GPS+ Reference **Manual**

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Chapter 1 GPS Overview

The Global Positioning System (GPS) is a satellite navigation system capable of providing a highly accurate, continuous global navigation service independent of other positioning aids. GPS provides 24-hour, all-weather, worldwide coverage with position, velocity and timing information.

The system uses the NAVSTAR (NAVigation Satellite Timing And Ranging) satellites which consists of 24 operational satellites to provide a GPS receiver with at least six satellites in view at all times. A minimum of four satellites in view are needed to allow the receiver to compute its current latitude, longitude, altitude with reference to mean sea level and the GPS system time.

 Figure 1: NAVSTAR Satellite Orbit Arrangement

1.1 GPS System Design

The GPS system design consists of three parts:

- The Space segment
- The Control segment
- The User segment

All these parts operate together to provide accurate three dimensional positioning, timing and velocity data to users worldwide.

1.1.1 The Space Segment

The space segment is composed of the NAVSTAR GPS satellites. The constellation of the system consists of 24 satellites in six 55° orbital planes, with four satellites in each plane (plus room for

spares). The orbit period of each satellite is approximately 12 hours at an altitude of 20 183 kilometers. This provides a GPS receiver with at least six satellites in view from any point on earth, at any particular time.

The GPS satellite signal identifies the satellite and provides the positioning, timing, ranging data, satellite status and the corrected ephemerides (orbit parameters) of the satellite to the users. The satellites can be identified either by the Space Vehicle Number (SVN) or the Pseudorandom Code Number (PRN). The PRN is used by the NovAtel receiver.

The GPS satellites transmit on two L-band frequencies; one centered at 1575.42 MHz (L1) and the other at 1227.60 MHz (L2). The L1 carrier is modulated by the C/A code (Coarse/Acquisition) and the P code (Precision) which is encrypted for military and other authorized users. The L2 carrier is modulated only with the P code.

1.1.2 The Control Segment

The control segment consists of a master control station, five base stations and three data up-loading stations in locations all around the globe.

The base stations track and monitor the satellites via their broadcast signals. The broadcast signals contain the ephemeris data of the satellites, the ranging signals, the clock data and the almanac data. These signals are passed to the master control station where the ephemerides are re-computed. The resulting ephemerides corrections and timing corrections are transmitted back to the satellites via the data up-loading stations.

1.1.3 The User Segment

The user segment, such as the NovAtel receiver, consists of equipment which tracks and receives the satellite signals. The user equipment must be capable of simultaneously processing the signals from a minimum of four satellites to obtain accurate position, velocity and timing measurements.

1.2 Height Relationships

What is a geoid?

An equipotential surface is any surface where gravity is constant. This surface best represents mean sea-level and not only covers the water but is projected throughout the continents. In North America this surface is most commonly used at its zero value, that is, all heights are referenced to this surface.

What is an ellipsoid?

An ellipsoid, also known as a spheroid, is a mathematical surface which is sometimes used to represent the earth. Whenever you see latitudes and longitudes describing the location, this coordinate is being referenced to a specific ellipsoid. GPS positions are referred to an ellipsoid known as WGS84 (World Geodetic System of 1984).

What is the relationship between a geoid and an ellipsoid?

The relationship between a geoid and an ellipsoid is shown in *[Figure 2, Illustration of Receiver](#page-6-1) [Height Measurements on Page 7](#page-6-1)*.

 Figure 2: Illustration of Receiver Height Measurements

From the above diagram, and the formula $h = H + N$, to convert heights between the ellipsoid and geoid we require the geoid-ellipsoid separation value. This value is not easy to determine. A worldwide model is generally used to provide these values. NovAtel GPS receivers store this value internally. This model can also be augmented with local height and gravity information. A more precise geoid model is available from government survey agencies for example, U.S. National Geodetic Survey or Geodetic Survey of Canada (see *[Chapter 8, Standards/References](#page-30-1)* starting on *[Page 31](#page-30-1)*).

Why is this important for GPS users?

The above formula is critical for GPS users as they typically obtain ellipsoid heights and need to convert these into mean sea-level heights. Once this conversion is complete, users can relate their GPS derived heights to more "usable" mean sea-level heights.

