# Development of a PC-Based Object-Oriented Real-Time Robotics Controller

by

### Hang Tran

A thesis presented to the University of Waterloo in fulfillment of the thesis requirement for the degree of Master's of Applied Science in Mechanical Engineering

Waterloo, Ontario, Canada, 2005

©Hang Tran, 2005

I hereby declare that I am the sole author of this thesis.

I authorize the University of Waterloo to lend this thesis to other institutions or individuals for the purpose of scholarly research

Signature

I further authorize the University of Waterloo to reproduce this thesis by photocopying or by other means, in total or in part, at the request of other institutions or individuals for the purpose of scholarly research.

Signature

### Abstract

The industrial world of robotics requires leading-edge controllers to match the speed of new manipulators. In order to improve the performance of the Deltabot, an ultra high-speed cable-based robot, a new controller called the QNX Multi-Axis Robotic Controller (QMARC) was developed. QMARC is a PC-based controller built for the replacement of the existing commercial controller called PMAC, created by Delta Tau Data Systems. Although the PMAC has its own real-time processor, the rigid and complex internal structure of the PMAC makes it difficult to apply advanced control algorithms and interpolation methods. Adding unconventional hardware to PMAC, such as a camera and vision system is also quite challenging. With the development of QMARC, the flexibility issue of the controller is resolved. QMARC's open-sourced object-oriented software structure allows to the addition of new control and interpolation techniques as required. In addition, the software structure of the main Controller process is decoupled for the hardware, so that any hardware change does not affect the main controller, just the hardware drivers. QMARC is also equipped with a user-friendly graphical user interface, and many safety protocols to make it a safe and easy-to-use system.

Experimental real-time test has proven QMARC to be a reliable real-time system. Despite minor fluctuations in the servo loop periods, the controller can still achieve close path tracking running at 2.5 kHz. In comparing the PMAC and QMARC controller performance on two pick-and-place paths, it was found that for both paths QMARC yielded better results than PMAC on all three motors of the Deltabot. Accumulated following error for the PMAC was at least one order of magnitude greater than QMARC, and QMARC was more easily tuned than PMAC. These experimental results show that QMARC is a reliable and safe controller with consistent results.

The stable software foundation created by the QMARC will allow for future development of the controller as research on the Deltabot progresses. Its open source structure will ease the way for new researchers implementing software modules such as servo control algorithms and trajectory, or new hardware like grippers and vision sensors, creating a flexible and powerful system that can be used for many applications.

### Acknowledgements

For the past two years, I have received a generous amount of help and guidance from my supervisors, Dr. Amir Khajepour and Dr. Kaan Erkorkmaz. I would like to thank Dr. Khajepour for taking me into the Robotics research group, which has provided me with both practical experience in robotics control, and academic experience in the development of new robotic manipulators, such as the Deltabot. I also thank Dr. Erkorkmaz for sharing his knowledge and expertise in control systems, trajectory generation and software development, which was pivotal in my research.

I take great pride in my work, but where would I be without the help of my peers and colleagues. I would like to give a big hug to Edmon Chan for his insight into all things mechanical and electrical, Saeed Behzadipour for his assistance in my research, Gireesh Dharwarkar for keeping me on my toes, and Matthew Asselin for sharing his knowledge of the QNX operating system with me without hesitation.

With all of the software and hardware implementation involved in this project, I would like to graciously thank Robert Wagner, Andy Barber and Steve Hitchman, our fine technicians, for their help and kindness to us pesky students.

I would like to thank my family for their undying support when I told them that I wanted to continue my education and especially my boyfriend, Neil Lonsdale, for encouraging me and picking me up when things went astray in my research.

Last, but not least, I would like to acknowledge the financial support of Materials and Manufacturing Ontario (MMO) in this research. Without their support our ideas could not have been realized.

## Contents

Chapter	1 Background	1
1.1	Deltabot	1
1.2	PMAC	
1.3	QNX Real-Time Operating System	4
1.4	Object-Oriented Software Design	6
1.4.	1 Reusability	6
1.4.	2 Encapsulation	7
1.4.	3 Inheritance	7
1.4.	4 Polymorphism	
1.4.	5 Operator Overloading	9
1.4.	6 Constructors and Destructors	9
Chapter	2 Literature Review	
2.1	PC-Based Controllers	
2.1.	1 Distributed Multiprocessor Control Systems	
2.1.	2 Single-Processor Host and DSP Control Systems	
2.2	Object-Oriented Software Design in Robotic Controllers	
2.3	Robot Control Structure	
2.3.	1 Trajectory Generation	16
2.3.	2 PID Control Algorithm	
Chapter	2 Design and Implementation	
3.1	Overview	
3.2	Hardware Setup	
3.3	Process Structure of the QMARC	
3.3.	1 QNX Message-Handling Functions	
3.4	Design of the Controller Console	
3.5	Design of the Starter Process	

3.6	Design of the Hardware Server	
3.7	Design of the Timer	
3.8	Design of the Controller	
3.9	Running the Controller	44
3.10	Safety Features	44
3.10	0.1 Hardware Limit Switches	44
3.10	0.2 Software Position Limits	45
3.10	0.3 Following Error Limit	46
3.11	Control Algorithm	46
3.11	1.1 Notch Filter	
3.12	Trajectory Generation	
3.12	2.1 Offline Cubic Spline Trajectory Generation	
3.12	2.2 Online Position-Velocity-Time (PVT) Trajectory Generation	
Chapter	4 Software Design Issues	
4.1	Timing	
4.1.	1 POSIX Timer vs. QMARC Timer	53
4.2	Data Logging	54
4.3	Memory Allocation of Variables	55
Chapter	5 Software Testing and Analysis	57
5.1	Real-Time Behavioural Tests and Results	
5.2	Controller Performance Tests and Results	60
5.2.	1 Standard X-Z Plane Path Test	61
5.2.2	2 Rotated Standard Path Test	69
5.3	Reproducibility Tests and Results	75
Chapter	<b>6</b> Conclusions Error!	Bookmark not defined.
Chapter	7 <b>Recommendations</b> Error!	Bookmark not defined.
Bibliogra	aphy	

## List of Figures

Figure 1-1: General structure of the Deltabot [5]	2
Figure 1-2: Encoder Conversion Table Process [6]	3
Figure 1-3: Class inheritance code example	7
Figure 1-4: Polymorphism class declaration example	8
Figure 1-5: Polymorphism function call example	9
Figure 2-1: Block Diagram of Kriegman and Siegel hand control system [18]	12
Figure 2-2: QMotor 2.0 Hardware/Software Architecture [33]	15
Figure 2-3: Class Hierarchy of QMotor Robotic Toolkit Platform [33]	16
Figure 3-1: QMARC Control Structure	22
Figure 3-2: QMARC Process Communication Structure	24
Figure 3-3: Message Structure for Client-Server Communication	25
Figure 3-4: Example code for client-server communication and message-handling	26
Figure 3-5: QMARC Photon Graphical User Interface (GUI)	29
Figure 3-6: Flow Chart of Starter Process	31
Figure 3-7: Flow-chart for Hardware Server	33
Figure 3-8: Code for Timer ISR and Setup Procedure	34
Figure 3-9: Class structure of robotic motion controller	36
Figure 3-10: Flow-chart of algorithm for offline trajectory generation control loop, ctrlLoop()	41
Figure 3-11: Flow-chart of algorithm for online trajectory generation control loop,	
ctrlLoopOnlineTraj()	42
Figure 3-12: Schematic of PID Feed-Forward Velocity and Acceleration Control Algorithm	47
Figure 3-13: Schematic of path for PVT online trajectory generation	50
Figure 4-1: Memory allocation code sample	55
Figure 5-1: Real-Time Servo Loop Period Variation in a Step Input Test	59
Figure 5-2: Standard X-Z Plane Path in Cartesian Space	61
Figure 5-3: X-Z Plane Path – Arm Positions with Selected Path Knots	61
Figure 5-4: X-Z Plane Path – End-Effector Position using PMAC and QMARC	62
Figure 5-5: X-Z Plane Path - Arm Positions for PMAC and QMARC with Cubic Spline	63

Figure 5-6: X-Z Plane Path - Arm Position Errors for PMAC and QMARC with Cubic Spline	65
Figure 5-7: X-Z Plane Path - Command Velocity using PMAC and QMARC with Cubic Spline	66
Figure 5-8: X-Z Plane Path – Command Velocities for PVT and Cubic Spline on QMARC	67
Figure 5-9: X-Z Plane Path – Arm Position Errors with PVT and Cubic Spline on QMARC	68
Figure 5-10: X-Z Plane Path - Command Acceleration	69
Figure 5-11: Rotated Standard Path in Cartesian Space	69
Figure 5-12: Rotated Path - Arm Positions with selected path knots	70
Figure 5-13: Rotated Path - End-Effector Position for PMAC and QMARC	70
Figure 5-14: Rotated Path – Arm Position for PMAC and QMARC	72
Figure 5-15: Rotated Path – Arm Position Error for PMAC and QMARC	73

## List of Tables

Table 1: QMARC Controller Gains	.60
Table 2: Arm Position Errors (in radians) for PMAC and QMARC using Cubic Spline	. 64

### Chapter 1

### Background

Robotics is being used for increasingly more applications in different industries. The mass production of everything from cars to surgical needles requires precision repetitive work ranging from assembling parts, welding, machining, and pick and place tasks. To control these robots, engineers have built a multitude of controllers using Programmable Logic Controllers (PLC's), Digital Signal Processing (DSP) boards and Personal Computers (PC's). Although PLC's are still widely used in industry, research in the past decade or so has been concentrated on the development of PC-based controllers for industrial applications. Typically, DSP controllers with host computers have been used as controllers, however the high cost and complexity have made PC-based controllers a desirable field of research. In this work, a single-processor PC-based controller was developed for a three degree-of-freedom ultra high-speed cable-based parallel robot, named the Deltabot, created at the University of Waterloo [1], [2].

### 1.1 Deltabot

The Deltabot was designed based on the Stewart Platform [3], a six degree-of-freedom mechanism developed for flight simulations that used six linear actuators in parallel created in 1965. The parallel structure of the Deltabot is depicted in Figure 1-1. This cable-based robot is among a new line of high-speed robots built for pick-and-place operations. In its novel design, there are three motors attached to three aluminum arms that control the location of the end-effector through a set of lightweight cables. The end-effector is attached to a central shaft that is pressurized to keep the cables in tension. By using cables instead of rigid links, the inertia of the manipulator is minimized, thus allowing high accelerations of 2g. Currently, this prototype can run a 35cm path at 120 cycles per minute [4].



Figure 1-1: General structure of the Deltabot [5]

Parallel manipulators have distinct advantages over serial chain-link counterparts, namely, greater stiffness, higher precision and less inertia. However, these advantages come at the cost of singular configurations in the workspace, and smaller and more complex workspaces. For parallel manipulators, computation of the forward position kinematics is a challenging task involving non-linear equations. Whereas the inverse position kinematics calculation is relatively straightforward. This is opposite to kinematic calculations for serial manipulators. Due to the nature of parallel manipulators, more computation is required for proper control of the robot [4]. In addition, more advanced control algorithms must be considered for the Deltabot because, not only is it a parallel manipulator, but it also has cable-based links. In spite of disadvantages with control and workspace issues, parallel manipulators offer promising performance speed and precision for pick and place operations.

### 1.2 PMAC

Currently, the Deltabot uses a general-purpose commercial controller called the Programmable Multi-Axis Controller (PMAC) version 2.0 made by Delta Tau Data Systems Inc [6]. The PMAC does not perform the inverse or forward position kinematics on the manipulators, but rather it performs control based on joint coordinates. This controller is composed of a real-time multi-tasking computer with DSP technology. Although the PMAC has the capability to control up to eight motors simultaneous on eight separate coordinate systems, each standard PMAC 2.0 module controls only four motors. The software architecture of the PMAC is complex and somewhat hidden to make it simpler for users. What is known is that each PMAC module contains four encoder inputs, which each has hardware encoder counters with associated timers. As shown in Figure 1-2, at the end of each servo cycle, a servo interrupt is sent to latch the counter values and store them in a software structure called the Encoder Conversion Table. This Encoder Conversion Table consists of two columns: X memory and Y memory. In X memory, the actual 24-bit value of the encoder position is stored in the highest word. The rest of the X memory contains intermediate values. Memory Y contains the information required to process and convert the position value so that it can be stored in the X memory location. Y memory consists of a 16-bit address of the source of the encoder that it is reading from plus an 8-bit value of the conversion method performed on the encoder value. The actual position is then extended to 48-bits by the software, which also multiplies the value by a position-scaling factor. Actual encoder positions are used as feedback data for the servo control loop. When the new servo control signal is calculated, the signal is sent at an opto-isolated set of Digital to Analog Converters (DAC) that are connected to the motor amplifier.



Figure 1-2: Encoder Conversion Table Process [6]

Although the PMAC has a wide range of options and an impressive range of capabilities that allow users to tailor the controller to each application, the process of understanding the PMAC architecture and modifying its programming is very slow and sometimes difficult due to the complexity of the PMAC system. Adding unconventional components to the controller, such as a vision system, can be quite challenging, time-consuming and costly. Due to the complex nature to the Deltabot's mechanical structure, more advanced control algorithms must also be considered for control of this cable-based manipulator.

In order to minimize hardware costs as well as allow for higher system flexibility in the controller, the PC-based controller was developed for motion-control of the Deltabot. The open-source code of the PC-based controller will allow future research to quickly produce controllers with advanced control algorithms for the Deltabot, along with the incorporation of sophisticated trajectory generation techniques, which cannot be performed by the PMAC.

In this research, a single-processor PC-based motion controller was developed on a real-time operating system called QNX Neutrino 6.0. This controller is named the QNX Multi-Axis Robotic Controller or QMARC. A literature review on different aspects of the real-time control systems will be discussed in Chapter 2. The detailed software design of the controller, from its object-oriented software structure to its control algorithm and safety features will be covered in Chapter 3. Chapter 4 will review the issues that arose during the development stage such as timing, logging data, and memory management, followed by the experimental results of the PC-based controller compared to the PMAC performance in Chapter 5. To produce comparable results, the PC-based controller was programmed with similar control and trajectory generation algorithms as the PMAC. The conclusions of this research along with details on future work will be discussed in Chapter 6.

### 1.3 QNX Real-Time Operating System

An operating system (OS) is a software platform on computers that manages resources, and controls memory and peripheral devices. Its responsibilities include performing all input/output operations and efficient use of devices [7]. In order to qualify as a real-time operating system (RTOS), the OS must be able to perform duties within a given time constraint, whether that objective time is measured in microseconds or milliseconds. A RTOS must also be able to handle simultaneous tasks that are triggered asynchronously as well as have an effective method of scheduling these tasks. The main function of the RTOS is to allocate processor time to different processes and have the ability to stop

and resume any task. QNX Neutrino 6.0 is an example of a RTOS developed by QNX Software Systems. The QNX operating system is a modular operating system with high fault tolerance, in the case of a device driver failing, the entire OS will not crash. A thorough analysis of different commercially available real-time operating systems was not the objective of this research. Instead, QNX was found to be the most economically choice for a RTOS that was suitable for development of the motion controller.

In a motion controller, there are multiple tasks that need to be performed simultaneously, such as monitoring limit switches, performing input/output operations to hardware, and performing the control loop and online trajectory generation on multiple motors. Saying that an RTOS can run multiple processes simultaneously, however, does not necessarily mean that the speed of task will be completed more quickly. This is because the computer usually still has only one processor and multiple tasks are not truly run "concurrently". There are different methods of scheduling processes so that each task can have a chance to run on the processor according to their *priority*, a numerical value assigned to each process. In *priority-based execution*, a ready process with higher priority will run first and to completion if the processor is idle. In *pre-emptive priority-base execution*, any task can be stopped, or pre-empted, if a higher priority task is suddenly ready, and the interrupted task will only continue when the high priority task is completed [8]. QNX uses pre-emptive priority-based scheduling with two different types of scheduling algorithms: First-In First-Out (FIFO) and Round Robin (RR) with 64 priority levels.

In FIFO scheduling a task can run on the processor as long as it wants, unless a higher priority task is ready to run. Tasks with the same priority are locked from running, and wait in a first-in first-out queue. Lower priority tasks get an opportunity to run when there are no other tasks ready. RR scheduling is pretty much the same as FIFO except tasks can only run for a predefined timeslice that can be set by the programmer. If the task is not complete after the timeslice is up, another task with the same priority will have the opportunity to run. For this research, RR scheduling is used for all processes and threads. A *process* refers to any application running on the processor, whereas *threads* are created from within a process and typically run smaller segments of code for increased parallelism in the software.

In QNX multiple processes can communicate through "message-handling". The idea of message handling is that one process can send a message to another process to trigger an action in the other process or simply to deliver or request data. When the second process has handled the message, it sends a reply message back to the first process, which also unblocks it. To prevent *dead-locking*, a

phenomenon with multiple processes whereby all process are blocked waiting for a message, it is common practice to only send messages that request action or information to a server. A server is a process that runs in an infinite loop waiting for messages from client processes. In client-server software architecture, only clients send messages requesting data, and only the server sends reply messages [9].

