

AN018**CC1000 Debugging Hints and Troubleshooting****By S. Hellan**

Keywords

- *CC1000*
- *Calibration*
- *VCO tuning*
- *VCO tuning range*
- *RF Link*
- *Locking averaging filter*
- *Procedure for detecting packets in receive mode*
- *Testing and verifying transceiver designs*

Introduction

CC1000 and the corresponding CC1000 Development Kit makes it very easy to evaluate the performance of the CC1000 chip, and in a short time, designers can develop their own RF modules based on this reference design. The SmartRF Studio software package provides the flexibility needed to automatically generate configuration data used by the microcontroller.

This application note gives some general debugging and troubleshooting hints for CC1000. Procedures for detecting packets in receive mode are also included.

This application note is just a quick reference guide to the most common pitfalls. It is by no means a substitute for the data sheet and the more in-depth application notes found on our web site. There is also a FAQ data base on our web site.

The application note also includes a step-by-step testing procedure.

Chipcon is a supplier of RFICs for all kinds of short-range communication devices. Chipcon has a worldwide distribution network.

Hints

1) Always perform calibration

CC1000 must be in LOCK both in Rx and Tx. Read back contents of register LOCK[0] after calibration or monitor the CHP_OUT (LOCK) pin. Remember to set the LOCK_SELECT[3:0] to '0001' in the latter case.

The calibration values are stored separately for each frequency register when single calibration is used. Therefore, in a single-channel application, it is sufficient to calibrate once in Rx and once in Tx when the system is powered up. Once this is done, the system can change between Rx and Tx by writing to the MAIN and CURRENT registers, and no recalibration needs to be performed unless one of the recalibration requirements stated in the data sheet occur.

If you use the CC1000 Development Kit and SmartRF Studio press 'Reset', 'Update', and finally 'Calibrate' in the SmartRF Studio *Normal View* to perform calibration.

2) Calibration: ALARM_L and ALARM_H

The correct VCO capacitor array ("digital" varactor) is found during calibration. The charge pump current is adjusted to give the correct loop filter bandwidth.

If the VCO is not able to tune to the correct frequency, the tuning voltage will end up at 0 V or at VCC (3 V). This will be indicated by ALARM_L (too close to ground) or ALARM_H (too close to the VCC). Note that the PLL can, in some cases, lock to the desired frequency even if the ALARM bit is set.

If the ALARM bit is set there could be several causes: The crystal or its programming is wrong, the frequency programming is wrong, or the VCO inductor is wrong.

3) VCO tuning range

CC1000EB-434 should cover the frequency range from approximately 433 MHz $\pm 10\%$. CC1000EB-868 should cover the frequency range from approximately 868 MHz $\pm 12.5\%$. If you have made your own PCB layout the VCO tuning range might be changed. Check the VCO tuning range as follows:

Set the frequency to a low value (TEST5=3F hex, TEST3=10 hex). Measure the output frequency. Similarly, set the frequency to a high value (TEST5=30 hex, TEST3=17 hex). Measure the output frequency.

Based on these measurements you can check whether the VCO tuning range is OK. Is your desired channel within this VCO tuning range and is the channel centered satisfactorily? If not, you will have to change the VCO inductor.

4) Check the current consumption

Approximately 25.4 mA in Tx (max power) and 7.7 mA in Rx. See CC1000 data sheet for more details. You will also get values from Smart RF Studio.

5) Is your configuration correct?

One way to simplify the HW debugging: Use SmartRF Studio and connect the control lines (PDATA, PCLOCK and PALE) from the CC1000EB over to your own testboard. Then you will know that the software/register values are OK and the calibration procedure is correct.

The SmartRF Studio operates through the PC parallel port. The PC parallel port operates at 5 V, so a voltage translator is needed between the PC and the RF module. The table below gives the pin numbering for the 25 pin PC parallel port connector.

PC parallel port pin number	Signal CC1000
4	PDATA (IN)*
3	PCLK
5	PALE
11	PDATA (OUT)*
13	CHP_OUT(LOCK) (this pin is optional)
2	5V (to supply translator)
18-26	GND

* The PDATA line is split in two as the PC parallel port pin is not bi-directional

An alternative to building a 5-to-3 Volt translator is to use the one on the Evaluation Board. The control signals (3 V) can be found at the board as given in the table below:

Signal	CC1000 Evaluation Board connection
PDATA	U3#8
PCLK	U3#4
PALE	U3#12
CHP_OUT(LOCK) (this pin is optional)	TESTPIN TP2
5V (to supply translator)	C26
GND	Groundplane

Note: The Ampere meter short circuit (at the voltage supply connector) must be removed in order to disconnect the power supply for the on-board transceiver and thus avoid interference from that device.