1.3 GPS Positioning

GPS positioning can be categorized as follows:

- 1. single-point or relative
- 2. static or kinematic
- 3. real-time or post-mission data processing

A distinction should be made between *accuracy* and *precision*. *Accuracy* refers to how close an

estimate or measurement is to the true but unknown value; *precision* refers to how close an estimate is to the mean (average) estimate. *[Figure 3](#page-7-1)* illustrates various relationships between these two parameters: the true value is "located" at the intersection of the cross-hairs, the centre of the shaded area is the "location" of the mean estimate, and the radius of the shaded area is a measure of the uncertainty contained in the estimate.

 Figure 3: Accuracy versus Precision¹

1.3.1 Single-Point vs. Relative Positioning

In *single-point* positioning, coordinates of a GPS receiver at an unknown location are sought with respect to the earth's reference frame by using the known positions of GPS satellites being tracked. The position solution generated by the receiver is initially developed in earth-centered coordinates which can subsequently be converted to any other coordinate system. With as few as four GPS satellites in view, the absolute position of the receiver in three-dimensional space can be determined. Only one receiver is needed.

In *relative* positioning, also known as *differential* positioning, the coordinates of a GPS receiver at an unknown point (the "rover" station) are sought with respect to a GPS receiver at a known point (the "base" station). The concept is illustrated in *[Figure 4, Example of Differential Positioning on Page 9](#page-8-0).* The relative-position accuracy of two receivers locked on the same satellites and not far removed from each other - up to tens of kilometers - is extremely high. The largest error contributors in single-point positioning are those associated with atmospheric-induced effects. These errors, however, are highly correlated for adjacent receivers and hence cancel out in relative measurements. Since the position of the base station can be determined to a high degree of accuracy using conventional surveying techniques, any differences between its known position and the position computed using GPS techniques can be attributed to various components of error as well as the receiver's clock bias. Once the estimated clock bias is removed, the remaining error on each pseudorange can be determined. The base station sends information about each satellite to the rover station, which in turn can determine its

^{1.}Environment Canada, 1993, Guideline for the Application of GPS Positioning, p. 22.

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position much more exactly than would be possible otherwise.

The advantage of relative positioning is that much greater precision (presently as low as 2 mm, depending on the method and environment) can be achieved than by single-point positioning. In order for the observations of the base station to be integrated with those of the rover station, relative positioning requires either a data link between the two stations (if the positioning is to be achieved in real-time) or else post-processing of the data collected by the rover station. At least four GPS satellites in view are still required. The absolute accuracy of the rover station's computed position will depend on the accuracy of the base station's position.

 Figure 4: Example of Differential Positioning

1.3.2 Static vs. Kinematic Positioning

Static and *kinematic positioning* refer to whether a GPS receiver is stationary or in motion while collecting GPS data. Refer to *Chapter 6, Volume 1* of the *OEM4 Manual* set for more details on static and real time kinematic positioning. SUPERSTAR-II based product manuals also contain a chapter on positioning modes of operation.

1.3.3 Real-time vs. Post-mission Data Processing

Real-time or *post-mission* data processing refer to whether the GPS data collected by the receiver is processed as it is received or after the entire data-collection session is complete. Refer to *Chapter 6, Volume 1* of the *OEM4 Manual* set for more details on static and real time kinematic positioning.

Chapter 2 INS Overview

GPS positioning observes range measurements from orbiting Global Positioning System Satellites. From these observations, the receiver can compute position and velocity with high accuracy. NovAtel GPS positioning systems have been established as highly accurate positioning tools, however GPS in general has some significant restrictions, which limit its usefulness in some situations. Accurate GPS positioning requires line of site view to at least four satellites simultaneously. If these criteria are met, differential GPS positioning can be accurate to within a few centimetres. If however, some or all of the satellite signals are blocked, the accuracy of the position reported by GPS degrades substantially, or may not be available at all.

In general, an Inertial Navigation System (INS) uses forces and rotations measured by an IMU to calculate acceleration, velocity and attitude. This capability is embedded in the firmware of our *plus* series of receivers. Forces are measured by accelerometers in three perpendicular axes within the IMU and the gyros measure rotations around those axes. Over short periods of time, inertial navigation gives very accurate acceleration, velocity and attitude output. The IMU must have prior knowledge of its initial position, initial velocity, initial attitude, Earth rotation rate and gravity field. Since the IMU sensor measures changes in orientation and acceleration, the INS determines changes in position and attitude, but initial values for these parameters must be provided from an external source. Once these parameters are known, an INS is capable of providing an autonomous solution with no external inputs. However, because of errors in the IMU sensor measurements that accumulate over time, an inertial-only solution will degrade with time unless external updates such as position, velocity or attitude are supplied.