### 1.4 Object-Oriented Software Design

Object-oriented design (OOD) is a method of programming whereby objects and concepts in the real world are used as the basis for building functions in the program. By grouping functions that are normally associated together into single entity, we express code in a more comprehensive way, which in turn makes the program easier to understand, maintain and modify.

OOD uses the concept of a *class* to group together a set of functions and properties related to the same entity. For instance, a class written to control a modem would contain actions performed on a modem, such as connecting to a port, dialing a number and hanging up. Theses actions would be written in code referred to as *member functions* of the class, or *methods*. Attributes of the modem, such as ringer volume, are called *member variables*. Grouping code into a class structure allows for reusability of the code. Other important properties of OOD are reusability, encapsulation, inheritance, polymorphism and operator overloading [10]. In addition, constructors and destructors can be used in OOD to facilitate class initialization and destruction.

### 1.4.1Reusability

Writing code for any task consumes both time and resources. The prospect of writing code that is reusable is therefore a highly desirable and practical. Programming languages such as C, C++, Java, Visual Basic, and Fortran are all examples of languages that provide code in the form of classes allowing programmers to develop software without having to write every single function from scratch. A well-written class can be used to in any application, for instance, CString is a C++ class that allows for the easy manipulation of character strings, can be used in any C++ program.

#### 1.4.2Encapsulation

Classes are written to allow high reusability, however, encapsulation is often used by programmers who do not want to reveal the details of their software structure, or do not want other programs to have access to functions or variables that are used internally. OOD allows programmers to define components as either *public* or *private*. Public variables and functions can be accessed by other programs outside of the class, whereas private variables cannot be accessed. Public and private labels are found in the class definition, as shown in Figure 1-3. By defining a concrete interface for a user, class functions are protected from improper function calls and make the classes simpler to use.

### 1.4.3Inheritance

Inheritance is another method of reusing code but specifically from an existing class, called a *base class*. A class can *inherit* the member functions and variables of a base class by how the class is defined. In C++ the declaration of a base class is shown in Figure 1-3. The base class contains one integer-type member variable, iBaseVar, and one member function called funct1(). The subclass CSubClass is defined as a subclass of public CBaseClass by using a single colon in the class definition. By doing this, all of the public member functions and variables of CBaseClass are automatically inherited by the subclass. Since variable iPrivateVar is a private member variable, it is not inherited by CSubClass. Functions and variables of the base class are often very general; therefore, subclasses usually add variables and functions that are more specific to its application.

```
//Base Class declaration
class CBaseClass
public:
    int iPublicVar;
                            //Declare member variables
    void funct1(void);
                            //Declare member functions
private:
    int iPrivateVar;
};
class CSubClass:public CBaseClass
    //Inherits all of the public variables and functions from CBaseClass
    //Add more specialized member variables
    int iSubClassVar;
    //Add more member functions
    void funct2(double);
};
```

```
Figure 1-3: Class inheritance code example
```

#### 1.4.4Polymorphism

Polymorphism is the ability of a subclass to implement a different version of a member function inherited from its base class. To keep the interface to the classes uniform, the subclass must have the same function definition as the base class, however the contents of the function can be different. In addition, the function must be declared as a *public virtual* function in the base class. A *virtual* function is one that can be overloaded by a subclass. A *public* function is one that can be accessed outside of the class. Based on the code segment from Figure 1-3, in order to redefine funct1() in CSubClass, funct1() must be declared as a virtual function in CBaseClass, as shown in Figure 1-4. Subclasses must also be declared from *public* base class. The virtual function in the base class must be implemented in order for the subclass to inherit it, ie. you can not simply declare the virtual function.

A pointer to CBaseClass can be used to point to any instance of its subclasses. As shown in Figure 1-5, the compiler will determine which version of the funct1() to use depending on which subclass it is pointing to. In CSubClass2, funct1() is not redefined, so it that case, the funct1() from the CBaseClass will be executed.

```
class CBaseClass
ł
public:
    //Declare member functions
    virtual void funct1(void)
          printf("funct1 in CBaseClass\n");
};
class CSubClass1:public CBaseClass
{
    //Redefine member function funct1()
    void funct1(void)
          printf("funct1 in CSubClass1\n");
};
class CSubClass2:public CBaseClass
{
    //But does not redefine funct1()
};
```

Figure 1-4: Polymorphism class declaration example

```
CBaseClass *classPtr; //Pointer to base class object

CSubClass1 subClass1; //subClass1 object

CSubClass2 subClass2; //subClass2 object

//Point classPtr to CSubClass1

classPtr = &subClass1;

classPtr->funct1(); //Calls funct1() defined in CSubClass1

//Point classPtr to CSubClass2

classPtr = &subClass2;

classPtr ->funct1(); //Calls funct1() defined in CBaseClass
```

OUTPUT: funct1 in CSubClass1 funct1 in CBaseClass

### Figure 1-5: Polymorphism function call example

### 1.4.50perator Overloading

Operator overloading was used in object-oriented design to override a base class function with a subclass function of the same name. If the parameters of the base class and subclass functions are different, then the parameter types used in the function call will determine which version of the function to use. This property is useful with subclasses that require additional parameters, which other subclasses, derived from the same base class, do not require.

### 1.4.6Constructors and Destructors

Constructors and destructors are special member functions that are called on the creation and destruction of a class object. Referring to Figure 1-5 when the "CSubClass1 subClass1" is called, the constructor of the subClass1 can be used to perform initialization actions. Destructors are called when object is deleted using the "delete" command.

### Chapter 2

### Literature Review

### 2.1 PC-Based Controllers

In the economic world, industries are constantly seeking ways to increase productivity while decreasing costs. The development of robotics use in automation has greatly facilitated production gains; however, researchers are constantly looking for more cost effective methods to control robots for greater efficiency.

In the 1970s, industry of robotic control and automation was dominated by Programmable Logic Controllers (PLCs). PLCs were based on "solid-state controllers" as opposed to computer technology, which was in early development stages at that time. Although the PLCs built the foundation for automation, they did not take advantage of the developing technology in electronics and computers. By the 1990s, the solid-state PLCs no longer met the needs of the industry. PLCs were integrated with micro-processors and became more powerful, but Relay Ladder Logic, the programming language of PLCs, were not suitable for high-functions required in modern control systems, such as data communication, diagnostics and data gathering. Engineers found that using controllers built on Personal Computers (PCs) gave them the ability to attain higher-functions, while reducing costs [11].

All complex PC-based controllers used for servo control must be able to perform real-time operations, communicate to peripherals, have high processing power for computations, have the ability to perform multiple tasks simultaneously and have a method to communicate between those tasks. Researchers have found many ways to build control systems that fulfill these requirements such as: using multi-processor computers, building multiple PC and device networks, interfacing with commercial motion controller cards, using Digital Signal Processing (DSP) boards with Host computers, and running the controller on single-processor PCs with Real-Time Operating Systems

(RTOS). When more than one computer is working together for a common goal, then the system is called a "distributed" system [12].

#### 2.1.1Distributed Multiprocessor Control Systems

Multi-processor control systems were used for parallel computations of inverse kinematics, dynamics, trajectory generation and other complex calculations. Many researchers have developed algorithms to determine which control calculations could be done concurrently, to maximize parallelism and hence minimize software execution time. Luh *et al.* [13] used inexpensive processors to increase real-time computation power by processing control algorithms in parallel based on Newton-Euler formulation. Kasahara and Narita [14] also used the Newton-Euler method, but were able to actually implement it on a six-joint robotic arm using a multiprocessing scheduling algorithm. Others have developed computer architectures for these multiprocessor systems to increase computation efficiency [15], [16], [17]. These researchers focused on minimizing processing time by splitting-up segments of the calculations and running them on parallel processors.

Another technique to parallel processing was to assign different tasks to each processor. Kriegman and Siegel [18] developed a control system for a four-digit Utah-MIT hand shown in Figure 2-1, which was composed of five microprocessors, one for each of the four fingers plus one processor to manage all of the tasks. All processors had access to a priority-based multi-bus, where all processes in the system had equal priority to ensure fair distribution of resources. They also shared dual-ported RAM, using in high-speed Direct Memory Access (DMA) operations on a VAX system. A servo loop scheduler was used to manage processes according to the rate of their servo loops. Higher priority was given to faster servo loops interrupting any slower loops that may have been running, which had lower priority. For the most part, the fingers were controlled independently and in parallel, since they were on separate processors, but the managing processor coordinated the fingers to achieve the desired position in Cartesian space. Inter-processor communication was accomplished with message passing system that sent standard formatted messages to each processor's mailboxes.



Figure 2-1: Block Diagram of Kriegman and Siegel hand control system [18]

General computer architectures have also been developed to for real-time control. Zheng and Chen [19] developed a simple, flexible, and modular software structure to manage any multilink systems. After the user decomposed their multilink system into tasks, they were required to schedule them on separate processors. Each processor contained a hierarchial executive structure, created by Zheng and Chen, which took care of task scheduling, interprocess communication and multilevel functions. Parallel computation of applied torques was also implemented on a separate processor to provide dynamic control. Other examples of computer architectures for control structures are the CHIMERA [20] and CONDOR [21].

### 2.1.2Single-Processor Host and DSP Control Systems

All research previously discussed used distributive systems to attain the computational power required for real-time systems. Single-processors prior to the 1990s were still too slow compared to the PCs found today. Instead of having four or five microprocessors to do computations, researchers have found that using a single-processor computer with a DSP board to be good enough to do the job. This system is referred to as the Host/DSP system. The host computer is often used to monitor analyze and collect data from the control system, while the servo control itself is done on the DSP board using built-in and customized library functions to achieve real-time tasks. Having the DSP board perform all of the real-time tasks minimizes the overhead in controller computation, and using multiple DSP boards can allow for concurrent processing. Erol and Altintas [22] developed an Open

Real-Time Operating System (ORTS) based on the OSACA system created by Pritschow [23], which handled and scheduled tasks running on multiple DSP boards in a single Windows NT computer. Erol and Altintas applied the ORTS for position and force control of a CNC Machine tool.

Disadvantages of Host/DSP architecture are high cost, complex software, and the amount of indepth knowledge required to interface all of the hardware components together. Research by Costescu and Loffler [24] showed that there are various advantages to using a single processor-single host PC for robotic control over Host/DSP systems. The advantages include a decrease in cost, less hardware, higher flexibility, and better reliability and stability. For these reasons, single-processor PC-based controllers have recently become highly desirable.

Attempts to create effective real-time controllers for large systems with a single process have been proven infeasible and inflexible, since such systems require multiple concurrent processes in order to be efficient. As control systems increase in size, their complexity increases exponentially [25]. Single processor, PC-based controllers require a stable task-scheduling system to manage concurrent processes, such as a Real-Time Operating System (RTOS).

### 2.2 Object-Oriented Software Design in Robotic Controllers

Software engineering has two main types of architectures: structured programming and objectoriented (OO) programming. Structured programming breaks down a program into its functions or behaviors as a top-down approach. These programs are simple to design, however they can be difficult to alter and adapt to new systems. OO design is based on the idea of creating modules of code, or classes, with generalized functions. This code is then encapsulated so that if one module changes, the other ones are not affected. Object-oriented software is more difficult to design because it requires a lot of pre-planning. However, it allows users to modify the code easily as well as reuse existing for code to minimize development time of new modules. Initially, it was believed that object-oriented design would cause too much overhead, which is detrimental in real-time control applications. However, the overhead is negligible [26] and object-oriented control software has been successfully used in many robotic control applications.

In 1990, Miller and Lennox [27] were one of the first to investigate the use of object-oriented software design for a robotic controller. They built the "Robot Independent Programming

Environment" (RIPE), a modular software environment that allowed for the quick implementation of robot systems without dealing with the costly low-level debugging common in structured software development. The environment itself had four layers: 1) task-level programming, 2) supervisory control, 3) real-time control and 4) device drivers. The first layer was for planning and simulation. The second layer was implemented in object-oriented programming based on the physical objects found in a work cell. It was written in C++ programming language on UNIX operating system. Using a common general-purpose programming language gave it high portability, and made the code easier to modify. The third layer dealt with real-time control of devices using a VME-based 68000 family processor running VxWorks, which is compatible with UNIX. The fourth layer contained device drivers.

OO design has been used for various aspects of robotic controllers. Bagchi and Kawamura used an object-oriented framework for client and server communication within their distributed robotic system, ISAC (Intelligenet SoftArm Control) [28]. Barcio and Ramaswamy developed on OO reactive robotic system built on event-driven state transitions [29]. Robotic control frameworks have also been created Fernandez and Gonzalez (NEXUS) [30] and Traub and Schraft [31] by applying OO design.

The most significant research into PC-based robotic controllers relevant to this project was done by Costescu and Dawson [32] with their development of the QRobot, later renamed QMotor. Unlike traditional PC-based controllers, QMotor system did not use a DSP for real-time control of hardware devices, instead all control was accomplished from the PC through the use of a real-time operating system called QNX Neutrino 4.0. QMotor was composed of four concurrent processes, as shown in Figure 2-2. QS is the server process used to monitor the MultiQ board used for input/output in the system. QC is the client process of QS, which contains all of the software that perform control on the system. QN and QG are additional processes for network communication and the graphical user interface (GUI) with real-time plots, respectively. Matlab was used to analyze the data from the GUI. QG could be run on the same PC as the controller, or connect to it through a network or on a remote workstation. All these processes were designed using structured programming.

In 2000, Loffler, Chitrakaran and Dawson [33] improved on the QMotor 2.0 to develop an objectoriented QMotor Robotic Toolkit (RTK), now running with QNX Neutrino 6.0. As seen in Figure 2-3, the controller design was based on three sets of classes: Core Classes, Generic Robot Classes and Specific Robot Classes. These classes built the infrastructure to the controller, including the QMotor Toolkit, which contained the actual control loop functions. Using an object-oriented design for the controller allows for easy code maintenance, and greatly flexibility. The QMotor RTK was successfully tested on a Puma 560 robot arm and a Barret Whole Arm Manipulator (WAM) using PID control.



Figure 2-2: QMotor 2.0 Hardware/Software Architecture [33]



Figure 2-3: Class Hierarchy of QMotor Robotic Toolkit Platform [33]

### 2.3 Robot Control Structure

The problem of robotic control has been divided into two main categories, trajectory generation (or planning) and path-control (or tracking). This research focuses more on developing a solid software infrastructure of the QMARC control system, as opposed to investigating advanced techniques in trajectory generation and path control. In the current implementation, the QMARC system is capable of cubic spline trajectory generation and Proportional-Integral-Derivative (PID) control with feed-forward velocity and acceleration compensation. More advanced trajectory generation and control methods can easily be added in the future, as required.

### 2.3.1Trajectory Generation

A large part of effective motion control for a robotic manipulator is the technique in which the command path is computed. Obviously, the shortest distance between two points in space is the straight-line distance, however, generating straight-line positional distance between several knots on the same path will cause discontinuities in the manipulator velocity and acceleration. These discontinuities translate to physical vibrations or jerk on the motors. For pick-and-place operations, although minimal vibration is tolerable, the overall motion of the manipulator should be as smooth as possible.

One of the earliest forms of robotic trajectory generation was developed by Richard Paul in 1979 [34], whereby straight-line segments with smoothed out transitions at controlled accelerations were used to connect path knots defined in Cartesian coordinate systems. If two time segments each required a different constant velocity, then before ending the first time segment a change of velocity was applied for a time interval of  $\tau$ . This constant acceleration was then maintained for an additional  $\tau$  length of time into the second time segment, hence giving a smooth transition of  $2\tau$  between the two desired velocities. With this trajectory generation method, the path did not actually pass any of the path knots, except for the end knot. The path, however, could be forced to go through all knots without causing overshoot at "trajectory extremums" if the velocity at extremums were forced to zero-velocity. Because all knots were defined in Cartesian space, manipulator link equations were used to calculate intermediate joint angles to achieve the goal. Taylor [35] improved upon Paul's Cartesian technique by developing a method that required the calculation of less intermediate points, however the computational time of each knot increased. Thus, he proposed a second interpolation method implemented in joint space, whereby joint space trajectories were preplanned offline prior to starting the control loop. Doing this greatly decreased the amount of real-time computations required but a certain number of path knots had to be known a priori. Taylor presented a method that produced intermediate points that would guarantee that the straight-line motion stays within predefined bounds. Both Paul and Taylor used straight-line paths to facilitate compatibility with conveyor motion.

Because the path segments were not simple straight-line segments, due to the reasons stated earlier, the path needed to be optimized for minimum time. Luh and Lin [36] developed a minimum time trajectory generation method using straight-lines with arcs to blend motion between time segments. The length of these arcs had to be minimized so that the path did not deviate too far from the desired trajectory. To perform this optimization, Luh and Lin applied two approaches: a "method of approximate programming" (MAP), and a "direct approximate programming algorithm" (DAPA). Doing optimization, in general, requires more computing time. It was found the DAPA converged and required less computing time than their modified version of MAP.