Please refer to the Evaluation Board schematics and layout for further details. The schematic and layout are found in the Development Kit User Manual.

6) It is always a good idea to test the Rx and Tx parts separately before setting up an RF link

Set up one CC1000 as a receiver. Measure the LO-leakage at the antenna. Tune the output frequency if required. Connect an RF generator to the antenna input to give an ideal RF signal. The frequency of the RF generator must be 150 kHz *below* the receiver LO frequency if high-side LO is used. Conversely, 150 kHz *above* the receiver LO frequency if low-side LO is used. Use FSK modulation with appropriate deviation and modulation rate. If you do not have the equipment to send FSK modulation, you can use an RF generator with FM modulation and use an external function generator to modulate the signal with a square wave. If you are in NRZ or UART mode the modulating signal should be equal to bitrate/2 (= baudrate/2) when sending alternating 0's and 1's. If you are in Manchester mode the modulating frequency should be equal to bitrate/2 (= baudrate/4) when sending alternating 0's and 1's.

If you are in receive and your transmitter is off you only receive noise. Hence, the demodulator will demodulate noise and this is what you see on the DCLK pin (in UART mode) or DIO pin (in NRZ/Manchester mode).

In synchronous NRZ mode and UART mode each bit is sampled 6 times. As an example, if you program 9.6 kBaud, each bit is 104.2 μ s. The "jitter" can then be 17.4 μ s (104/6). If the clocks are drifting or the signal is noisy then the bit synchronizer will keep on synchronising to track the signal and the DCLK will shift 17.4 μ s for each time a resynchronisation is done. In UART mode you can see the un-synchronous data has this jitter or even spikes due to noise because no bit decision is done in the chip. If you are going to use the UART mode, make sure that the UART does proper oversampling and that it can handle the jitter the RF communication introduces. In Manchester mode each bit is sampled 12 times. That is, each baud ('chip') is sampled 6 times. If you use Manchester mode the jitter will still be 17.4 μ s.

The NRZ and Manchester modes have the advantage that the data clock DCLK is available and that bit synchronisation and data decision is done on-chip (you have paid for this feature - so why not use it!). Using synchronous NRZ or Manchester mode will always give you a robust signal interface with a synchronous clock!

Set up one CC1000 as a transmitter. Check the output power and the output frequency (set FSEP=0 to find the carrier). Tune the output frequency if required. The output frequency should be 150 kHz above or below the LO frequency in Rx mode as measured above.

When the results from the above measurements are satisfactory you can use two CC1000 to set up an RF-link (through air or coax and attenuators).

7) RF Link

In your final system when using the Synchronous Manchester or the Synchronous NRZ mode, the DCLK pin on the CC1000 should be connected to an input pin that can generate an interrupt in the MCU. DIO should be connected to a bi-directional I/O pin.

In Tx mode, the interrupt should be triggered on the falling edge of DCLK. When the interrupt occurs, write the next bit to be transmitted to the I/O pin. The data is clocked into CC1000 at the rising edge of DCLK. In Rx mode, the interrupt should be triggered on the rising edge of DCLK. When the interrupt occurs, read the data from the I/O pin.

When setting up the RF-link using 2 CC1000 you must ideally use DCLK to synchronise the data (DIO) into the transmitter. If not, CC1000 tries to synchronise the data input to its internal clock. If there is a mismatch between the internal clock and DIO there might be bit errors.

Note that data transferred to/from the MCU is always NRZ coded, regardless of whether Synchronous NRZ or Synchronous Manchester mode is selected. The mode setting only affects the signal modulated onto the RF carrier. The Manchester encoding/decoding is done internally by the CC1000.

8) Locking the averaging filter.

The preamble is used to set up the correct decision level for the internal bit slicer (averaging filter). The bit synchronizer will synchronize as long as you are in Rx. That is, both during the preamble and data. Synchronization is handled internally.

At the **minimum** it takes 11 bauds to fill the averaging filter. In addition, 3 bits are required for synchronization (compare Manual Lock for NRZ and UART mode in Table 3, page 17 in the data sheet). This corresponds to SETTILING[1:0] in register MODEM1 being '00'. Using a different value for SETTILING[1:0] gives improved sensitivity (not much) at the expense of a longer preamble. In addition you might need 4-8 bits to detect a valid preamble.