NovAtel's SPAN system's combined GPS/INS solution integrates the raw inertial measurements with all available GPS solution and raw measurement information to provide the optimum solution possible in any situation. By using the high accuracy of the GPS solution, the INS measurement errors can be modeled and mitigated. Conversely, the continuity and relative accuracy of the INS solution enables faster GPS signal reacquisition and RTK solution convergence.

The advantages of using SPAN technology are its ability to:

- Provide a full attitude solution (roll, pitch and azimuth)
- Provide continuous solution output (in situations when a GPS-only solution is impossible)
- Provide faster signal reacquisition and RTK solution resolution (over stand-alone GPS because of the tightly integrated GPS and IMU observations)
- Output high-rate (up to 100 Hz) position, velocity and attitude solutions for high-dynamic applications
- Use raw phase observation data (to constrain INS solution drift even when too few satellites are available for a full GPS solution)

Chapter 3 Satellite**-B**ased **A**ugmentation **S**ystem

A Satellite-Based Augmentation System (SBAS) is a type of geo-stationary satellite system that improves the accuracy, integrity, and availability of the basic GPS signals. Accuracy is enhanced through the use of wide area corrections for GPS satellite orbits and ionospheric errors. Integrity is enhanced by the SBAS network quickly detecting satellite signal errors and sending alerts to receivers to not use the failed satellite. Availability is improved by providing an additional ranging signal to each SBAS geostationary satellite.

SBAS includes the Wide-Area Augmentation System (WAAS), the European Geo-Stationary Navigation System (EGNOS), and the MTSAT Satellite-Based Augmentation System (MSAS). At the time of publication, there are two WAAS satellites over the western Atlantic Ocean and the Pacific (PRN 122 and PRN 134 respectively) and one EGNOS satellite over the eastern Atlantic Ocean (PRN 120). SBAS data is available from any of these satellites and more satellites will be available in the future.

The primary functions of SBAS include:

•data collection •determining ionospheric corrections •determining satellite orbits •determining satellite clock corrections •determining satellite integrity •independent data verification •SBAS message broadcast and ranging •system operations & maintenance

As shown in *[Figure 5, The SBAS Concept](#page-12-1)* on *Page 13*, the SBAS is made up of a series of Reference Stations, Master Stations, Ground Uplink Stations and Geostationary Satellites (GEOs). The Reference Stations, which are geographically distributed, pick up GPS satellite data and route it to the Master Stations where wide area corrections are generated. These corrections are sent to the Ground Uplink Stations which up-link them to the GEOs for re-transmission on the GPS L1 frequency. These GEOs transmit signals which carry accuracy and integrity messages, and which also provide additional ranging signals for added availability, continuity and accuracy. These GEO signals are available over a wide area and can be received and processed by NovAtel receivers with appropriate firmware. GPS user receivers are thus able to receive SBAS data in-band and use not only differential corrections, but also integrity, residual errors and ionospheric information for each monitored satellite.

The signal broadcast via the SBAS GEOs to the SBAS users is designed to minimize modifications to standard GPS receivers. As such, the GPS L1 frequency (1575.42 MHz) is used, together with GPStype modulation, for example, a Coarse/Acquisition (C/A) pseudorandom (PRN) code. In addition, the code phase timing is maintained close to GPS time to provide a ranging capability.

 Figure 5: The SBAS Concept

Integrity data, differential corrections and ranging control

3.1 SBAS Receiver

Many models of the NovAtel receivers are equipped with an SBAS option. The ability to simultaneously track two SBAS satellites, and incorporate the SBAS corrections into the position, is available in some models.

These models can output the SBAS data in log format, and can incorporate these corrections to generate differential-quality position solutions. Standard SBAS data messages are analyzed based on RTCA standard DO-229B Change 1 Minimum Operational Performance Standards for GPS/WAAS airborne equipment. Please refer to your *SUPERSTAR II Firmware Reference Manual* or *Volume 2* of the *OEM4 Manual* set for details on SBAS commands and logs.

An SBAS-capable receiver permits anyone within the area of coverage to take advantage of its benefits.