An alternative to using straight line segments to connect path knots, is to use piece-wise low-order polynomials. Paul [37] and Finkel [38] proposed trajectory generation using cubic splines. Cubic splines provided smooth trajectories through path knots despite physical constraints on velocity and acceleration. To maximize the lifespan of the manipulator, jerk (the rate of change in acceleration) was also minimized. Lin *et al.* [39] used the piece-wise cubic polynomial to interpolate joint

trajectories as well. However, to ensure velocity and acceleration continuity, they added two extra knots to the trajectory that could be freely specified, giving the path enough degrees of freedom for continuity. To minimize the total travel time of the path, the Nelder and Mead's flexible polyhedron search was utilized. All of these earlier methods, only considered the kinematic model of the manipulator. Dynamic models were later incorporated by Bobrow *et al.* [40] for more realistic robotic control.

Trajectory generation and its optimization for both online and offline planning has been a thoroughly research topic area. Numerous types of splines have been investigated for trajectory generation, Lin and Chang [41] used X-splines and quartic splines, Dubowsky *et al.* [42] used the Bezier, and Bobrow [43] used B-splines, with varying optimization techniques.

#### 2.3.2PID Control Algorithm

Many advanced control algorithms have been developed for robotic control. Classic control methods include PID feedback control, computed torque method, feed-forward and state-space control. In the past two decades, growing interest in fuzzy controllers, neural networks and adaptable control methods has sparked many journal articles on the topic. However, PID controllers have dominated the control industry of sixty years with more than 95% process control applications [44], and most of industrial robotic control. PID control stability in rigid robotic arms has been proven by Rocco [45], based on a robotic model with decoupled linear and nonlinear uncertain components, used for independent joint control.

The dynamic model of an N degree-of-freedom robotic manipulator is given by a set of Lagrange equations in the form of:

$$M(q)\ddot{q} + C(q,\dot{q})\dot{q} + g(q) = \tau$$
(2-1)

Where, q is the motor joint angle, M(q) is the inertia matrix of the manipulator,  $C(q, \dot{q})$  is the Coriolis, centrifugal and damping terms, g(q) is the gravitational terms, and  $\tau$  is a vector of driving torques acting on the links, which are supplied by motors.

For classic PID control, all motors are treated as decoupled closed loop control systems. The torque of each individual motor,  $\tau_m$ , can be calculated as:

$$\tau_m = K_P e_m + K_I \int e_m dt + K_D \dot{e}_m \tag{2-2}$$

Where,  $e_m$  is the position error of the motor, and  $K_P$ ,  $K_I$ , and  $K_D$  represents the proportional, integral and derivative gains of the controller, respectively. Integration and derivation of  $e_m$  are calculated with respect to time, t [45].

The original method of tuning PID controllers was suggested by Ziegler and Nichols in 1942 [46], whereby an open loop step response was used to calculate the gains. Ziegler and Nichols presented a frequency response method and a step response method. Their methods were based on simulating a large number of different processes and correlating the data to suitable controller gains. The Ziegler-Nichols tuning method of a PID controller can be summarized as follows [47]:

- 1. Apply a step input to the system.
- 2. Increase the proportional gain until sustained oscillations occur, while keeping integral and derivative gains at zero.
- 3. When oscillations appear, record the proportional gain value as  $k_U$  and the period of the oscillations as  $t_U$ .

- 4. Three values,  $k_c$ ,  $T_i$  and  $T_d$ , are then computed from the following ratios:
  - Proportional Gain,  $k_c = 0.6 k_U$ Integral Time,  $T_i = 0.5 t_U$  (2-3) Derivative Time,  $T_d = 0.125 t_U$
- 5. Manually fine-tune the gains by trial-and-error to achieve controller design objective.

Ziegler-Nichols tuning formulas presented in Equation 2-3 are usually implemented in a slightly different form of the classic PID controller (Equation 2-2). PID implementation for Ziegler-Nichols is:

$$u_c = k_c \left( e + \frac{1}{T_i} \int e dt + T_d \frac{dy_f}{dt} \right)$$
(2-4)

$$e = y_r - y \tag{2-5}$$

$$y_f = \frac{1}{1 + sT_d / N} y$$
(2-6)

where,  $u_c$  is the control loop output, y is the process output, and  $y_r$  is the process command signal.

Although the Ziegler-Nichols tuning method has been very influential, the controller based on Equation 2-3 provided a closed loop control system with poor robustness [48]. Many researchers have developed methods to improve Ziegler-Nichols tuning. Cohen and Coon used normalized dead-time to improve controller tuning [49] and Astrom and Hagglund developed a step-response tuning method based on robust loop-shaping [50].

The time-consuming task of manually tuning the PID controller has also inspired a multitude papers regarding adaptive and auto-tuning PID controllers such as using pattern recognition [51], artificial intelligence [52], and fuzzy logic [53].

### Chapter 3

### Design and Implementation

### 3.1 Overview

The focus of this research was to build a reliable real-time PC-based Multi-Axis Robotic Controller (QMARC) using QNX operating system for motion control of the Deltabot. QNX is a real-time operating system, which allows programmers to create efficient multi-process applications. It is a fundamental tool to the development of the QMARC. The software was designed such that it would be modular, could easily adapted and would be easy to understand. A modular structure gives the software the flexibility to be modified to work with new hardware and new features. The overall structure of the QMARC, as shown in Figure 3-1, has five main software modules, the graphical user interface (GUI), the controller, the hardware driver, trajectory generator and safety protocols. Controller settings and initialization is done through the GUI, providing users with a comprehensive interface to run the controller. The controller itself has access to the trajectory generator, hardware driver and safety protocols, but only the controller and safety protocols have direct access to the hardware drivers, which are utilized to control the functionality of the interface card. This card provides counters to track the encoder position of the motors, analog output lines used to control the velocity of the DC motors, and digital output lines used to enable the motors through the analog amplifiers. Six digital input lines are also utilized on the card to interface with the limit switches on the manipulator. The control loop input is the encoder position read from the counters, and the controller output is the velocity command signal sent through the analog output lines. A watchdog timer on the card can also be employed to protect the system in case of the PC crashing. Together, this structure creates a closed loop control system for position control of the Deltabot.



Figure 3-1: QMARC Control Structure

To keep the software modular, the hardware drivers are kept separate from the controller software. The controller software itself was developed using object-oriented design (OOD), in order to maximize software modularity and code reusability without sacrificing readability of the code.

Currently, the Deltabot uses the Delta Tau Programmable-Multiaxis-Controller (PMAC) for servo control. Due to rigidity in the software structure of the PMAC, it was difficult to incorporate customized control algorithms and trajectory generation techniques. In order to provide a fair comparison between the controller developed in this research to the PMAC, the controller was programmed using PMAC control and spline techniques.

### 3.2 Hardware Setup

The controller runs on a Dell Optiplex GX110 Pentium III /667MHz computer with a Sensoray 626 encoder card using a QNX Neutrino 6.0 operating system. The encoder card provides up to six 24-bit

counters for quadrature decoding, as well as 48 digital input/output channels that have edge-triggered interrupt capabilities and four analog output channels with 14-bit digital-to-analog conversion (DAC) providing an output voltage of  $\pm 10$ V. The motor enable signals, as well as the limit switches are connected to the digital input/output lines of the 626 card with 0V(off) and 5V(on) states. The RS422 protocol encoder signals from all three motors of the DeltaBot are connected to the 626's dedicated encoder input channels. The cost of a single 626 card is only \$500 US, allowing for the development of a cost effective control system around a standard personal computer.

### 3.3 Process Structure of the QMARC

The distributed software system of the controller consists of five concurrent processes, shown in the ovals in Figure 3-2. These processes are the GUI, Starter, Timer, Controller and Hardware Server. As their names suggest, the GUI is the QNX Photon Graphical User Interface. On the GUI, the user can change settings for the QMARC system, and initialize the Starter process. The purpose of the Starter process is to run (or spawn) the Controller and Hardware Server, and to establish communication with these processes. The reason that the GUI does not do this directly is because QNX Photon applications do not have the same communication channels as regular QNX programs. It is simpler for the GUI to spawn the Starter process to handle the process communication. The Timer process is a real-time interrupt that keeps track of the system clock initiated from the Controller process. The Timer sends the Controller messages at a fixed sampling rate. When the Controller receives a Timer message, it sends a message to the Hardware Server requesting information about the current position of the motor. Using the data about the motor, the Controller performs its control algorithm and sends a second message to the Hardware server providing it with the command for the motor. The Hardware Server is a separate process that manages all data to and from the encoder card as well as analog/digital inputs and outputs and safety features. This process is always waiting for the Controller to send it messages. When the Hardware Server has completed its task, it replies to the Controller, freeing it from its blocked state.



Figure 3-2: QMARC Process Communication Structure

Once the Controller runs to completion, it ends the Timer and sends a message to the Hardware Server telling it to exit. Before exiting, both the Hardware Server and the Controller sends a message to the Starter program telling it to end as well. Thus all processes exit and the user can return to the GUI process to run the controller again.

The messages sent between the processes only occur in one direction, with replies returning in the opposite direction. The Starter sends replies to the Controller and Hardware Server and the Hardware Server replies to the Controller, however the Timer does not require a reply. Using this client-server communication network prevents deadlock, which is a serious problem in multi-process systems. The Hardware Server runs at the highest priority, next is the Timer and then the Controller. Setting important processes to high priorities ensures that they execute without interruption by low-priority processes. The priority of the Hardware Server is 60, whereas the Controller and Timer are at a priority of 50. The Starter runs at the lowest priority of 30.

Using the distributed software structure with this hardware-communication setup allows for fast, efficient real-time control of the motor. Because only the Hardware server deals with direct protocols to the 626 Encoder card, the hardware is effectively decoupled from the software system. This means that changing the hardware will not affect the controller software, and just the Hardware Server needs to be updated.

#### 3.3.1QNX Message-Handling Functions

QNX has many message handling functions that can be used for ease of communication between processes. Before sending a message to a process, the structure of the message must be defined and communication connection must be established between the processes.

The message structure can vary between applications depending on the need of the client and servers. For this research, four different fields were required in the message, defined by structure called ClientMessageT, as shown in Figure 3-3. The first field is an integer, iMsgType, representing the message type, or what kind of task it wants performed by the server. The second field is fMsgData, a floating-point array containing data transferring between the client and server processes. The third field is an integer array containing initialization data used to establish communication between the client and server processes. The fourth field is an integer representing the status of the server, iStatus, used to communicate success or hardware failures. The fMsgData and iInitData arrays are defined to be the size of the maximum number of motors in the system, providing enough room to contain data for every motor in a single message. For the Deltabot, NUM\_MOTOR\_MAX is equal to three.

```
// message structure
typedef struct
{
    int iMsgType; //Message Type
    float fMsgData[NUM_MOTOR_MAX]; //Floating-Point Data
    int iInitData[NUM_MOTOR_MAX]; //Initialization Data
    int iStatus; //Status of hardware
}ClientMessageT;
```

#### Figure 3-3: Message Structure for Client-Server Communication

To establish communication between the client and server processes, the server needs to provide the client with its process id and channel id numbers. The process id number can be retrieved within any process by calling the getpid() function, and the channel id can be created by calling ChannelCreate(). With this information, the client can establish a connection to the server by calling ConnectAttach(). ConnectAttach() returns a connection id number, which is then used to send messages to the server. Sample code of how to do this is shown in Figure 3-4. Messages are sent from the client using the MsgSend() function, and is received by the server with the MsgReceive() function. MsgReply() is used to send a reply message to the client after the server is finished. It is important to plan how the

server process id and channel id will be sent to client processes, so that they can establish communication to the server.

```
#define MT ENABLE MOTORS
                           30
                                 //Message Type
#define NO_ERR
                            0
ClientMessageT outmsg, replymsg, inmsg;
/* In server process */
Process_id = getpid();
                                       //Get process id
Channel_id = ChannelCreate(0); //Create a communication channel
//Server loops infinitely processing messages
while (1)
ł
    //get the message and print it
    rcvid = MsgReceive (chid, &inMsg, sizeof (ClientMessageT), NULL);
    //perform function to enable motors
    //Reply to client when completed
    outMsg.iStatus = NO_ERR;
    MsgReply (rcvid, EOK, &outMsg, sizeof (ClientMessageT));
}
.
/* In client process*/
connection_id = ConnectAttach (0, process_id, channel_id, 0, 0);
outmsg.iMsgType = MT_ENABLE_MOTORS;
                        outmsg, sizeof(ClientMessageT), replymsg,
MsqSend(connection id,
      sizeof(ClientMessageT));
```

#### Figure 3-4: Example code for client-server communication and message-handling

After the client process calls MsgSend(), the client process will stop running (or be in *blocked* state) until the it receives a reply message from the server call to MsgReply(). On the server side, the server is blocked until it receives a message from the client with MsgReceive(). When a process is in a blocked state, other processes are allowed to run. By setting the client and server to high priorities, it can be ensured that they can continue to run again as soon as they are unblocked. For the QMARC, all message types are defined in the MsgType.h header file located in the Include folder of the main directory of the QMARC system.
# 3.4 Design of the Controller Console

Programming a Graphical User Interface (GUI) on the QNX operating system is very similar to Microsoft Visual C++ development. Using the QNX Momentics Software Development suite, GUIs can be creating with predefined widgets, such as buttons, integer edit boxes, floating point edit boxes, combo boxes, and labels available in the Photon Application Builder. Photon operates on the principle that any event caused by moving or clicking the GUI, will send a message to the main Photon message loop. It is up to the programmer to write specific functions to handle desired events. For example, when a button is clicked on by the mouse an "arm" message is created. By writing a callback function for the "arm" message, the programmer can specify what actions are taken when the button is clicked. Because Photon has special messages that it uses to process actions on the GUI, regular QNX message-handling described in section 3.3.1 can not be done. Instead, special Photon message channels must be setup to establish communication. In the QMARC system, the GUI will be referred to as Controller Console and its purpose is to initialize the controller. Since the Controller Console is not updated by information from other processes, it was not necessary to setup Photon communication channels. Instead, the GUI spawns Starter, a QNX process that handles all of the communication for it.

The layout of the Controller Console is shown in Figure 3-5, depicts the five main sections of the GUI. The first section is "Controller General Settings", which allows user to set the number of motors to be controlled, the servo loop period and the home position measured from the top limit switch in counts. The servo loop period is restricted to periods of at least 300µs and must be an even multiple of 100. The second section has the "Trajectory Generation" settings. This section allows the user to select the method of trajectory generation to use and select the file location where the path knots are stored. The third section is the "Step Motor" settings. When tuning the PID controller, a step input is generally used. The size (in counts) and duration (in seconds) for the step input can be specified from the GUI. To run the step, the user must click on the "Step Motor Now" button. Note, that doing this will step <u>all</u> motors specified in the first section of the PID controller with feed-forward velocity and acceleration compensation and notch filter for the number of motors specified. Although there are entries for four motors, the maximum number of motors allowable on the Deltabot is currently three. The edit boxes for motor gains, which are not being used will be disabled on the GUI whenever the user updates the "Number of motors" edit box. The sixth section is "Data Gather"

Settings". Here, the user can specify the frequency to collect data, the file location to log the data, and what fields to collect. The frequency of gather data is a function of the servo loop, it can be set to gather data every servo loop, every other servo loop etc. There are four different fields that can be collected: time of the sample, DAC output to the motors, the command position and the actual position of the motor, measured in counts. The data is output in a Matlab data file and should have a ".m" extension. Writing the data to a Matlab file allows the user to graph to data more easily on a computer with a Microsoft Windows platform. Currently, graphing features are not used on the QNX computer.

All controller settings on the Controller Console, except for the "Step Motor" settings are saved to a *settings.txt* file, located in the directory of the Console program, before exiting the program. Whenever the GUI is started, the controller settings are retrieved from the file and loaded onto the GUI.

After the controller settings are entered, the user can click on the "Home Robot" button to run the homing sequence of the robot, or click on the "Start Controller" button to run the robot with the trajectory generator specified. The "Cancel" button is closes the GUI without saving changes to the settings file, whereas the "Exit" button will save the settings before exiting. Whenever the "Step Motor Now" button, "Home Robot" button or "Start Controller" button is clicked on, the data from the GUI is saved to the settings file, and the Starter process is spawn from the GUI. To determine which button was pressed, the GUI sends a message type flag to the Starter process. This information is then passed along to the Controller process so that it can start up in the appropriate controller mode.

While tuning the controller, it is often useful to know the accumulated absolute position error of the motors. This statistical data is displayed on the same terminal where the user runs the Controller Console program. All error messages from the Hardware Server or the Controller will be displayed on this terminal as well.