If manual lock is selected:

Make sure you manually lock the averaging filter the first time you are in Rx in order for the decision level to be saved.

Although the averaging filter keeps the threshold value after power down it might be a good idea to manually lock the filter every time you receive data (unless there is a good reason for not doing so).

If you decide to manually lock the filter the first time you enter Rx there is no need to send a long dc balanced preamble when you re-enter Rx-mode. You only need to send a short preamble (for synchronisation) when you enter Rx from Tx or PD in this case.

If automatic lock is selected:

You have to send a preamble each time you enter to Rx-mode. This is to set the averaging filter correctly. Note that the automatic lock is not intelligent; i.e. it does not detect valid data in any way.

Finally, in CC1000 there is no constraint with respect to the RF link having to be (even moderately) balanced (which some receivers require). After you have locked the averaging filter you can send any number of consecutive 0's or 1's.

9) Procedure for detecting packets in NRZ/Manchester mode

1. Search for the preamble. This is most easily done by simply shifting the data into a shift register, and then comparing the register to 0xAA and 0x55. Once you have one of these values, you go on to the next step.
2. Declare a tentative "preamble detected" (set a flag or something), and continue shifting in data. If you're in NRZ mode, lock the averaging filter now. Compare the data to your SOF (start-of-frame, a unique ID which is sent at the start of your data stream), if you find this, go to the next step. If not, compare it to 0xAA and 0x55. If it isn't equal to one of these, you have an error. You may want to tolerate a few errors here, but if you get several, give up and go back to step 1.
3. OK, you've found your SOF. Depending on the application, you may want to add another byte of SOF (if you have problems with noise showing up as data). If you do this, compare the data to your second byte of SOF; go back to 1 if it does not match.
4. Done! You now know you are receiving valid data. If your data packets are of variable size, you can either add a size field in the packet header, or have a specific end-of-packet marker. Just make sure to handle it gracefully if this info should be subject to bit errors. A CRC checksum at the end of the packet is a good idea; you can then discard or retransmit the data according to the needs of your application.

If you are in the Manchester mode, you'll probably want to include the Manchester Violation bit as well to the above procedure, if you get a violation, you can count it as an error. The Manchester violation signal (available at CHP_OUT if you set the LOCK register correctly) is updated each bit (just as the DIO pin), the threshold for declaring a violation can be set in the MODEM1 register. The Manchester violation flag is an additional piece of information to use in the procedure, and does not replace it.

The procedure above is applicable to an application where you are in receiving mode looking for data all the time. If you are doing polling, awakening at intervals to see if there is any data, you should limit the time you spend in step 1, going back to sleep if you don't find a preamble after a suitable amount of time.

10) Procedure for detecting packets in UART mode

There are some issues regarding detection of preamble, locking of averaging filter, and byte synchronisation you need to consider:

1. Search for the preamble. Searching for 0xAA and 0x55 most easily does this. Once you have one of these values, you go on to the next step.
2. Manually lock the averaging filter.
3. Byte-alignment. See <http://www.piclist.com/techref/microchip/ammermansync.htm> for more information on this. Disregard the constraint/comment regarding the maximum number of consecutive 0's and 1's. In CC1000 there is no constraint with respect to the link being moderately balanced because you have locked the averaging filter in 1) above (the preamble must be dc balanced).
4. Depending on the application, you may want to add another byte of SOF (if you have problems with noise showing up as data). If you do this, compare the data to your byte of SOF, go back to 1 if it does not match.
5. Done! You now know you are receiving valid data. If your data packets are of variable size, you can either add a size field in the packet header, or have a specific end-of-packet marker. Just make sure to handle it gracefully if this info should be subject to bit errors. A CRC checksum at the end of the packet is a good idea, you can then discard or retransmit the data according to the needs of your application.

The procedure above is applicable to an application where you are in receive mode looking for data all the time. If you are doing polling, awakening at intervals to see if there is any data, you should limit the time you spend in step 1, going back to sleep if you don't find a preamble after a suitable amount of time.

Since only raw data is provided in UART mode, synchronization or decoding must be done by the UART. Make sure that the UART does proper oversampling and that it can handle the jitter the RF communication introduces.