Chapter 4 L-Band Positioning

The transmission of OmniSTAR or CDGPS corrections are from geostationary satellites. The L-Band frequency of geostationary satellites is sufficiently close to that of GPS that a common, single antenna, like the NovAtel GPS-600-LB, may be used.

Both systems are portable and capable of sub-meter accuracy over their coverage areas.

The OmniSTAR system is designed for worldwide coverage. A subscription charge by geographic area is required. The CDGPS system is a free Canada-wide DGPS service that is accessible coast-tocoast, beyond the U.S. border, and into the Arctic.

4.1 Coverage

The two systems provide different coverage areas:

- Worldwide OmniSTAR
- • Canada/America-Wide CDGPS

4.1.1 Worldwide OmniSTAR

In most world areas, a single satellite is used by OmniSTAR to provide coverage over an entire continent - or at least very large geographic areas. In North America, a single satellite is used, but it needs three separate beams to cover the continent. The three beams are arranged to cover the East, Central, and Western portions of North America. The same data is broadcast over all three beams, but the user system must select the proper beam frequency. The beams have overlaps of several hundred miles, so the point where the frequency must be changed is not critical.

The North American OmniSTAR Network currently consists of ten permanent base stations in the Continental U.S., plus one in Mexico. These eleven stations track all GPS satellites above 5 degrees elevation and compute corrections every 600 milliseconds. The corrections are sent to the OmniSTAR Network Control Center (NCC) in Houston via wire networks. At the NCC these messages are checked, compressed, and formed into packets for transmission up to the OmniSTAR satellite transponder. This occurs approximately every few seconds. A packet will contain the latest corrections from each of the North American base stations.

All of the eastern Canadian Provinces, the Caribbean Islands, Central America (south of Mexico), and South America is covered by a single satellite (AM-Sat). A single subscription is available for all the areas covered by this satellite.

OmniSTAR currently has several high-powered satellites in use around the World. They provide [coverage for most of the World's land areas. Subscriptions are sold by geographic area. Any Regional](http://www.omnistar.com) OmniSTAR service center can sell and activate subscriptions for any area. They may be arranged prior to traveling to a new area, or after arrival. Contact OmniSTAR at www.omnistar.com for further [details.](http://www.omnistar.com)

4.1.2 Canada/America-Wide CDGPS

The CDGPS service utilizes the MSAT-1 and MSAT-2 communications satellites.

In order to enable CDGPS positioning, you must enable L-band tracking to the CDGPS signal. The CDGPS signal is broadcast on 4 different spot beams on the MSAT-1 satellite. Depending on your geographic location, there will be a different frequency for the CDGPS signal as shown in *[Figure 6](#page-14-1)*.

 Figure 6: CDGPS Frequency Beams

The following are the spot beam names and their frequencies:

The data signal is structured to perform well in difficult, or foliated conditions, so the service is available more consistently and has a high degree of service reliability.

CDGPS features wide area technology, possible spatial integrity with all Government of Canada maps and surveys $\frac{1}{2}$, 24-hour/7 days-a-week built-in network redundancies and an openly published broadcast protocol.

[Figure 7, CDGPS Percentage Coverage Map](#page-15-0) on *Page 16* is a conservative map of the coverage areas that CDGPS guarantee. The coverage may be better in your area.

^{1.} If the coordinates are output using the CSRS datum. Refer to the DATUM command in *Volume 2* of the *OEM4 Manual* set.

In *[Figure 7](#page-15-0)*, 100% coverage means that a correction is received for every visible satellite (at or above 10 degrees). 90% coverage means that a correction is received for 90% of visible satellites. For example, if a user views 10 satellites but has 90% coverage then there are no corrections available for one of the satellites. In that case, our firmware shows that a correction is missing for that SV and excludes it from the position calculation.

4.2 L-Band Service Levels

Two levels of service are available:

4.2.1 Standard Service

The OmniSTAR VBS service uses multiple GPS base stations in a solution and reduces errors due to the GPS signals traveling through the atmosphere. It uses a wide area DGPS solution (WADGPS) and data from a relatively small number of base stations to provide consistent accuracy over large areas. A unique method of solving for atmospheric delays and weighting of distant base stations achieves submeter capability over the entire coverage area - regardless of your location relative to any base station. This achieves a truly wide-area system with consistent characteristics.