University of Waterloo, 2005         QMARC is a real-time serve controller created for research and development on the DehaBot.         Controller General Settings:         Number of motors:       3         Servo Interrupt Period:       400         (microseconds)       400         Home distance from upper limit switch (counts):       110         rajectory Generation:       00         Method:       PVT (online)         Data File Source:       0ptional Notch Filter (coefficient range= -2.0 2.0)         N1       0.00       0.00       0.00         1/QMARC/RobotCtriler/PathRotated.txt       0       0       0         Step size (counts):       0.00       0.00       0.00       0.00       0.00         Step size (counts):       0.00       0.00       0.00       0.00       0.00         Duration (seconds):       0.00       0.00       0.00       0.00       0.00       0.00         Step Motor Now       Step Motor Now       Select data to output for all motors:       Command Position	QMARC	(QNX Multi-Axis R	obot Controller) Co	onsole					
Controller General Settings:       Controller Gains:         Number of motors:       3         Servo Interrupt Period:       400         (microseconds)       400         Home distance from upper limit switch (counts):       110         110       100         rajectory Generation:       0         Method:       PVT (online)         Data File Source:       0         /QMARC/RobotCtriler/PathRotated.txt          Step Motors:       0.00         Step size (counts):       0.00         Duration (seconds):       0.00         Step Motor Now      Step Motor Now  Controller Gains:  Controller Gains:  Controller Gains:  Motor 1 Motor 2 Motor 3 Motor 4 (Kp 182000 182000 183000 (Ki 100 100 100 100 (Kd 3000 3000 3000 3000 00 (Kd 3000 3000 3000 00 (Koff 109000 102500 104000 00 (Kaff 100 000 0.00 0.00 (Control 100 0.00 (Control 100 0.00 0.00 (Control 100 (Control 100 0.00 (Control 100 0.00 (Co	University of Waterloo, 2005 QMARC is a real-time servo controller created for research and development on the DeltaBot.								
Number of motors:       3       Motor 1       Motor 2       Motor 3       Motor 4         Servo Interrupt Period:       400       400       182000       182000       183000       183000         Home distance from upper limit switch (counts):       110       Ki       100       100       100         rajectory Generation:       0       0       100       100       100       100         Method:       PVT (online)       •       0       000       0.00       0.00       100         Mater Seurce:       0       •       0       0.00       0.00       0.00       0.00         /QMARC/RobotCtriller/PathRotated.txt        0       0.00       0.00       0.00       0.00         Step size (counts):        0       •       0       0.00       0.00       0.00         Duration (seconds):       0.00       •       •       Select data to output for all motors:       Select data to output for all motors:       X	Controller General Settings:	Contr	oller Gains:						
Number of motors:       3       Kp       182000       183000       Image: Serve interrupt Period:       400       Ki       100       100       100       Image: Serve interrupt Period:       Ki       100       100       100       100       Ki       100       100       100       Ki       Ki       100			Motor 1	Motor 2	Motor 3	Motor 4			
Servo Interrupt Period: (microseconds)       400 ↓         Home distance from upper limit switch (counts):       110 ↓         Home distance from upper limit switch (counts):       110 ↓         rajectory Generation:       100 100 100 100         Method:       PVT (online)         Data File Source:       0ptional Notch Filter (coefficient range= -2.0 2.0)         N1       0.00       0.00         VQMARC/RobotCtriler/PathRotated.txt          Step Motors:       0.00 ↓         Duration (seconds):       0.00 ↓         Step Motor Now       0.00 ↓             Step Motor Now       0.00 ↓	Number of motors:     3       Servo Interrupt Period: (microseconds)     400       Home distance from upper limit switch (counts):     110	💌 Кр	182000	182000	183000	0			
Home distance from upper limit switch (counts):       110         Home distance from upper limit switch (counts):       110         Frajectory Generation:       Kvff         Optional Notch Filter (coefficient range= -2.0 2.0)         Method:       PVT (online)         Data File Source:       Optional Notch Filter (coefficient range= -2.0 2.0)         N1       0.00       0.00       0.00         /QMARC/RobotCtrller/PathRotated.txt        Data Gather Settings:         Step size (counts):       0        Output data file path and name (*.m):         Duration (seconds):       0.00        Select data to output for all motors:         Step Motor Now       Select data to output for all motors:       X Actual Time       X command Position		кі	100	100	100	0			
Home distance from upper limit switch (counts):       110         Imit switch (counts):       110         Kvff       109000       102500       104000         Frajectory Generation:       0ptional Notch Filter (coefficient range= -2.0 2.0)       N1       0.00       0.00       0.00         Method:       PVT (online)       •       0ptional Notch Filter (coefficient range= -2.0 2.0)       N1       0.00       0.00       0.00       0.00         Data File Source:       /QMARC/RobotCtriler/PathRotated.txt        0       0.00       0.00       0.00       0.00         Step Motors:       0       0       0       0.00       0.00       0.00       0.00         Duration (seconds):       0.00       0.00       0.00       0.00       0.00       0.00       0.00         Step Motor Now       Step Motor Now       Select data to output for all motors:       Select data to output for all motors:       Select data to output for all motors:       Scommand Position		Kd	3000	3000	3000	65			
rajectory Generation:   Method:   PVT (online)   Oata File Source:   /QMARC/RobotCtriler/PathRotated.txt   /QMARC/RobotCtriler/PathRotated.txt   Step size (counts):   Duration (seconds):   0.00   Step Motor Now     Kaff   100   100   100   0.00		Kvff	109000	102500	104000	0			
Image: Comparison of the second se		Kaff	100	100	100	0			
Step Motors:     Data Gather Settings:       Step size (counts):     0 •       Duration (seconds):     0.00 •       Step Motor Now     Select data to output for all motors:       Step Motor Now     Actual Time	Data File Source: /QMARC/RobotCtrller/PathRotated.txt	N2 D1 D2	0.00	0.00	0.00	0.00 0.00 0.80			
Step size (counts): 0 •   Duration (seconds): 0.00 •     Step Motor Now Select data to output for all motors:     Step Motor Now \vee Actual Time     Duration (December 2)	tep Motors:	Data	Gather Setting	s:					
	Step size (counts): 0 Duration (seconds): 0.00 Step Motor Now	Gat	her data every: tput data file pat MARC/RobotCtrlle lect data to outpu I Actual Time DAC Output	4	servo cycle(s) :.m): 's: IX Comman IX Actual Po	)  d Position Isition			
Home Bobot Start Controller CANCEL E	Hom	e Rohot	Start C	ontroller					

Figure 3-5: QMARC Photon Graphical User Interface (GUI)

# 3.5 Design of the Starter Process

The purpose of the Starter program is to be a gateway between the Controller Console and the Controller and Hardware Server processes. As mentioned in section 3.4, the Controller Console does not use the same message channels as the QNX processes, making communication more difficult. However, since the console does not need to be updated by any other process, the GUI only needs to do one-way communication. As shown in Figure 3-6, when a button (other than the Exit button) is pressed on the console, the Starter process is spawned from the GUI passing along information about

which button was pressed, using the spawnl() function. The Starter program reads these values in as string arguments and converts them to integer or floating-point values. Starter than spawns the Hardware Server and Controller processes using spawnl() passing them its channel id number. Starter's channel id is used by the Hardware Server and the Controller to connect it. The connection allows the Starter to know if the spawnl() was successful. When Hardware Server is spawn it sends a message to the Starter to inform it that the spawnl() call was successful, and it also sends back its own Process ID and Channel ID numbers. These ID numbers are then passed on the Controller process by the Starter, so that the Controller can establish direct communication with the Hardware Server. If the "Step Motor Now" button was pressed on the GUI, then the step size and duration are passed to the Starter program as arguments in spawnl() and passed to the Controller process in the reply message. Starter then waits for a message from the Hardware Server and the Controller indicating that it is done. Once it receives messages from both processes, the Starter program exits. Keeping the Starter process running ensures that any error messages from the child processes will be displayed on the terminal window. If the Starter process exits immediately after spawning the processes, the error messages and statistical data will be lost, unless it is output to file.



**Figure 3-6: Flow Chart of Starter Process** 

# 3.6 Design of the Hardware Server

The Hardware Server is a process initialized from the Starter process, and terminated by a message from the Controller process. This server receives messages regarding input and output to the Sensoray 626 Encoder card. It performs all hardware input and output, and monitors limit switches using an edge-triggered interrupt line built into the interface card. The Hardware Server runs in a semi-infinite loop blocked by the operating system on a MsgReceive() command until it receives a message from the Controller. When a message is received, the Hardware Server unblocks, determines the type of message that was sent to it using the integer field, iMsgType, in the message and then performs the appropriate actions. After the action is completed, the Hardware Server sends a reply message back to the Controller along with the status of its actions, and then continues back to the beginning of the message loop. The server handles twelve different messages:

- 1. Retrieve the encoder counter values for all motors.
- 2. Send DAC output for all motors.
- 3. Retrieve the encoder counter value for a single, specified motor.
- 4. Send DAC output for a single, specified motor.
- 5. Enable a single, specified motor.
- 6. Disable a single, specified motor
- 7. Disable all motors
- 8. Reset encoder counter to "zero" value.
- 9. Enable interrupts to monitor hardware safety features.
- 10. Disable interrupts to monitor hardware safety features.
- 11. Clear safety status flag.
- 12. Exit Hardware Server

A safety status flag is used to monitor the errors in the Hardware Server. If the limit switches are tripped, encoder overflow occurs, or an unrecognized message is detected, the status flag is set and sent back to the Controller in the reply message. Messages are processed in order of time-critical importance. Messages related to retrieving encoder positions and sending DAC output is checked first in the message loop because they are used in a real-time control loop by the Controller. Single motor functions are kept separate from functions that apply to all motors. Single motor functions are used in homing procedures. Functions concerning all motors are used for time-critical

control loops, since sending a single message for each motor can be time consuming. All data passed in the messages are stored in the fMsgData array contained in the message structure.

The Hardware Server was written specifically for the Sensoray 626 encoder card using the Sensoray QNX library. Hardware protocols are kept separate from the Controller so that the Controller is decoupled from the equipment used in the application. This means that if new hardware is purchased, only the Hardware Server will have to be rewritten, saving both time and money.

When the Hardware Server is initially started from the Controller Console, it connects to the Starter and sends it a message with its process id and channel id number. Through the Starter, the process id and channel id of the Hardware Server is passed to the Controller. As shown in Figure 3-7, the Hardware Server then runs in a semi-infinite loop processing messages received from the Controller and performing calls to the Sensoray QNX library. When the server receives an exit message from the Controller indicating that the Controller is complete, the Hardware Server sends a "Done" message to the Starter program and then exits. Safety protocols and homing procedures will be covered in section 3.10.



Figure 3-7: Flow-chart for Hardware Server

# 3.7 Design of the Timer

The Timer consists of a software interrupt handler, using the timer interrupt number 0 built into QNX Neutrino 6.0. The period of the timer interrupt is determined by calling ClockPeriod(), a QNX function called from the setupTimer() function in the MultiAxisRobot class. A global timer event variable, timevent, is attached to the timer interrupt and then linked to an interrupt service routine (ISR), as shown in Figure 3-8. For the QMARC, the interrupt handler is set for a period of 100 µs. In the ISR, a global variable is used to keep track of the number of times the timer interrupt has occurred. This variable, timetr, must be declared as *volatile*. When the counter equals the servo interrupt time of the servo loop, then the ISR returns the timer event, so that the Controller process unblocks the InterruptWait() command in the servo loop.

```
struct sigevent timevent;
                                               //Timer Event
volatile unsigned timctr;
                                               //Timer for counter
//ISR - Interrupt Service Routine
//Handles the timer ClockPeriod() interrupts
const struct sigevent *handler(void *area, int id)
ł
    //Clock runs by period set by ClockPeriod()
    if(++timctr == iServoIntRnd)
    {
          timctr=0;
          return(&timevent);
    }
    else
          return(NULL);
}
//Set the timer interrupt according to ClockPeriod(), interrupt 0
int MultiaxisRobot::setupTimer(void)
ł
    struct clockperiod clkper;
    //Set the Clock Period to minimum value of 100 microseconds
    clkper.nsec = 100000;
    clkper.fract = 0;
    ClockPeriod(CLOCK_REALTIME,&clkper,NULL,0);
    ThreadCtl(_NTO_TCTL_IO,0);
                                        //Request I/O privity
    timevent.sigev_notify=SIGEV_INTR; //Initialize event structure
    //Attach ISR vector, interrupt 0 is clock interrupt
    timid=InterruptAttach(SYSPAGE_ENTRY(qtime)->intr,&handler,NULL,0,0);
    return 0;
}
```

#### Figure 3-8: Code for Timer ISR and Setup Procedure

# 3.8 Design of the Controller

The Controller is the heart of the QMARC system. It consists of the control algorithm, trajectory generation, safety procedures, timing and hardware message handling in closed control-loop. Objectives of the Controller design were to create a general software structure that had high flexibility, expandability, and was easy to follow, update and understand. High flexibility allows for expansions in the software such as applying different control algorithms and trajectory generation techniques. Hardware changes such as the incorporation of a vision system and different end-effectors, motor drives and manipulators should also be possible with minimal change to the existing software. To build a flexible system, the software structure needs to be modular. A modular program keeps segments of code encapsulated, such that a change in one component of the software will not adversely affect other areas. In software engineering, a technique called Object-Oriented design is used to achieve this goal [10].

The object-oriented structure used for this project was developed based on research by Loffler et al. [33]. As shown in Figure 3-9, the controller was organized into Base Classes and Specific Subclasses. The Base Classes are modules providing general functions and properties commonly found in a robotic motion controller. Five base classes were created for this motion controller: CObject, CManipulator, CGripper, CTrajGenerator, and CServoCtrl. All Base Classes are preceded with a "C" to distinguish them for Specific Subclasses.

The Base Classes are divided into two groups: physical classes and functional classes. Physical classes are based on physical hardware used in the motion controller, whereas functional classes deal with the mathematical aspects of the controller. On the hardware side, there is the CObject class. This class contains all properties common to any physical object, such as a universal system timer, servo loop period etc. CManipulator and CGripper are classes for manipulators and grippers, respectively, and are subclasses of CObject. Being a subclass means that it inherits all of the parent class' public properties and functions. If additional hardware is required, then new subclasses can be made from CObject. The remaining two base classes: CTrajGenerator and CServoCtrl, contain the operations and calculations required for trajectory generation and servo control, respectively. By default, the CTrajGenerator produces a constant trajectory used for Step Input. Using the five base classes defined above, Specific Subclasses can be derived that are specific to the controller application. All base classes were designed to maximize reusable code by a specific subclass.

The motion controller in this research was designed for control of the Deltabot. Key functions such as performing the control loop are defined in the MultiaxisRobot class, a subclass of the CManipulator base class. The MultiaxisRobot class also contains the communication protocols to the Hardware Server and the Timer used for the control loop. The control algorithm implemented on the manipulator was PID control with Velocity and Acceleration Feed-Forward compensation, which is contained in the PIDffCtrl class derived from the CServoCtrl base class. Details on this control algorithm are covered in Section 3.11. In addition, two different methods of trajectory generation were implemented in this controller: offline cubic spline and online Position-Velocity-Time (PVT) These techniques were separated into two different classes named trajectory generation. CubSplineTrajGen and PVTOnlineTrajGen. Trajectory generation is used to determine the command position for each time instance of the servo loop. Details on these algorithms are covered in Section 3.12. In addition, it should be noted that both the control and trajectory generation algorithms were implemented from the PMAC model, to facilitate the comparisons between the two controllers. The control of the gripper was not necessary in this research; therefore CGripper does not have a specific subclass.



Figure 3-9: Class structure of robotic motion controller

#### 3.8.1.1 Detailed Base Class Descriptions

This section will cover the detailed software description of each base class: CObject, CManipulator, CGripper, CTrajGenerator and CServoCtrl. Not all base classes are fully implemented but are still presented here to demonstrate the full software infrastructure for future research development.

As a standard naming convention for all member variables, variables with an "i" prefix represents an integer data type and "f" represents a floating point number. Integers are two-byte signed values ranging from -32768 to 32767. Floating-point numbers are four bytes long and range from  $-3.4 \times 10^{-38}$  to  $3.4 \times 10^{38}$ .

Base classes: CObject, CTrajGenerator and CServoCtrl all contain a floating-point variable, fServoInt used to specific the period of the servo interrupt in seconds. This variable is defined by calling the init() function in each base class. This init() function is declared as *virtual* so that it can be overloaded by subclasses if necessary.

#### 3.8.1.1.1 CObject Class Description

The CObject class contains a member variable for the servo interrupt period, fServoInt. It also contains the init() function that sets this variable and converts it from microseconds to seconds.

#### 3.8.1.1.2 CManipulator Class Description

The CManipulator Class has three member variables: iNumMotors, iHome and fCurPos, which represents the number of motors in the manipulator, the home position of each motor measured in counts and the current position of each motor in counts.

Virtual functions are also defined for the control loop (ctrlLoop()) and to setup the timer (setTimer()). These functions are implemented in the subclass level. Only empty functions are provided here to ensure the polymorphism can be applied to future subclasses of CManipulator.

#### 3.8.1.1.3 CGripper Class Description

The CGripper class currently does not contain any member variables or function. It is added as a demonstration of how the CObject class can be used and is reserved for future research development.