11) LO leakage

The most important issue in reducing LO leakage is VCO inductor type and placement. Among all the inductors we have tried, we strongly recommend using the KOA part listed in the data sheet or a similar spiral thin film inductor, as this provides the best LO performance. Please note that LO leakage can be dependent on inductor orientation, the KOA part has a thick yellow marking on one side which can be used to indicate orientation.

The second thing you should try is to step through different values for the decoupling capacitors, decoupling is especially important for the LNA (pin 5) and VCO (pin 9) power pins.

The LO signal can couple to the antenna output in two ways, either through the PCB wires from the power supply, or through radiation from the VCO inductor to other components or PCB routes. Better decoupling may be necessary to prevent the signal from coupling via the power supply. We have developed the CC1000PP layout with LO leakage very much in mind. Have a look at this layout to see a good PCB layout for low LO leakage.

As a general advice, keep the VCO inductor as close as possible to the chip, with symmetrical connections to the pins. Also, make sure you have good decoupling of the VCC. See also Application Note AN002 "LO emission" for more details.

Instrumentation

It is not possible to do RF development or RF module design without proper RF instrumentation.

The *minimum* RF instrumentation required is:

- Spectrum Analyser (SA) covering up to 3 times the RF frequency used (3rd harmonic)
- RF signal generator with FSK modulation capability
- Network analyser would also be necessary if RF filter optimisation, input/output matching and antenna tuning must be done.

Module testing

Below is a list of important RF parameters to verify once a new design is done. However, the list should not be considered as complete, but advisory. Also additional testing must be done to comply for type approval.

This list is also useful if you require help from Chipcon's support team. Fill in the table and include it with your e-mail to support@chipcon.com.

Step-by-Step Testing Procedure

DEVICE NUMBER:				
#	Test	Value	Unit	Condition
1	Voltage Supply			
	Supply voltage		V	Measure across device supply pins
2	Current consumption			
	RX mode		mA	
	TX mode		mA	at PA output power programmed: ____dBm
	PD mode		uA	Xtal oscillator is (on/off): ____
3	Crystal oscillator			
	Crystal frequency		MHz	Measure approximate frequency using an oscilloscope.
	Oscillator voltage		mVpp	Measure at peak-to-peak voltage at XOSC_Q1 pin
4	RF frequency			
	RF frequency		MHz	at RF frequency programmed: ____MHz Set device to TX mode, NRZ mode, Frequency separation = 0 Hz. Calibrate. SA: SPAN=100 kHz, RBW=1 kHz, VBW=Auto
5	VCO tuning range			
	VCO min. frequency		MHz	Set device to TX mode. Measure with a spectrum analyser at antenna output. Configure the chip to a very low/high frequency as explained on page 2. SA: SPAN=200 MHz, RBW=Auto, VBW=Auto
	VCO max frequency		MHz	
6	Phase noise			
	Phase noise at 100 kHz offset		dBc/Hz	SPAN=200 kHz, RBW=1 kHz, VBW=10 Hz
7	Modulation			
	Peak to peak deviation		kHz	Measure the distance between the two tops in the spectrum SPAN=500 kHz, RBW=3 kHz, VBW=1 kHz
	Modulation response		kHz	Use Spectrum Analyser FM demodulator option (frequency versus time). Measure frequency separation. Make plot.
8	TX output power			at PA output power programmed: ____dBm PA_POW: ____
	Output power		dBm	SPAN=1 MHz, RBW=10 kHz, VBW=1 kHz
9	Harmonics			
	2. harmonic			SPAN=1 MHz, RBW=10 kHz, VBW=1 kHz
	3. harmonic			
10	LO leakage			
	Frequency			Shall be 150 kHz above/below the carrier frequency measured above SPAN=1 MHz, RBW=10 kHz, VBW=1 kHz
	LO leakage		dBm	SPAN=1 MHz, RBW=10 kHz, VBW=1 kHz
11	Receiver sensitivity			
	Sensitivity		dBm	Use signal generator set up with correct modulation frequency and deviation. View DIO and DCLK signal using an oscilloscope. Adjust level until BER = 10^{-3}

Notes to the tests

1. Supply voltage

The supply voltage should be in the range 2.1 – 3.6 V. Operation is not guaranteed outside this range. If measured voltage is less than expected it could be a current limiter in the power supply causing the problem.

2. Current consumption

The typical current consumption for the different modes are calculated by SmartRF Studio, and can be seen in the *Status bar* of the *Normal view*. It is also available in the data sheet.

