives. Research Report 6-65. Washington: Navy Experimental Diving Unit.

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# 11.2 Units Of Diving

### From an original document written by Erik C. Baker

The units used to describe depth in diving should be in units of PRESSURE and not units of LENGTH. This is a common source of confusion and misunderstanding and the conversion between these units is often done incorrectly.

Two systems have evolved in diving regarding pressure units - the system of American usage and the system of European usage. Neither system is particularly "correct" and neither system conforms entirely to SI standards of usage.

In both systems, the pressure units for depth are defined ARBITRARILY and INDEPENDENTLY:

The American usage unit of depth (pressure) is feet of seawater (fsw) and is DEFINED as,

1 fsw = 1/33 standard atmosphere = 3.0705 kPa = 3.0705 x  $10^3$  Pascals (N/m<sup>2</sup>)

This unit conforms to a specific gravity for sea water of 1.020.

The European usage unit of depth (pressure) is the meter of seawater (msw) and is DEFINED as,

1 msw = 1/10 bar = 10 kPa =  $10^4$  Pascals (N/m<sup>2</sup>)

This conforms to a specific gravity for sea water of 1.027.

Note that the units fsw and msw LOOK LIKE units of LENGTH but they are NOT!

The conversion between these PRESSURE UNITS is 3.2568 fsw/msw and 0.30705 msw/fsw.

The conversion between the linear units of LENGTH is 3.2808 feet/meter and 0.3048 meters/foot. These conversion factors are often INCORRECTLY applied to convert between fsw and msw.

Sea water ranges in specific gravity between about 1.020 and 1.030. Thus, both the American and European units were chosen to stay within these limits. The density of the water (or the depth for that matter) does not matter if the PRESSURE of the diver is measured and used to determine the proper

decompression. Thus a dive in fresh water involves no adjustment as long as the diver's PRESSURE is measured with the same gauge calibration as is used for the decompression calculations.

Some important notes about USAGE CONVENTIONS need to be mentioned:

- 1. In the American system, sea level is considered to be at STANDARD ATMOSPHERIC PRESSURE = 101.325 kPa = 1.01325 bar = 760 mm Hg.
- 2. Some users of the American system, including the U.S. Navy and the Journal of Undersea and Hyperbaric Medicine, deviate from the standard definition of fsw and define 1 fsw = 1/33.08 standard atmosphere. However, most users of the American system define 1 fsw = 1/33 standard atmosphere or 33 fsw = 1 atm.
- 3. In the European system, sea level is considered to be 1.0 bar. The standard atmosphere, however, is 1.01325 bar. This means that the European system differs from the American system by 13.25 mb or 1.3%.

The daily fluctuations in barometric pressure will most likely outweigh the trivial differences between the American system and the European system.

Another point worth mentioning is that neither the American unit, fsw, nor the European unit, bar, conform to SI standard usage. Technically, divers should all be using the SI unit of pressure, the Pascal. However, the common practices of usage are so entrenched that this is unlikely to change.

PROPER CONVERSION OF FEET OF SEAWATER (FSW) TO METERS OF SEAWATER (MSW)

Prepared by Erik C. Baker

References: ANSI/IEEE Std. 268-1992, ASTM E380-91a, R.W. Bill Hamilton

### **DEFINITIONS**

- 1. One MSW is DEFINED as 1/10 bar
- 2. One FSW is DEFINED as 1/33 atm

Note: FSW and MSW are units of PRESSURE and NOT length!

SI CONVERSIONS

SI unit of pressure is the pascal (Pa) = Newtons per square meter

1 bar = 100 kPa

1 atm = 1.013250E+05 Pa (Atmosphere, standard)

1 atm = 1.01325 bar

# **CONVERSION OF UNITS**

(1 atm (33 FSW) 1 MSW = (0.1 bar) \* ------ \* ----- = 3.25684678 FSW (1.01325 bar (1 atm)

FSW	MSW	FSW	MSW	FSW	MSW
5	1.5	205	62.9	405	124.4
10	3.1	210	64.5	410	125.9
15	4.6	215	66.0	415	127.4
20	6.1	220	67.6	420	129.0
25	7.7	225	69.1	425	130.5
30	9.2	230	70.6	430	132.0
35	10.7	235	72.2	435	133.6
40	12.3	240	73.7	440	135.1
45	13.8	245	75.2	445	136.6
50	15.4	250	76.8	450	138.2
55	16.9	255	78.3	455	139.7
60	18.4	260	79.8	460	141.2
65	20.0	265	81.4	465	142.8
70	21.5	270	82.9	470	144.3
75	23.0	275	84.4	475	145.8
80	24.6	280	86.0	480	147.4
85	26.1	285	87.5	485	148.9
90	27.6	290	89.0	490	150.5
95	29.2	295	90.6	495	152.0
100	30.7	300	92.1	500	153.5
105	32.2	305	93.6	505	155.1
110	33.8	310	95.2	510	156.6
115	35.3	315	96.7	515	158.1
120	36.8	320	98.3	520	159.7
125	38.4	325	99.8	525	161.2
130	39.9	330	101.3	530	162.7
135	41.5	335	102.9	535	164.3
140	43.0	340	104.4	540	165.8
145	44.5	345	105.9	545	167.3
150	46.1	350	107.5	550	168.9
155	47.6	355	109.0	555	170.4
160	49.1	360	110.5	560	171.9
165	50.7	365	112.1	565	173.5
170	52.2	370	113.6	570	175.0
175	53.7	375	115.1	575	176.6
180	55.3	380	116.7	580	178.1

185	56.8	385	118.2	585	179.6
190	58.3	390	119.7	590	181.2
195	59.9	395	121.3	595	182.7
200	61.4	400	122.8	600	184.2