#### 3.8.1.1.4 CTrajGenerator Class Description

Command positions are created for servo control via trajectory generation. CTrajGenerator class contains four member variables: fServoInt represents the servo interrupt period, fPosQueue represents a pointer to the position queue, iPosCurPtr indicates the index of the current position to read command values, and iPosQueueCtr gives the total size of the queue. All of these variables are used for the collection of command positions at each time instance of the servo control. For offline trajectory generation, these position values are calculated prior to starting the control loop. The size of the position queue is dynamically allocated in real-time based on the total time length of the manipulator motion, as well as the desired servo control clock frequency. Dynamic memory

allocation is performed by calling member function setPosQueue(), giving it the size of the desired queue. Queue size is calculated using the following equation:

Position queue size = (total time of move / servo interrupt period) + 1

Member function getCurPosQueue() is used to retrieve the current command position from the position queue.

In CTrajGenerator there are two sets of virtual member functions for: online and offline trajectory generation. Online trajectory generation requires separate functions for interpolating between two knots (interpPoint()), calculation path segment coefficients (calcCoeff()) and to retrieve real-time data (readData()). Offline trajectory generation combines all computations in one simple function called to calcPath(). All of these functions are redefined at the subclass level. The default trajectory implemented in calcPath() is an ideal step input, with a step size and duration defined by the user in the Controller Console.

#### 3.8.1.1.5 CServoCtrl Class Description

The control algorithm for the motion controller is contained in the CServoCtrl base class. CServoCtrl contains one member variable for the new DAC output, fDACOut, and two member functions to set the gains of the controller (setGain()) and the control computation itself called ctrlCalc(). Both setGain() and ctrlCalc() are empty in this base class and are reserved for implementation in its subclasses.

# 3.8.1.2 Detailed Specific Subclass Descriptions

The Specific Subclasses are written for a specific application of the QMARC. All subclasses are derived from one of the five base classes described in Section 3.8.1.1. For motion control, four specific subclasses are used: MultiaxisRobot, CubSplineTrajGen, PVTTrajGen and PIDffCtrl. Variable data type naming conventions are identical to those described for the Base Classes.

#### 3.8.1.2.1 MultiaxisRobot Class Description

The MultiaxisRobot Class is derived from the CManipulator base class, and is primarily used for the communication to the Hardware Server, to initialize and monitor the Timer of the controller, perform the control loop, and handle safety protocols involved with hardware and software faults.

There are two member variables in this class used for communication: the connection ID (iCoid), is used to communicate to the Hardware Server, and iTimid holds the process id for communication to the Timer. Functions sendServerMsg() is used to send messages to the Hardware Server, faultHandler() is used to handle fault messages received from the Hardware Server, and setupTimer() is used to initialize and setup the Timer.

The settings for gathering data are summarized in three member variables: outFilePtr is a file pointer to the output file, iDataGatherFreq gives the frequency to gather data in the servo loop, and iDataGatherFlags contains the bit flags indicating the fields to gather data from. The options for data collection during the servo loop are: time, DAC output, command position and actual position. The logged data is output to a Matlab file by calling the outputDataFile() member function.

In order to read knots that define the desired manipulator path, two variables are used: iCurQueuePtr representing the position of the circular queue with knot data and bQueueEOF flag used to indicate the end of the queue. This circular queue is an array of the position-velocity-time (PVT) structure type with a length of 10, which is declared globally. It is used only for online trajectory generation in the member function readFile() of the PVTOnlineTrajGen class.

All of these member variables and functions covered thus far are private and can only be accessed within the class. Another private member function called homeCtrlLoop() is a special control loop used to home the motors.

Public member functions include initiating communication to the Hardware Server and setting the servo interrupt period in init(), ending communication in close(), setting the home position of all motors in setHomePos(), setting the "zero" encoder positions for the motors in zeroMotorPos() and the performing the control loop. Depending on the value of member variable indicating the trajectory generation mode (iTrajGenMode), ctrlLoop() is called for offline trajectory generation, whereas ctrlLoopOnlineTrajGen() is called for online trajectory generation. Both ctrlLoop() and ctrlLoopOnlineTrajGen() require pointers to CTrajGenerator and CServoCtrl objects to perform the control loop, however online trajectory generation also requires a pointer to a data file containing information on path knots. Since the control loop functions use base class pointers as inputs, they accept any subclasses of that base class as well. This is possible due to the polymorphic nature of object-oriented software design. By setting the base class pointers to the appropriate subclass, the trajectory generation and control algorithm can be altered without modifying the member function.

The calcPath() function must always be called prior to calling the ctrlLoop() function. Since ctrlLoop() assumes that the position queue for the command path has already been calculated. The algorithm used for this control loop is shown in Figure 3-10. Basically, the program determines the length of the position queue by reading the CTrajGenerator member variable iPosQueueCtr, and then

loops around waiting for an interrupt from the Timer. It then extracts the current command position using getCurPosQueue() and calculates the new DAC output by calling ctrlCalc() in CServoCtrl. Sending messages between processes take considerable time, so to minimize time in the control loop a single message is sent to the Hardware Server to retrieve <u>all</u> motor positions and to send <u>all</u> motors their new DAC output signal. All statistical data is saved to a buffer array during the motion, and is output to a Matlab file after the move is completed. The motors and safety features are automatically enabled before the move and disabled after the move is done.

The algorithm for the control loop used in online trajectory generation (ctrlLoopOnlineTrajGen()) is shown in Figure 3-11. This control loop is very similar to ctrlLoop() used in offline trajectory generation, except the total time of the move is marked by the end of the data file containing the PVT knots for trajectory generation. The readFile() function in the MultiaxisRobot class is used to read data from the PVT data file and store knots into a circular queue. The first time readFile() is called, the first three knots in the path are read, then every successive call reads two knots. This means that in order to do PVT online trajectory generation at least three points on the manipulator path must be known a priori. Instead of reading in three points, the function can be easily modified to read in only two, however this is left for future research. The PVTOnlineTrajGen class has its own readData() function used to copy knot points from the circular queue to a small array located within the class memory. After reading the initial path knot from the queue, the program enters a loop where it first reads in a point representing the end of the time segment, calculates the coefficients of the cubic spline between the two knots and then loops through waiting for the interrupt and interpolating command positions, doing control, at each time instance within that segment. When the time segment covered by the two knots is finished, the function reads another knot from the circular queue, until the end flag in the circular queue is found. This end flag signifies an end of file, which terminates the control loop and outputs data to file.



Figure 3-10: Flow-chart of algorithm for offline trajectory generation control loop, ctrlLoop()



Figure 3-11: Flow-chart of algorithm for online trajectory generation control loop, ctrlLoopOnlineTraj()

#### 3.8.1.2.2 CubSplineTrajGen Class Description

The cubic spline offline trajectory generation class CubSplineTrajGen is derived from the CTrajGenerator base class. CubSplineTrajGen has two private member functions: getAcceleration(), which calculates the acceleration of each knot so that the acceleration, velocity and position of the trajectory is continuous and interpPoint(), which interpolates the position for any point in time. InterpPoint() is declared as a virtual function in the base class CTrajGenerator, however, for offline trajectory generation overloads the operators to make the function suitable for offline computation. Both interpPoint and getAcceleration() are used by calcPath(), which is the only public member function of this class. CalcPath() calculates the cubic spline path for any set of non-uniformly spaced knots, and produces a full position queue ready for the control loop. The mathematics of this class are covered in Section 3.12.1.

#### 3.8.1.2.3 PVTOnlineTrajGen Class Description

The Position-Velocity-Time (PVT) trajectory generation class PVTOnlineTrajGen is derived from the CTrajGenerator base class. There are eight member variables in this class: iCurKnotPtr is the current position on the circular queue used by the trajectory generator, the coefficients fA, fB, fC and fD of the cubic spline polynomial equation, and arrays for two time instances of position, velocity and time in variables fP, fV, and fT. Public member functions include: a constructor used to initialize class variables, readData() used to read PVT values from circular queue, calcCoeff() uses the PVT knots to calculate the fA, fB, fC, and fD coefficients of the cubic polynomial for the current time segment, interpPoint() is used to interpolate the position within a spline segment, and saveDataInstance() used to move array values from the current time instance to previous time instance in fP, fV and fT. The mathematical details of this class are covered in Section 3.12.2.

#### 3.8.1.2.4 PIDffCtrl Class Description

The PID control with feed-forward acceleration and velocity algorithm with a notch filter is implemented in the PIDffCtrl class. This class is derived from the CServoCtrl base class and has five private member variables representing the gains of the controller, which can be set by calling the public setGain() member function. The gains are: portional gain (fPGain), integral gain (fIGain), derivative gain (fDGain), feed-forward velocity gain (fKvff), and acceleration gain (fKaff). Two private arrays are used to store the coefficients of the notch filter. Array fNcoeff stores the coefficients for the numerator and fDcoeff stores the coefficients of the denominator, covered in Section 3.11.1 of the notch filter.

In addition, this class has five member variables used to store a few time instances of intermediate variables used for the control calculation, these are: position error (ferror), integral error (fIntError), command velocity (fCmdVel), command position (fCmdPos), and actual position (fActPos). To calculate the feedrate for the motors, the controller calls the ctrlCalc() function. The init() is first called to initialize all private member variables. The mathematical details of this control algorithm are covered in Section 3.11.

# 3.9 Running the Controller

Before starting the control loop, the Controller is initialized by the Starter process, receiving the process id and channel id of the Hardware Server. The Controller then reads the *settings.txt* data file written by the Controller Console and saves the settings into the memory. It then processes the reply message type from the Starter to determine which button on the GUI was pressed. Depending on the button type, three different functions are called homeRobot(), stepMotor() or initCtrller(). These three functions call and initialize the class functions.

# 3.10 Safety Features

Applying the QMARC to a robotic manipulator required the implementation of safety measures to ensure that the robot arm and the motors of the Deltabot were not damaged if the control law became unstable. Safety protocols monitoring motor positions with limit switches, software limits of the encoder counters, and following error of the controller were developed.

#### 3.10.1 Hardware Limit Switches

The DeltaBot uses two proximity limit switches to indicate maximum and minimum angles allowed by the arms connected to each of the three motors. The QMARC uses six digital input channels to monitor the limit switches via hardware interrupts initialized from the Hardware Server. When a limit switch is tripped, the server determines which limit switch it was and sets a status flag for that motor. As a result all limit switch interrupts are temporarily disabled. When the Controller process requests information from the Hardware Server during the servo control loop, the server informs the controller process that the limit switch has been tripped using the iStatus field in the message. When the Controller receives a non-zero status flag, the Controller exits the control loop and enters the fault handler function, faultHandler() in the MultiaxisRobot class. The faultHandler() immediately disables all motors and outputs an error message to the terminal.

#### 3.10.1.1 Robot Homing Procedure

During homing, the limit switches are used to set the home position of each motor of the manipulator. This is activated by pressing the "Home Robot" button on the GUI. The homing is done through the setHomePos() function in the MultiaxisRobot class. Function setHomePos() calls the homeCtrlLoop() function, to move the robot arm at a constant velocity up to the top limit switch. When the Hardware Server finds the top limit switch, it sets the status flags and informs the Controller of the status of the limit switch at the next hardware request. The control loop will end immediately and return to the setHomePos() function in MultiAxisRobot class. The homing subroutine will move the motor down slowly. At every sampling interval it will check to see if the status of the limit switch triggered has changed, to make sure that the motor is no longer outside of its boundaries. If the motor does not clear the limit switch within 10 counts, then a fatal error could have occurred, so all motors are disabled as a safety measure. If the motor clears the limit switch within 10 counts successfully, then robot arm moves to the home distance set by the Controller Console. The motor encoder counter is set to "zero" value. The entire process is repeated for each motor one-byone.

To maintain the client-server communication hierarchy, the Hardware Server cannot send a message to the controller process directly when it knows that a limit switch has been tripped. In the worse case scenario, the limit switch would occur immediately after the client receives a response from the Hardware Server. This means that it would take one sampling interval for the appropriate actions to be taken by the Controller. For our application a delay of one servo interrupt period is tolerable.

#### 3.10.2 Software Position Limits

The counters used to measure the position of the motor encoder signals are located on the Sensoray 626 encoder card. These counters have 24-bit resolution, with a range from 0 to 16777216. At the end of the homing sequence described in section 3.10.1.1, the counters are set to "zero". This "zero" value is actually 8388608, a value in the mid-range of the counter. An addition 32-bit signed long software counter is used for every motor, which is set to zero by the zeroHomPos() function in the

MultiAxisRobot class. Every time the hardware counter is read, the Hardware Server calculates the change in the counter from the previous time instance, and adds the difference in counts to the software counter. The software counter ranges from -2,147,483,648 to 2,147,483,648. Using a a variable to store the counter value prevents the problem of counter overflow, which may occur in robot motion using a hardware counter. Any hardware counter overflow that does occur is handled by the calculation of the software counter.

#### 3.10.3 Following Error Limit

When a controller becomes unstable, the accumulated following error of the position can blow up dramatically. To ensure that controller instability does not damage the manipulator, a software limit on the integrated following error is implemented in the ctrlLoop() and ctrlLoopOnlineTraj() functions of the MultiaxisRobot class. This following error limit has been set to 200,000 counts in the MsgType.h header file, but can be easily redefined by the programmer. If a following error occurs the control loop will exit, and enter the fault handler subroutine, faultHandler(), located in the MultiaxisRobot class. The faultHandler will immediately disable all motors and output an error message to the terminal.

# 3.11Control Algorithm

Digital control in the QMARC was modeled after the control algorithm utilized by the PMAC, so that results and gains from the two controllers were comparable. PMAC uses a discrete time controller that calculates the 16-bit DAC output of the system during every servo cycle [6]. The control algorithm consists of a straightforward PID discrete time controller with feed-forward velocity and acceleration, as shown in Figure 3-12.



Figure 3-12: Schematic of PID Feed-Forward Velocity and Acceleration Control Algorithm

The control algorithm for the DAC output of the PMAC at each *n*th time instance can be expressed as the following equation:

$$DACOut(n) = 2^{-19} \cdot K_p \left( FE(n) + \frac{K_{vff} \cdot CV(n) + K_{aff} \cdot CA(n)}{128} + \frac{K_i \cdot IE(n)}{2^{23}} - \frac{K_d \cdot AV(n)}{128} \right)$$
(3-1)

Where,

Command velocity, CV(n) = command position(n) - command position(n-1)Actual velocity, AV(n) = actual position(n) - actual position(n-1)Command acceleration, CA(n) = CV(n) - CV(n-1)Following error, FE(n) = command position(n) - actual position(n)

Integrated error,  $IE(n) = \sum_{j=0}^{n-1} FE(j)$ 

Variables  $K_{p}$ ,  $K_{i}$ , and  $K_{d}$  are the proportional, integral and derivative gains of the PID controller, respectively.  $K_{vff}$  and  $K_{aff}$  are the velocity and acceleration feed-forward gains.

In the PMAC control algorithm, the following error and derivative terms are multiplied by a scaling factor of 96 because in the PMAC process, the position is converted from a 24-bit value to a 48-bit value and divided by 96. Since, the QMARC does not extend the position value in software, these scaling factors are eliminated from Equation 3-1. Additional scaling factors found in the equation are used to ensure numerical accuracy in the control calculation.

The DAC output signals from the Sensoray 626 Encoder card used for the QMARC system only have only 14-bit resolution opposed to 16-bit found on in the PMAC. Because of this difference Equation 3-1 was divided by a factor of  $2^2$  when implemented into QMARC.

General tuning of the PID gains of the controller can be done using Ziegler-Nichols method with a step input and then fine-tuned manually to minimize the accumulated squared error in position. The feed-forward gains can be tuned with a standard second-order trajectory path. This control algorithm was implemented in the PIDffCtrl class derived from the CServoCtrl base class in the software. The gains of the controller are set through the graphical user interface, and initialized in the controller using the setGain() function in the PIDffCtrl class.

#### 3.11.1 Notch Filter

A second-order notch filter shown in equation 3-2 was implemented on the QMARC to compensate for resonant frequencies in the robot manipulator. The notch filter equation is:

Notch Filter = 
$$\frac{1 + n_1 z^{-1} + n_2 z^{-2}}{1 + d_1 z^{-1} + d_2 z^{-2}}$$
 (3-2)

where  $n_1$  and  $n_2$  are the numerator coefficients and where  $d_1$  and  $d_2$  are the denominator coefficients.

Due to the light-weight design of the DeltaBot, the resonant frequency of the robot is not apparent, and the notch filter is not required for its control. However, the notch filter can be used in future control applications.

# 3.12 Trajectory Generation

Trajectory generation in QMARC can be accomplished through online or offline computation. Offline computation has the advantage of ensuring ( $C^2$ ) acceleration continuity, and allows the control loop to run at a slightly faster rate. However, offline trajectory generation requires exact knowledge of the manipulator path prior to starting the control loop. Online trajectory generation requires the user to specify path knots in a data file. These points can be generated in real-time allowing the manipulator higher flexibility in movement for obstacle avoidance. Online computations and reading the input data file adds computation time in each servo loop, however it can still be done without slowing down the servo cycle rate of 2.5 kHz. Currently, both online and offline trajectory generation does not guarantee acceleration continuity, which would be dependent on the criterion used to calculate the position, velocity and time points for each knot. Both trajectory generation methods calculates the path using absolute position reference, opposed to relative positions.