3. Crystal oscillator

The crystal oscillator operation can be verified very simply using an oscilloscope. However, the actual frequency must be measured when testing the transmitter frequency because the oscilloscope probe would load the crystal and de-tune it during the test. The peak-to-peak voltage should be 400 – 600 mVpp.

4. RF frequency

This test measures the accurate RF frequency and hence the crystal frequency. Set the device to TX mode, NRZ mode and the frequency separation to 0 Hz. Measure with a spectrum analyser at the antenna output. If the measured frequency is off by a few kHz, then the load capacitance for the crystal must be changed. If it is far from the expected frequency, most likely the VCO tuning range is wrong, or calibration has not been done correctly.

5. VCO tuning range

The VCO tuning range is measured by forcing the tuning voltage to min/max by programming a very low/high frequency. It is important to have a correct (large enough) tuning range in order to cover the desired frequency for all expected component tolerances. Changing the VCO inductor value will change the tuning range.

6. Phase noise

The phase noise depends on the loop filter bandwidth, but should typically be –85 dBc/Hz. When measuring the noise using a spectrum analyser the measurement must be corrected for the resolution bandwidth. Using 1 kHz resolution bandwidth, the measurement must be corrected with -30 dBHz ($10\log(1000)$). That means, if you are measuring the noise 100 kHz away from the carrier to be –55 dBc using 1 kHz resolution bandwidth, the phase noise is $(-55 - 30) = -85$ dBc/Hz at 100 kHz offset.

7. Modulation

Looking at the modulation spectrum can help to discover any problems with the loop bandwidth. The peak-to-peak deviation should be close to the specified frequency separation. An excessive deviation could be due to low phase/gain margin in the PLL leading to “peaking” in the closed loop response. If this is the case, the calibration and the TEST0, TEST2 and TEST4 registers should be investigated. Looking at the modulation response using an FM demodulator can also tell a lot about the loop response.

8. TX output power

The output power should be close to the specified output power, but taking the harmonic filter loss into account. The insertion loss of a low pass LC filter is typically 1.5 – 2 dB. If the output power is too low, the LC filter should be checked. The filter is very sensitive to layout paracitics.

9. Harmonics

The transmitter harmonics should be attenuated sufficiently by the LC low-pass filter. Some spectrum analysers provide automatic measurement of harmonics presenting the result as a list for convenience.

10. LO leakage

The LO leakage is measured at the antenna output when the transceiver is in receive mode. The LO frequency will be 150 kHz above or below the RF carrier frequency, depending on whether low-side or high-side LO injection is used (programmable from SmartRF Studio).

11. Sensitivity

Assuming you do not have a Bit Error Tester the sensitivity is measured using a signal generator with FSK modulation at the specified frequency and deviation. If you do not have the equipment to send FSK modulation, you can use an RF generator with FM modulation and use an external function generator to modulate the signal with a square wave (see page 3). The Rx DIO signal and the modulating signal are monitored using an oscilloscope. A bit error rate (BER) of 10^{-3} can then be determined visually. The expected sensitivity for different data rates, frequency separations and current settings are shown in the CC1000 data sheet. Any loss in the front-end filter must be taken into account.

Less than expected sensitivity can be due to mismatch at the LNA input, excess loss in the front end filter, or frequency offset between transmitter and receiver.

12. Still problems?

Contact your local distributor (or Chipcon directly) if you still need help on your RF circuit design. Fill in the test table above as carefully as possible and send to us for further advice.

For more detailed information

Read the information on our web-site. There are several detailed application notes available as well as a FAQ data base.

General Application Notes:

AN_001_SRD_Regulations
AN_002_LO_emission
AN_007_Manufacturers
AN_021_Voltage_Level_Conversion

CC1000 specific Application Notes:

AN_009_CC1000_MCU_Interfacing
AN_011_Programming_the_CC1000_frequency_for_best_sensitivity
AN_015_RF_Modem_Reference_Design
AN_016_CC1000_CC1050_On_Off_Keying
AN_019_Crystal_Oscillator_Issues_CC1000_CC1010
AN_020_Remote_Keyless_Entry_Reference_Design

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Contact Information

Address:

Chipcon AS
Gaustadalléen 21
N-0349 Oslo,
NORWAY

Telephone : (+47) 22 95 85 44
Fax : (+47) 22 95 85 46
E-mail : wireless@chipcon.com (information about RF-IC products)
support@chipcon.com (support on our standard products)
Web site : <http://www.chipcon.com>

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