#### 3.12.1 Offline Cubic Spline Trajectory Generation

The CubSplineTrajGen class provides smooth offline trajectory generation for an *N* number of knots in a predefined path. For position control of a DC motor, the program requires a data file containing the position of the motor at different time instances as input. Using a natural cubic spline interpolation method by Press *et al.* [54], the full path of the motor is determined at discrete time instances corresponding to the sampling frequency. The knots can have regular or irregular time intervals.

For QMARC, the interpolation is done for time (t) vs. motor position (y). Interpolation of the knots is accomplished in two steps, first the second derivative of each knot is determined, and then the joint position for each time instance, in between the knots, is calculated by evaluating the cubic spline. The cubic spline equation takes the form of:

$$y = Ay_{j} + By_{j+1} + Cy_{j}'' + Dy_{j+1}''$$
(3-3)

where,

$$A \equiv \frac{t_{j+1} - t_j}{t_{j+1} - t_j}, \ B \equiv \frac{t - t_j}{t_{j+1} - t_j},$$
(3-4)

$$C \equiv \frac{1}{6} (A^3 - A)(t_{j+1} - t_j)^2, \qquad (3-5)$$

$$D = \frac{1}{6} (B^3 - B) (t_{j+1} - t_j)^2$$
(3-6)

In order to ensure that the second derivative of the equation above is also continuous for the first derivative, we evaluate the first derivative of Equation 3-3, y', for  $t=t_j$  in the interval of  $(t_{j-1}, t_j)$  and set it equal y' for  $t=t_j$  in the interval of  $(t_j, t_{j+1})$ . This produces the following equation, for j=2,... *N-1*:

$$\frac{t_{j}-t_{j-1}}{6}y_{j-1}'' + \frac{t_{j+1}-t_{j-1}}{3}y_{j}'' + \frac{t_{j+1}-t_{j}}{6}y_{j+1}'' = \frac{y_{j+1}-y_{j}}{t_{j+1}-t_{j}} - \frac{y_{j}-y_{j-1}}{t_{j}-t_{j-1}}$$
(3-7)

There will be N-2 linear equations for N unknown y'' values. The remaining two equations are developed by setting the boundary conditions of y'' at the two end knots of the path to zero. Doing this will obtain a "natural" spline. Press *et al.* takes advantage of the *tridiagonal* property of this set of equations to solve this system numerically. A tridiagonal is a "special case of a system of linear

equations ... that has nonzero elements only on the diagonal plus or minus one column" [54]. Systems with this characteristic can be solved using LU decomposition, forward and backwards substitution in the order of N operations.

After calculating the y'' for each knot in the getAcceleration() function, the calcPath() function calls the interpPoint() method that using a bisection search to find the appropriate time segment of the spline and uses the appropriate y'' values to solve Equation 3-3 for the command position of any given time instance. All command positions generated are stored in an array of values, fPosQueue. The ctrlLoop() function in MultiaxisRobot class calls the getCurCmdPos() function in the CTrajGenerator class to retrieve these command positions from fPosQueue. Although the control loop accesses the command position queue in real-time, all calculations for the trajectory are done offline, prior to starting the control loop.

# 3.12.2 Online Position-Velocity-Time (PVT) Trajectory Generation

Online trajectory generation in the QMARC is performed by calculating the piece-wise cubic polynomial between any two knots. Like the PMAC, each knot is specified with a position, velocity and time interval,  $X_k$ ,  $V_k$  and  $T_k$ , respectively, as shown in Figure 3-13. The piece-wise cubic polynomial spans from the *k*th knot to the (k+1)<sup>th</sup> knot, and is different for each time segment.



Figure 3-13: Schematic of path for PVT online trajectory generation

Using the general third order cubic polynomial equation, the position  $X_k$  can be defined as follows:

$$X_{k} = At^{3} + Bt^{2} + Ct + D$$
(3-8)

Taking the derivative of Equation 3-8 gives the velocity:

$$\dot{X}_{k} = V_{k} = 3At^{2} + 2Bt + C \tag{3-9}$$

where, polynomial coefficients A, B, C, and D must be solved for each time segment.

Between knots k and k+1, the initial position  $X(0) = X_k$  and initial velocity  $V(0) = V_k$ . By substituting the initial conditions into Equations 3-8 and 3-9, C and D can be solved to be  $C = V_k$  and  $D = X_k$ .

Substituting the values of C and D back into Equations 3-8 and 3-9 gives a set of two equations and two unknowns, A and B, which can be solved algebraically. The result is four linearly independent equations that can be used to solve the coefficients of the cubic polynomial.

$$A = \frac{2(X_k - X_{k+1})}{T_k^3} + \frac{(V_k - V_{k+1})}{T_k^2}$$
(3-10)

$$B = \frac{3(X_k - X_{k+1})}{{T_k}^2} - \frac{(2V_k - V_{k+1})}{{T_k}}$$
(3-11)

$$C = V_k \tag{3-12}$$

$$D = X_k \tag{3-13}$$

Since each time segment calculates the cubic polynomial with the assumption the polynomial starts at time zero, in order to connect the piece-wise cubic polynomials to form a continuous path, a time shift must be applied to Equation 3-8. The time shift,  $t_{shift}$ , is the total time of the path up to the *k*th knot. Subtracting  $t_{shift}$  from time *t* will cause a shift in the positive direction of the time-axis. The modified cubic polynomial equation used for PVT trajectory generation is therefore as follows:

$$X_{k} = A(t - t_{shift})^{3} + B(t - t_{shift})^{2} + C(t - t_{shift}) + D$$
(3-14)

In the PVTOnlineTrajGen class, Equations 3-10 to 3-13 are implemented in calcCoeff() function, and Equation 3-14 is implemented in the interpPoint() function. Both of these functions are called from the ctrlLoopOnlineTraj() function in the MultiaxisRobot class as part of the online trajectory generation control loop.

# Chapter 4

# Software Design Issues

In real-time software development, there are a number of issues that commonly occur that can be resolved with practical programming techniques. While developing the QMARC system, problems encountered involved timing, data logging and memory allocation. All of these issues were addressed and analyzed on the QMARC.

# 4.1 Timing

In robotic control, this time limit is determined by the sampling frequency of the controller. In each sampling interval there are a number of tasks that must be completed before the next sample can be processed. These tasks are as follows:

- 1. Retrieve the current motor encoder position.
- 2. Attain the current command position from the trajectory generator.
- 3. Calculate the new DAC output for velocity command of the motor using a servo control algorithm.
- 4. Output the new control signal to the DAC hardware.
- 5. Record the diagnostic data for each motor to a data buffer.

To minimize the computation time of the tasks required in every servo loop, separate control loop functions, ctrlLoop() and ctrlLoopOnline() in the MultiaxisRobot Class, were written to reduce the number of "if" conditional statements that would be needed if the two were incorporated into one function.

In addition, the control loops were programmed with the following programming guidelines. The degree of code efficiency using these guidelines depends heavily on the compiler [55].

- 1. The number of "special cases" and if-statements were kept to a minimum.
- 2. Recursive loops were kept to a minimum.
- 3. Procedures were written inline (opposed to calling functions) whenever possible.
- 4. Procedures that were not required in the control loop were done before or after the loop.
- 5. All messages sent within the control loop to the Hardware Server (steps 1 and 4) performed all motor operations with a single message, to minimize overhead caused by message-handling.
- 6. Integer arithmetic is faster than floating-point arithmetic, so variables were kept as integers whenever possible.
- 7. Boolean variables were be eliminated and replaced with integers.

#### 4.1.1POSIX Timer vs. QMARC Timer

Initially, the real-time controller used the POSIX timer functions built into the QNX operating system. POSIX is a Portable Operating System Interface standard common to operating systems such as UNIX, LINUX and QNX with additional library functions specific to each operating system. In the POSIX libraries there is a timer function that allows programmers to easily set a periodic timer according to the computer clock. QNX extends the timer capabilities by allowing programmers to link the timer to a communication network that sends messages to the controller at every time pulse. Using the POSIX timer may seem to be a plausible alternative to writing a software interrupt. Unfortunately, high-speed control applications require very quick and accurate timers. The POSIX functions did not provide a reliable periodic timer.

The key to understanding the POSIX timer problem is associated with how the POSIX timer works. Before using the POSIX timer, the timer resolution of the system must be set with a QNX function called ClockPeriod(). ClockPeriod() sets the time of a periodic interrupt associated with interrupt number 0 on the operating system. The minimum interval is determined by either the computer processor speed or 10µs [56]. The POSIX timer is basically an interrupt handler that allows the user to set the period of the timer as long as it is an even multiple of the time set by ClockPeriod(). Having a clock period of 10µs, for instance, would allow a higher resolution periodic timer, but the processor will be interrupted every 10µs. For a sampling interval of 500µs, it would therefore be feasible to set ClockPeriod() to 100µs, instead of 10µs. Since the POSIX timer is not open-source code, what happens in the handler is unknown, which may cause irregular time signals due to unknown overhead sources.

It was found that using the POSIX timer, in the real-time controller, caused irregular time samples for the first 0.30s of the control loop, no matter what the sampling frequency was set to. This irregularity was related to the message-passing to the hardware server and the clock period, but could not be isolated or amended. As a result, a specialized interrupt service routine (ISR) was written to solve the problem. This ISR was attached to a built-in timer interrupt 0 as opposed to using the POSIX timer. After each servo interrupt period, the ISR sent a timer event out to unblock any processes waiting on an InterruptWait() command. Because the ISR is a time-critical subroutine, the code in the function should be minimal. In addition, the ISR can only access a limited number of library functions [56].

Interrupt latencies have been documented by Krten [9]. These latencies arise when interrupts do not occur at exactly 400µs from when the timer is started because other processes consume processor time. For the most part, setting the control loop to the highest priority can diminish the effects of latencies, but a timer request would still be asynchronous with the clock, so it would depend on when in the clock cycle the request is made. Other latencies are involved with saving system variables before switching to and from the interrupt.

# 4.2 Data Logging

For statistical analysis of the QMARC system, data logging was implemented. A common problem in real-time systems is missing samples when logging data. By using a timer interrupt instead of the POSIX timer, the timevent.sigev\_notify property of the timer event associated with the ISR could be controlled and set SIGEV\_INTR, shown in Figure 3-8. This property allows one timer event to be queued if it cannot be processed immediately. This means that no timer event will be missed as long as the processing time of the control loop is not more than two times the sampling interval. If the control loop is not finished when another timer event has arrived, the event will be put on queue until the control loop is completed; the next iteration will simply be delayed. Data is stored in a buffer array and output to a file after the move is completed. No data will be missed as long as there is enough memory. For redundancy, the execution time of the control loop is calculated by keeping track of the ClockCycles() function, which gives the current system clock pulse. If the sampling interval is more than 40µs greater than the desired sampling period then an error message is displayed on the screen. Data logged is stored into a large static array called fBuffer. The maximum size of the buffer is 2000 samples for 10 data fields. If the number of data samples reaches the maximum size, and error message will be displayed and the control loop will go into the fault handler. This buffer size can be increased to whatever is necessary.

# 4.3 Memory Allocation of Variables

In a controller the memory allocation of large arrays is a major concern. Large arrays are used to store path knots, the position command queue and the data buffer. When allocating memory for these arrays it is often beneficial to declare a static pointer and then allocate memory to the pointer dynamically. For instance, the fPosQueue using in CTrajGenerator class is a pointer to a floating-point value. Using the setPosQueue() function in the CTrajGenerator class the memory is allocated to the position queue using the *new* command available in the C++ programming libraries, as shown in Figure 4-1. Variable iPosQueueCtr must be set prior to calling setPosQueue(), in order to initialize the position queue with the correct size. Declaring the position queue size dynamically ensures that there is exactly enough memory of the queue preventing memory waste from static declarations that are too large or memory faults from static arrays that are too small. If there is not enough memory in the system, the *new* command will return a NULL value.

```
//Declaration of relevant variables in CTrajGenerator class
class CTrajGenerator
{ private:
    float * fPosQueue;
  public:
    int iPosQueueCtr;
}
//Allocate just enough memory to store all data points
int CTrajGenerator::setPosQueue()
    //Allocate memory for position queue
    fPosQueue=new float[iPosQueueCtr];
    if (fPosQueue==NULL)
          printf("Error: Allocating memory for fPosQueue\n");
    {
          return(-1);
    }
    return 0;
}
```

#### Figure 4-1: Memory allocation code sample

The *new* operator, however, does not work for memory allocation of multi-dimensional arrays in QNX. The data buffer, fBuffer, in QMARC had to be declared statically to the size 2000 by 10 units. However, depending on where this buffer is declared a memory fault error can occur. To understand the problem, the memory allocation of programs must be examined. When programs are loaded into memory, it is organized into three segments: the *text* segment (or *code* segment), *stack* segment and *heap* segment. The text segment contains the compiled code, the stack contains variables saved during a context switch when calling a function as well as local variables declared within the function or class, and the heap stores global and static variables used in the program [57].

Initially, the fBuffer was declared in the MultiaxisRobot class. In QNX, the stack has 50kB of memory, which is enough for a small application, however the fBuffer is 2000 by 10 floating-point values in size. Each floating point is four bytes therefore the entire fBuffer is 80kB. This exceeds the 50kB limit on the stack. To resolve the problem the fBuffer was declared as a global variable, allowing the buffer to be stored on the heap, which has a lot more memory thus avoiding memory faults.

# Chapter 5

# Software Testing and Analysis

The testing of distributed real-time software systems such as the QMARC can be challenging since a real-time system is highly coupled to its environment. There are two main types of systems: Event-Triggered (ET) and Time-Triggered (TT) systems. In ET systems, actions are initiated by an observed event. Since ET systems rely heavily on other tasks, they are generally more difficult to develop and test. On the other hand, TT systems perform actions exclusively at predefined moments in time. They are synchronous to the clock, so as long as all processes have access to the same global clock source, then development is relatively easy [58]. The QMARC can be considered as an Event-Triggered system. Although QMARC have a Timer process, the Controller acts on a timer event, not at a predefined point in time. Being an ET system has drastic implications on how the system can be effectively tested.

In general, distributed software systems are tested in phases, first starting from the development and testing of individual processes, then their interfaces and finally system integration. Important properties in testing a distributed system are observability and reproducibility. Observability of a software system is the ability to test what the system does, how it does it and when it does it. In an ET system, adding the elements to observe the system could change the behaviour of the system itself. For instance in QMARC, if a printf() statement is added in the Hardware Server process to view an intermediate value during the servo loop, then the delay caused by the printf() statement itself can create a delay in the servo loop cycle, which in turn produces an error. Reproducibility is the ability to predict and reproduce the same results given the same sequence of inputs. In a system that has many concurrent processes, improper timing of events can cause differences in the observable output. A reliable distributed software system must have predictable output. Experimental testing of the QMARC can be categorized into three main groups:

- 1. Tests for real-time behaviour of the servo controller.
- 2. Tests for the controller performance.
- 3. Tests for reproducibility of the controller results.

All data collected for these experiments were done after the robot motion had completed, as to not effect the observability of the system. Testing of the trajectory generation, and safety protocols were done in unison to all tests are will not be presented as a formal experiment.

# 5.1 Real-Time Behavioural Tests and Results

The real-time behaviour of the QMARC was monitored using the ClockCycles() function available in QNX. The ClockCycles() function returns the value of the computer clock and was used as a timer for the servo loop interval.

Inaccurate clock pulses are detrimental to the controller because a fixed sampling interval is used in the trajectory generation prior to entering the control loop. If the timer pulses are incorrect and the error accumulates, then the command velocity will not be exactly as desired. Through benchmark testing, slight variations in the actual sampling interval within 5µs were detected.

Currently, the QMARC operates at a maximum frequency of 2.5kHz, or with a sampling interval of 400µs, for three concurrent motors. Calculations in the control loop on a 667MHz PC only requires about 190µs. Out of this 190µs, about 65µs is taken to send the DAC output to the motor, which is about 20µs to send an analog output signal to each motor using a single-ended command signal (opposed to a differential signal).

A step input of 1000 motor counts was applied to a single motor. As shown in Figure 5-1, when the DAC output changes drastically from a positive to negative voltage or vice-versa, the desired servo period of 400µs was increased by 20µs. This occurs at 0.025 seconds, 0.035 seconds and 0.045 seconds. If the magnitude of the DAC output during the change in polarity is large, then the result is a longer delay due to the analog output. In fact, it can take up to 40µs per channel for the digital-to-analog conversion depending on the magnitude of the DAC signal during this change. Smaller magnitude polarity changes can be observed at 0.062s and 0.0085s resulted in 10µs addition on to the servo period. The servo loop period also varies at the beginning of the move when the system is busy starting up the Sensoray 626 Encoder card. Slight variations in the servo period within 5µs are expected due to the resolution of the ClockCycles() function output.



Figure 5-1: Real-Time Servo Loop Period Variation in a Step Input Test

Technically, the additional 40µs per DAC channel would bring the total computational time of the five steps to about 310µs (for three motors), which is still within the 400µs time constraint, however, this does not happen in practice. The Timer process is set at a high priority of 50, however, the driver for the hardware preempts the Timer interrupt handler when the DAC output is taking more than 65µs. Changing the priority of the Timer to a higher priority than the Hardware Server has made no difference. The DAC driver causes up to 40µs per channel to be added on to the total time from that sampling interval. If this time accumulated, then the trajectory that was generated offline would be incorrect. However, every time the DAC signal changes signs and causes a longer servo cycle, the next servo cycle is compensated with a shorter servo cycle, such that the average between the two intervals is still about 400µs. This compensation occurs because of the global variable keeping track of the number of times the timed Interrupt 0 occurs is not cleared and the timer events are queued. As a result, the odd characteristic of the DAC driver does not affect the overall performance of the controller.

# 5.2 Controller Performance Tests and Results

The performance of the QMARC was compared to the commercial PMAC controller, currently used for control of the Deltabot. Experimental command trajectories for both controllers were developed by Rob Dekker [4]. The first path represents a standard pick-and-place operation on the X-Z plane of the Deltabot's workspace, and the second path was an arched pick-and-place path rotated by 30 degrees.

The experimental data collected from the PMAC was performed by Rob Dekker [4]. Using eleven knots to define the path in Cartesian space, he generated the joint space knots using the inverse kinematic equation of the Deltabot. These joint angles were then converted to motor counts using a quadrature encoder resolution of 4096 counts/revolution and a gear ratio of 12:1. PMAC used these knots to generate a uniform non-rational cubic B-spline path (using the *spline1* function) [6]. Unfortunately, the controller gains used by Dekker are unknown; therefore, the paths cannot be recreated. PMAC, however, was tuned for the best results possible; therefore, QMARC was also tuned for optimal performance.

The PID portions of the QMARC controller was initially tuned using Ziegler-Nichols method [46] with a 1000 count step input and then manually adjusted for fine-tuning. The velocity and acceleration feed-forward components were tuned to a sinusoidal input with an amplitude of 1000 counts for 0.5ms. Tuning was done with the objective of minimizing the sum of absolute position error. The controller gains used for QMARC are listed in Table 1. All tests on PMAC were run at 2.26 kHz (442µs period) and tests on QMARC were run at 2.5 kHz (400µs period).

Gains	Motor 1	Motor 2	Motor 3
K <sub>p</sub>	182000	182000	183000
$K_{i}$	100	100	100
K <sub>d</sub>	3000	3000	3000
$K_{v\!f\!f}$	119000	103500	104000
K aff	100	100	100

**Table 1: QMARC Controller Gains** 

#### 5.2.1Standard X-Z Plane Path Test

The standard path for the Deltabot is a pick and place motion in the X-Z plane, shown in Figure 5-2, was applied to the three arms of the Deltabot. The path moves 300mm along the X-axis and 25mm in the Z-axis, with a total move time of approximately 0.5s, allowing the Deltabot to move at the rate of about 120 cycles per minute.

The command path from the PMAC experiments was used as a basis for the QMARC experiments. Only eleven points could be used to define the path in the PMAC tests because its trajectory generator has a minimum time between knots. There is no such limit in QMARC. A Matlab program was written to extract 37 knots from the command position, uniformly spaced 10ms apart. Having more knots allows the QMARC to follow the desired path more closely. These 37 knots were then used in QMARC with cubic spline trajectory generation and then with PVT. The command positions of the three arms are depicted in Figure 5-3, along with the 37 selected knots. Note that the path for arm 2 was the same as the path for arm 3, due to the symmetry of the robot moving in the X-Z plane.



Figure 5-2: Standard X-Z Plane Path in Cartesian Space



Figure 5-3: X-Z Plane Path – Arm Positions with Selected Path Knots

After running the tests on QMARC using cubic spline and PVT trajectory generators, the end-effector position was calculated using the forward kinematics equations of the Deltabot. The achieved arm positions in Cartesian space are shown in Figure 5-4. It can be seen that the QMARC was able to follow the desired end-effector path more closely than the PMAC, whether using PVT or cubic spline trajectory generation. The greatest factor in controller performance was the tuning. Since controller tuning in QMARC is much faster and simpler than tuning in PMAC [59], it can be seen that the QMARC yielded better results.



Figure 5-4: X-Z Plane Path – End-Effector Position using PMAC and QMARC

# 5.2.1.1 Tests using Cubic Spline Trajectory Generation

Cubic spline trajectory generation was used for QMARC tests to ensure that the robot motion was smooth. Offline cubic spline interpolation guaranteed velocity and acceleration continuity. By using path knots sampled directly from the PMAC tests, the cubic spline trajectory generator in QMARC was able to reproduce the PMAC command signal within 0.002 radians.

As shown in Figure 5-5, the actual positions of the arms were much closer to the command path user QMARC than PMAC. The actual position of all three arms using PMAC lagged behind the command position in regions of high velocity. In QMARC, this velocity error was compensated for by increasing feed-forward velocity compensation. In theory, this could have also been done in PMAC; however, both controllers have limits to the feed-forward velocity compensation. By increasing the gain too high, the motor will start to vibrate and become unstable. Although QMARC was implemented with the same controller algorithm as PMAC, their internal structures are very different as a result; the limits on controller gains are also different. If PMAC's feed-forward compensation could have been increased more, then it probably would have been tuned further. PMAC must have hit its gain limit. In general, QMARC feed-forward velocity gains can be used with more success in mitigating velocity effects on servo position control than PMAC.


Figure 5-5: X-Z Plane Path - Arm Positions for PMAC and QMARC with Cubic Spline

The Arm position errors for both PMAC and QMARC are shown in Figure 5-6. The position error of the PMAC ranged from –0.0970 to 0.0964 radians from Arm 1, -0.0609 to 0.0616 radians for Arm 2, and –0.0619 to 0.0616 radians for Arm 3. QMARC had an error from –0.00627 to 0.00680 radians for Arm 1, -0.00634 to 0.00327 radians for Arm 2 and –0.00676 to 0.00442 radians from Arm 3. Overall, the accumulated following error of PMAC was 8 to 12 times that of QMARC with cubic spline trajectory generation. These results are summarized in Table 2. Looking at the velocity profiles of the position errors for PMAC and comparing them to the velocity profile of the command signal in Figure 5-7 confirms the observation that velocity was the cause of high following error in PMAC. The velocity profile of Arm 1 matches that of position error, and the same goes with Arm 2 and 3. The velocity profile and the position error for PMAC were very closely related.

Arm #	Controller	Min. Position Error (rad)	Max. Position Error (rad)	Accumulated Absolute Following Error (rad)
1	PMAC	-0.0970	0.0964	6.407
	QMARC	-0.00627	0.00680	0.538
2	PMAC	-0.0609	0.0616	4.344
	QMARC	-0.00634	0.00327	0.513
3	PMAC	-0.0619	0.0616	4.358
	QMARC	-0.00676	0.00442	0.525

Table 2: X-Z Plane Path - Arm Position Errors for PMAC and QMARC using Cubic Spline

The source of position error using QMARC was mostly due to arm acceleration. This error will be analyzed in more detail in the next section.



Figure 5-6: X-Z Plane Path - Arm Position Errors for PMAC and QMARC with Cubic Spline



Figure 5-7: X-Z Plane Path - Command Velocity using PMAC and QMARC with Cubic Spline

#### 5.2.1.2 Tests with PVT Trajectory Generation

As a comparison between the two types of trajectory generation in QMARC, the PVT interpolation algorithm was also applied to the standard X-Z plane path using the same 37 path knots uniformly spaced 10ms apart. The command position generated by the cubic spline and PVT algorithms were within 0.001 radians of each other. The most significant difference between PVT and cubic spline trajectory generators were the arm velocities. Because PVT does not guarantee velocity and acceleration continuity, the command velocities was not smooth, causing slightly higher position error than cubic spline. The QMARC PVT command velocity in Figure 5-8 depicts the slight arcs between path knots. These arcs can be minimized by using a greater number of path knots in PVT trajectory generation.



Figure 5-8: X-Z Plane Path – Command Velocities for PVT and Cubic Spline on QMARC

The position errors of the three arms using the cubic spline and PVT are depicted in Figure 5-9. The accumulated following error using cubic spline was 0.667 radians for Arm 1, 0.648 radians for Arm 2 and 0.711 radians for Arm 3. Whereas the accumulated following error for PVT was 0.03% to 0.09% higher at 0.668 for Arm 1, 0.675 for Arm 2 and 0.715 for Arm 3. Not only were the accumulate errors very close, but the actual profile of the position errors were almost identical. Looking more closely at the command acceleration of the path, shown in Figure 5-10, revealed that the position errors were due to the acceleration of the command signal. Knowing this, the feed-forward acceleration compensation in the QMARC was increased; however, the error did not change significantly. QMARC could not compensate for acceleration any further. Whether using the cubic spline trajectory generation or PVT online method, the following error was still exceptionally low compared to PMAC.



Figure 5-9: X-Z Plane Path – Arm Position Errors with PVT and Cubic Spline on QMARC



Figure 5-10: X-Z Plane Path - Command Acceleration

### 5.2.2Rotated Arc Path Test

The second path was an arched pick-and-place path rotated by 30 degrees about the Z-axis. This path traveled 300 mm along the X-axis, 15mm in the Z-axis and 200mm across the Y-plane, as shown in Figure 5-11. Using an rotated arc command path allows for faster pick-and-place motion, by saving time in the distance the end-effector needs to travel, and also by creating smoother velocity and acceleration profiles so that controllers can track the path more easily.



Figure 5-11: Rotated Arc Path in Cartesian Space

Like the standard X-Z plane path test, the command positions from the PMAC were used to create the path knots of QMARC trajectory generation. For this path, 57 knots were used, uniformly spaced 10ms apart. The total time of the motion is about 0.65s. Arm positions of the three motors are depicted in Figure 5-12. Notice that the command path is a lot smoother for the arched path than the

X-Z plane path in Figure 5-3. Because the motion moves along all three axes, the arm motions for each motor had different profiles. The rotated arc path tests were tested on PMAC and QMARC using only cubic spline trajectory generation.



Figure 5-12: Rotated Arc Path - Arm Positions with selected path knots

The end-effector positions were calculated using the forward kinematic equations for the arms from both the PMAC and QMARC tests, as shown in Figure 5-13. It can be seen that the PMAC path was closer to the command path using this arched trajectory instead of the square trajectory in the previous test, showing that the smoother command path does make a difference in the controller performance. The end-effector position using QMARC, however, was still closer to the command position.



Figure 5-13: Rotated Arc Path - End-Effector Position for PMAC and QMARC

The nature of the position errors on the rotated path was very similar to those of the X-Z plane path. Arm positions for the Deltabot are shown in Figure 5-14. Again, the arm position using PMAC lagged behind the command position at times of higher velocity. QMARC was very close to the command position but had slight overshooting at around 0.04s. The command paths for PMAC and QMARC were nearly identical with differences up to 0.001 radians at areas of high velocity.

Positional errors for both PMAC and QMARC are shown in Figure 5-15. The PMAC following error was lower with the rotated path than the X-Z plane path, despite the rotated path being 0.2s longer. For the rotated path, the position errors for PMAC ranged from -0.0509 to 0.0523 radians for Arm 1, -0.0229 to 0.0238 radians from Arm 2 and -0.0520 to 0.0530 radians from Arm 3. Corresponding errors on the QMARC ranged from -0.00313 to 0.000508 radians for Arm 1, -0.00383 to 0.00000243 radians for Arm 2, and -0.00484 to 0.0011 radians from Arm 3. In general, the accumulated following error of PMAC was one order of larger than QMARC. These results are summarized in Table 3.

Arm #	Controller	Min. Position Error (rad)	Max. Position Error (rad)	Accumulated Absolute Following Error (rad)
1	PMAC	-0.0509	0.0523	5.196
	QMARC	-0.00313	0.000508	0.457
2	PMAC	-0.0229	0.0238	3.200
	QMARC	-0.00383	0.00000243	0.606
3	PMAC	-0.0520	0.0530	5.268
	QMARC	-0.00484	0.0011	0.562

Table 3: Rotated Arc Path - Arm Position Errors for PMAC and QMARC



Figure 5-14: Rotated Arc Path – Arm Position for PMAC and QMARC



Figure 5-15: Rotated Arc Path – Arm Position Errors for PMAC and QMARC

Like the X-Z Plane tests, the PMAC position errors had the same profile as the command velocity for the rotated path shown in Figure 5-16. It seemed like the PMAC could not match the velocity peaks of the arms, and lagged behind throughout the motion. QMARC followed the command velocity better but still had some overshoot in the first 0.05s and in areas of high acceleration. Acceleration was again the cause of error in QMARC, which was expected since the controller gains were not changed between the X-Z plane path tests and the rotated path tests. Overall, PMAC's performance on the rotated path was better than the X-Z plane path, however, QMARC still out-performed PMAC in both experiments.



Figure 5-16: Rotated Arc Path - Arm Velocity of PMAC and QMARC

### 5.3 Reproducibility Tests and Results

The standard X-Z plane path was run on QMARC one hundred times consecutively to observe the reproducibility of the controller, its ability to reproduce similar results given the same input. The number of times the servo period took 40µs less than or greater than the desired servo period was also recorded. Looking at the number of times servo cycles where the controller was too slow is a good indication to the consistency of the real-time aspect of the controller.

#### 5.3.1Repeated Trials

The Controller Console was run manually for one hundred cycles using the X-Z plane path. After each cycle, the accumulated absolute following error was record. The scatter plots of the trials are depicted in Figure 5-17. For the most part, it was found that the error stayed consistent throughout the trials, this demonstrates the effectiveness and reliability of the controller. The accumulated error ranged from 0.665 to 0.682 radians for Arm 1, 0.636 to 0.649 radians for Arm 2 and 0.713 to 0.733 radians for Arm 3. Average accumulated following error of Arm 1, Arm 2 and Arm 3 were 0.667 radians, 0.641 radians, and 0.720 radians, respectively. There were a few trials, however, that were not as successful as others, such as Trial number 34 on Arm 1, which was 0.02 radians higher than the rest of the trials. Variation in the trials is not completely dependent on QMARC, but also on the motors and amplifiers themselves. If the motor suddenly moves faster than a regular trial, then the QMARC will have to correct a larger position error, this can result in a higher accumulated error. Overall, these errors are still quite consistent proving that QMARC outputs are reproducible.



Figure 5-17: Scatter Plots of Accumulated Absolute Following Error for 100 Trials

### 5.3.2Erroneous Sampling Periods

During the one hundred trials, the number of sampling periods outside of the acceptable variation range of 40µs was also recorded. The bar graph, shown in Figure 5-18, illustrates the number of erroneous servo periods in each trial. Out of the 100 trials, 27 of them had at least one erroneous servo period. However, considering that each trial has 1048 servo periods, which equals 104800 servo periods for the 100 trials, only 29 periods were outside acceptable range. This means that only 0.0277% of the servo periods were erroneous. This variation in real-time behaviour is tolerable for QMARC.



Figure 5-18: Number of Erroneous Servo Periods in 100 Trials

### Chapter 6

# Conclusions

As robotic manipulators try to achieve higher operating speeds, it has become increasing important to have controllers that can move these robots as fast as possible without sacrificing the smoothness of the motion. Many commercial controllers are available in today's market, but these controllers have a rigid structure, limit programming capabilities and a high price tag. A new class of PC-based controllers has been introduced in the past two decades as an alternative to traditional PLC and DSP solutions. These PC-based controllers use distributed real-time systems to perform the diverse concurrent tasks required in motor servo control. By using higher-level programming languages, such as C/C++, the capabilities of the PC-based controller can be greatly expanded.

In this research, a new QNX Multi-Axis Robotic Controller (QMARC) was developed in order to improve the performance of the Deltabot, a three-degree-of-freedom, ultra high-speed parallel cable-based manipulator at the University of Waterloo. QMARC was developed as an object-oriented real-time PC-based controller on QNX Neutrino 6.0 operating system to replace an existing commercial controller called PMAC, created by Delta Tau Data Systems. Although the PMAC has its own real-time processor, the rigid and complex internal structure of the PMAC makes it difficult to apply advanced control algorithms and interpolation methods. Adding unconventional hardware to PMAC, such as a camera and vision system is also quite challenging. With the development of QMARC, the flexibility issue of the controller is resolved. QMARC's open-sourced object-oriented software structure allows simple addition of new control and interpolation techniques. In addition, the software structure of the main Controller process is decoupled for the Hardware Server, so that any hardware change does not change the main controller, just the Hardware Server. QMARC is also equipped with a user-friendly graphical user interface, and many safety protocols to make it a safe and easy-to-use system.

In experimental tests, it was determined that the QMARC is a very reliable real-time controller. Real-time tests showed that although the servo loop period is not always exact the same due to the DAC output, the  $40\mu$ s differences in the period does not impact the overall controller performance because the error does not accumulate. In addition, these erroneous servo periods only occur in 0.0277% of the servo loop intervals.

By comparing the PMAC and QMARC controller performance on two pick-and-place paths, it was found that in both paths QMARC yielded better results than PMAC on all three motors of the Deltabot. Accumulated following error for the PMAC was at least one order of magnitude greater than QMARC. For a 0.5s pick-and-place move, the QMARC's accumulated following error was only 0.05 radians. PMAC positional error was mostly attributed to the tuning of PMAC compared to QMARC. Although both controllers have the same control algorithm, their internal structures differ resulting in different threshold. QMARC can be tuned for better results than PMAC and with more ease. Unlike PMAC, QMARC also does not have any trajectory generation restrictions on it. These experimental results show that QMARC is a good and safe controller. Running the controller for one hundred trials also demonstrated consistent results in the QMARC performance.

The stable foundation laid down by the QMARC will allow for future development of QMARC into a fully functional controller ready for commercial use. The object-oriented software structure will make the QMARC more expandable, easier to maintain and easier to understand. These characteristics allow for future research into the servo control, trajectory generation and vision system to be more easily implemented. Due to the class structure, the existing code can be reused, hence decreasing the development time that would be required to code and debug new software modules. Finally, the use of a simple Pentium III computer with a single Sensoray 626 Encoder Card makes QMARC a highly cost-effective system. The QMARC has proved to be a highly successful controller that yields endless possibilities for future applications.

### Chapter 7

## Recommendations

QMARC was built as a foundation for further research into control algorithms, trajectory generation and different types of hardware, such as gripper and a vision system. The software structure of the QMARC can be expanded to accommodate these changes without rewriting the whole system. Although the QMARC was created for the Deltabot, it can be implemented on any manipulator; all that needs to be updated is the Hardware Server process. Recommendations on how to incorporate a vision system, gripper, watch-dog timer and how to use QMARC as a controller in an existing system are covered in this chapter.

### 7.1 Adding a Vision System

There are two main components to adding a vision system to the QMARC: the hardware driver and the camera data processing. The simplest way to add the camera hardware to the system is by adding the procedures required to read the camera data in the Hardware Server. Since the Controller process already sends messages requesting hardware-related tasks to the Hardware Server, it is most appropriate to add another message type for camera requests in the server and then write new functions to access camera hardware. Theses functions would be to trigger the camera, read data and change settings. If the Cognex Insight 5100 vision sensor is used on the QMARC, then additional protocols for network communication must also be added to the system, because the Cognex vision sensor transmits data through the network ports on the computer.

The vision sensor will most likely be used to detect the position and orientation of objects in its field of view. Data about these objects will need to be processed and stored in a queue in memory. All of this data processing should be done in the main Controller process. First, a new Base Class, for example, called CCamera can be derived from the CObject base class. This CCamera class will

inherit the fServoInt, the servo period variable, from CObject class. Procedures such as storing object data to the queue and getting information from the queue should be contained in the CCamera class. To deal with the particular format of the camera data, a Specific Subclass, like CognexCamera, can be created. CognexCamera can contain the specific functions to parse the data, process the data, and convert it to different coordinate systems. These functions will change for different vision sensors. By creating a new CCamera base class separate from the specific type of sensor, this allows a variety of vision sensors to be implemented without having to rewrite all procedures.

Higher functions such as image processing and pattern recognition should be implemented as a completely new Base Classes that are not derived from anything because they are not related to any of the existing Base Classes.

### 7.2 Adding a Gripper to the End-Effector

Simple devices such as grippers or suction-cups may be added to the end-effector of the Deltabot. These devices will most likely require some digital output ports from the Sensoray 626 Encoder card. Currently, only nine out of forty-eight digital input/output channels on the card are being used. To add a gripper, a Specific Subclass should be derived from the existing CGripper class, which was included in the QMARC design. The signal to turn the digital line on and off can be handled by another message type in the Hardware Server, which is already configured to perform digital input/output.

### 7.3 Watch-dog Timer

Currently, the QMARC system does not protect the manipulator from a computer crash. There, however, is a watch-dog timer built into the Sensoray 626 Encoder card. If a separate thread is used to send an "ok" signal periodically to the watch-dog timer, then if the computer crashes the watch-dog timer will know that something has gone wrong and take the appropriate actions. The watch-dog timer should be further investigated for future implementations of QMARC.

### 7.4 Using QMARC in an Existing System

The QMARC can be incorporated into an existing system as a dedicated controller, if the data for the trajectory generation and controller execution could be passed to the QNX computer through the network card. QNX has advanced network protocols that have been used by other researchers [32] to do this. A new Base Class can be written for the network communication protocols and to handle the data processing. QMARC may also need another process or thread to act as a server waiting for network data. This server can then send messages to the Controller process.

# Bibliography

- [1] Khajepour, A., Chan, E., Behzadipour, S., Dekker, R., "Deltabot: A new cable-based ultra high speed robot", in *Proceedings of IMECE S'03*, ASME, 2003.
- [2] Amir Khajepour, Saeed Behzadipour, Robert Dekker, and Edmon Chan "Light Weight Parallel Manipulators using Active/Passive Cables", US Provisional Patent: 60/394,272.
- [3] Stewart, D., "A platform with six degrees of freedom,", in *Proceedings of Institute of Mechanical Engineers*, London, 1965, pp. 371-386.
- [4] Dekker, R., Design and Testing of an Ultra High Speed Cable-Based Parallel Robot, Masters of Science Thesis, University of Waterloo, Waterloo, ON, 2003.
- [5] Behzadipour, Saeed, *Ultra High-Speed Cable-based Parallel Robots*, Ph.D. Proposal, University of Waterloo, ON, 2003, p.32.
- [6] Inc. Delta Tau Data Systems, User Manual: PMAC, Delta Tau Data Systems, Chatsworth, CA, USA, May 29, 2003, Chapter 7, p. 3-27.
- [7] Koivo, Heikki N., and Peltomaa, Arto S., "Microcomputer real-time multi-tasking operating systems in control applications", in *Computers in Industry*, vol. 5, n. 1, March 1984, p. 31-39.
- [8] Joseph, Mathai, *Real-time Systems Specification, Verification and Analysis*, Prentice Hall International Series in Computer Science, Trowbridge, Wiltshire, 1996, p.18-19.
- Krten, Rob, Getting Started with QNX Neutrino 2 A guide for Realtime Programmers, PARSE Software Devices, Kanata, ON, Canada, 2001, p. 111-159.
- [10] Todd, Micheal, and Green, David G., "Object-oriented approach to robotic motion", in Conference Proceedings of IEEE SoutheastCon, Charlotte, NC, USA, Apr. 4-7, 1993.
- [11] Gee, D., "The how's and why's of PC based control", *Pulp and Paper Industry Technical Conference*, June 18-22, 2001, pp. 67-74.
- [12] Urban, J. E., Hankyu, J., "Executable specification for distributed software systems," in *Proc. Of Fifth IEEE Computer Society Workshop on Future Trends of Distributed Computing Systems*, Aug. 28-30, 1995, pp. 257-265.

- [13] Luh, J. Y. S., Lin, C. S., "Scheduling of parallel computation for a computer-controlled mechanical manipulator", *IEEE Trans. Syst., Man, Cybern.*, vol. SMC-12, pp. 214-234, March, 1982.
- [14] Kasahara, H., Narita, S., "Parallel Processing of Robot-Arm Control Computation on Multimicroprocessor System," *IEEE Journal of Robotics and Automation*, Vol. RA-1, No. 2, June 1985, pp. 104-113.
- [15] Nigam, Ravi, Lee, C. S. G., "A Multiprocessor-Based Controller for the Control of Mechanical Manipulator", in *Proc. Of IEEE Int'l Conf. on Robotics and Automation*, March 1985, pp. 815-821.
- [16] Chen, J. B., Fearing, R. S., Armstrong, B. S., Burdick, J. W., "NYMPH: A multiprocessor for manipulation applications", in *Proc. IEEE Int'l Conf. On Robotics and Automation*, San Francisco, CA, April 1986, vol. 3, pp. 1731-1736.
- [17] Liu, C. H., Chen, Y. M., "Multimicroprocessor-based Cartesian space control techniques for a mechanical manipulator", in *Proc. IEEE Int'l Conf. On Robotics and Automation*, 1986, pp. 823-827.
- [18] Kriegman, D. J., Seigel, D. M., Narasimhan, S., Hollerbach, J. M., Gerpheide, G. E., "Computational architecture for the Utah/MIT hand", *IEEE Conference on Robotics and Automation*, 1984, pp. 918-924.
- [19] Zheng, Y. F., and Chen, B. R., "A multiprocessor for dynamic control of multilink systems", 1985 IEEE Int'l Conf. On Robotics and Automation, Vol. 2, March 1985, pp. 295-300.
- [20] Stewart, D. B., Schmitz, D. E., Khosla, P. K., "The CHIMERA II: real-time multiprocessing environment for sensor-based control applications", in *Proc. IEEE Int'l Symp. Intelligent Control*, 1989, pp. 265-271.
- [21] Narasimhan, S., Siegel, D. M., Hollerbach, J. M., "Condor: an architecture for controlling the utah-mit dexterous hand", *IEEE Trans. Robotics and Automation*, vol. 5, Oct. 1989, pp. 616-627.
- [22] Erol, N. A., Altintas, Y., "Open architecture modular took kit for motion and machining process control", *Manufacturing Science and Technology*, Vol. 1, 1997, pp. 15-22.
- [23] Pritschow, G., Daniel, Ch., Junghans, G., Sperling, W., "Open System Controllers-A Challenge for the Future of the Machine Tool Industry", *CIRP Annals*, Vol. 42, No. 1, 1993, pp. 449-452.
- [24] Costescu, N., Dawson, D., Loffler, M., "QMotor 2.0 a real-time PC based control environment", *IEEE Control Systems*, Vol. 19, Issue 3, June 1999, pp. 68-76.

- [25] Y. P. Luh, S. S. Chiou, J. W. Chang, "Design of Distributed Control System Software Using Client-Server Architecture", in Proc. IEEE Int'l Conf. Industrial Technology, 1996, pp. 348-350.
- [26] Stroustrup, B., "An overview of the C++ programming language", in *Handbook of Object Technology*, Boca Raton, FL: CRC Press, 1999.
- [27] Miller, D. J., Lennox, R. C., "An object-oriented environment for Robot System Architectures," in Proc. IEEE Int'l Conf. on Robotics and Automation, 1990, pp. 52-361.
- [28] Bagchi, S. Kawamura, K., "An Architecture of a Distributed Object-oriented Robotic System", in *Proc. Intelligent Robots and Systems*, 1992 Vol. 2, pp. 711-716.
- [29] Bacio, B. T., Ramaswamy, S., and Barber, K. S., "OARS: An Object-oriented architecture for reactive systems", in *Proc. IEEE Int'l Conf. on Robotics and Automation*, 1996, pp. 1093-1098.
- [30] Fernandex, J. A., Gonzalez, J., "The NEXUS open system for integrating robotic software", *Robotics Comput Integrated Manuf*, Vol. 15, No. 6, 1999, pp 431-440.
- [31] Traub, A., and Schraft, R., "An object-oriented realtime framework for distributed control systems," in *Proc. IEEE Int'l Conf. on Robotics and Automation*, May, 1999, pp.3115-3121.
- [32] Costescu, N., Loffler, M., Zergeroglu, E., Dawson, D., "Qrobot a multitasking PC based robot control system", in *Proc. IEEE Conf. on Control Applications*, 1998, Vol. 2, Part 2, pp. 892-896.
- [33] Loffler, M. S., Chitrakaran, V. K., Dawson, D. M., "Design and Implementation of the Robotic Platform", in *Proc. IEEE Conf. on Control Applications*, 2001, pp. 357-362.
- [34] Paul, R., "Manipulator Cartesian path control", *IEEE Trans. On Systems, Man and Cybernetics*, Vol. SMC-9, No. 11, Nov. 1979, pp. 702-711.
- [35] Taylor, R. H., "Planning and execution of straight-line manipulator trajectories", *IBM J. Research and Development*, Vol. 23, 1979, pp. 424-436.
- [36] Luh, J. Y. S., Lin, C. S., "Optimal path planning for mechanical manipulators", ASME Journal Dynamic Systems, Measurement, and Control, Vol. 102, June, 1981, pp. 142-151.
- [37] Paul, R. C., "Modeling, trajectory calculation and servoing of a computer controlled arm," *Ph.D. dissertation*, Stanford Univ., CA., Aug. 1972.
- [38] Finkel, R. A., "Constructing and debugging manipulator programs," *Memo AIM-284*, Stanford Artificial Intelligence Laboratory, Stanford Univ., CA., No. 1972.
- [39] Lin, C. S., Chang, P. R., Luh, J. Y. S., "Formulation and optimization of cubic polynomial joint trajectories for industrial robots", *IEEE Trans. Aut. Control*, Vol. AC-28, 1983, pp. 1067-1073.
- [40] Bobrow, J. E., Dubowsky, S., Gibson, J. S., "Time optimal control of robotic manipulators along specified paths", *Int'l Journal Robotics Res.*, Vol. 4, 1985, pp. 3-17.

- [41] Lin, C. S., Chang, P. R., "Joint trajectories of mechanical manipulators for Cartesian path approximation", *IEEE Trans. Syst., Man, Cybern*, Vol. SMC-13, Nov. 1983, pp. 1094-1102.
- [42] Dubowsky, S., Norris, M. A., Shiller, Z., "Time Optimal Trajectory Planning for Robotic Manipulators with Obstacle Avoidance: A Cad Approach," *Proc. Of IEEE Int'l Conf. On Robotics and Automation*, 1986, pp. 1906-1912.
- [43] Bobrow, J. E., "Optimal Robot Path Planning Using Minimum-Time Criterion," *IEEE Journal of Robotics and Automation*, Vol. 4, No. 4, 1988, pp. 443-450.
- [44] Astrom, K.J., Hagglund, T., *PID controllers: theory, design, and tuning,* Second Edition, Instrument Society of America.
- [45] Rocco, P., "Stability of PID control for industrial robot arms", *IEEE Trans. on Robotics and Automation*, Vol. 12, No. 4, Aug. 1996, pp. 606-614.
- [46] Ziegler, J. G., Nichols, N. B., "Optimum settings for automatic controllers", *Transactions of the ASME*, Vol. 64, 1942, pp. 759-768.
- [47] Hayward, G. L., Computerized Control System: Basics. In: Gauri, S. (ed) Computerized control systems in the food industry, New York: Marcel Dekker, Inc., 1997, pp. 87-117.
- [48] Astrom, K. J., Hagglund, T., "The future of PID control", *Control Engineering Practice*, Vol. 9, No. 11, Nov. 2001, pp. 1163-1175.
- [49] Cohen, G. H., and Coon, G. A., "Theoretical consideration of retarded control", *Transactions of ASME*, Vol. 75, 1953, pp. 827-834.
- [50] Astrom, K. J., Hagglund, T., "Revisiting the Ziegler-Nichols step response method for PID control", *Journal of Process Control*, Vol. 14, 2004, pp. 635-650.
- [51] Kraus, T. W., Mayron, T. J., "Self-tuning PID controllers based on pattern recognition approach,", *Control Engineering*, 1984, pp. 106-111.
- [52] Higham, E. H., "A self-tuning controller based on expert systems and artificial intelligence", *Proc. Control 85*, UK, 1985, pp. 110-115.
- [53] He, S. Z., Tan, S., Xu, F. L., and Wang, P. Z., "Fuzzy self-tuning of PID controllers", *Fuzzy Sets and Systems 56*, 1993, pp. 37-46.
- [54] Press, W. H., Flannery, B. P., Teukolsky, S. A. and Vetterling, W. T., *Numerical Recipes: The Art of Scientific Computing (Fortran Version)*, Cambridge University Press, Cambridge, 1989, pp. 86-89.

- [55] Sollbach, E. M., Goldenberg, A. A., "Real-Time Control of Robots: Strategies for Hardware and Software Development", *Robotics & Comptuer-Integrated Manufacturing*, Vol. 6, No. 4, 1989, pp. 323-329.
- [56] (QNX Online Developer Support) QNX Software Systems, 2004, Available: http://www.qnx.com/developers/docs/momentics621 docs/neutrino/sys arch/kernel.html (URL).
- [57] (EE150 Introduction of Computer Programming Methods Lecture Notes) University of Hawaii Electrical Engineering, 1994, Available: http://www-ee.eng.hawaii.edu/Courses/EE150/Book/ chap14/subsection2.1.1.8.html (URL).
- [58] Schütz, Werner, *The Testability of Distributed Real-Time Systems*, Kluwer Academic Publishers, Norwell, Massachusetts, 1993.
- [59] Tran, H., Khajepour, A., Erkorkmaz, K., "Development and Analysis of a PC-Based Object-Oriented Real-Time Robotics Controller", accepted for Proc. of *IEEE Conference on Control Applications*, Toronto, ON, August 28-31, 2005.