CDGPS is able to simultaneously track two satellites, and incorporate the corrections into the position. The output is SBAS-like (see WAAS32-WAAS45 in *Volume 2* of the *OEM4 Manual* set), and can incorporate these corrections to generate differential-quality position solutions. CDGPS allows anyone within the area of coverage to take advantage of its benefits.

NovAtel's ProPak-LBplus provides GPS with L-Band corrections in one unit, using a common antenna. This means that, with CDGPS or a subscription to the OmniSTAR VBS service, the ProPak-LB*plus* is a high quality receiver with sub-meter capabilities.

The position from the GPSCard in the receiver is used as the L-Band system's first approximation.

After the L-Band processor has taken care of the atmospheric corrections, it then uses its location versus the base station locations, in an inverse distance-weighted least-squares solution. L-Band technology generates corrections optimized for the location. It is this technique that enables the L-Band receiver to operate independently and consistently over the entire coverage area without regard to where it is in relation to the base stations.

4.2.2 High Performance Service

The OmniSTAR High Performance (HP) service gives you more accuracy than the OmniSTAR VBS or CDGPS services. OmniSTAR HP computes corrections in dual-frequency RTK float mode (within about 10 cm accuracy). To obtain OmniSTAR HP corrections, your receiver must have an HP subscription from OmniSTAR.

 Figure 8: OmniSTAR Concept

Reference Description

- 1 GPS satellites
- 2 Multiple L-Band ground stations
- 3 Send GPS corrections to 4
- 4 Network Control Center where data corrections are checked and repackaged for uplink to 5
- 5 L-Band Geostationary Satellite
- 6 L-Band DGPS signal
- 7 Correction data are received and applied real-time
- 8 DGPS uplink

4.3 L-Band Commands and Logs

The ASSIGNLBAND command allows you to set OmniSTAR or CDGPS base station communication parameters. It should include relevant frequencies, for example:

```
assignlband omnistar 1551489 1200
or,
```

```
assignlband cdgps 1547547 4800
```
The PSRDIFFSOURCE command lets you identify from which base station to accept RTCA1, RTCM1, CDGPS or OmniSTAR VBS differential corrections. For example, in the PSRDIFFSOURCE command, OMNISTAR enables OmniSTAR VBS and disables other DGPS types. OmniSTAR VBS produces RTCM-type corrections. CDGPS produces WAAS-type corrections. AUTO means the first received RTCM or RTCA message has preference over an OmniSTAR VBS or CDGPS message.

The RTKSOURCE command lets you identify from which base station to accept RTK (RTCM, RTCA, CMR and OmniSTAR HP) differential corrections. For example, in the RTKSOURCE command, OMNISTAR enables OmniSTAR HP, if allowed, and disables other RTK types. OmniSTAR HP computes corrections in RTK float mode or within about 10 cm accuracy. For RTK models, AUTO means the NovAtel RTK filter is enabled and the first received RTCM, RTCA or CMR message is selected. For non-RTK models, AUTO means the OmniSTAR HP message, if allowed, is enabled.

The PSRDIFFSOURCE and RTKSOURCE commands are useful when the receiver is receiving corrections from multiple base stations.

Several L-Band specific logs also exist and are prefixed by the letters RAWLBAND, LBAND or OMNI. CDGPS corrections are output similarly to SBAS corrections. There are four SBAS fast corrections logs (WAAS32-WAAS35) and one slow corrections log (WAAS45) for CDGPS. The CDGPS PRN is 209.

 \boxtimes In addition to a NovAtel receiver with L-Band capability, a subscription to the OmniSTAR, or use of the free CDGPS, service is required.

Consult *Volume 2* of the *OEM4 Manual* set for more details on individual L-Band commands and logs.

Chapter 5 L5 Overview

The United States plans to implement a third civil GPS frequency $(L5^1)$ at 1176.45 MHz beginning with GPS satellites to be launched in 2005. This frequency is located within the 960-1215 MHz frequency band already used worldwide for Aeronautical Radio Navigation Services (ARNS) as well as by the Department of Defense (DoD). Certain measures have been taken within the United States to ensure that L5 can coexist with government systems operating at the same or nearby frequencies.

The carriers of the L5 signal are modulated by two bit trains in phase quadrature. The L5 signal is contained within a 24 MHz band centered about L5. L5 power is increased by 6 dBW compared to the L1 signal (-154 dBW versus -160 dBW). This is equally split between an in-phase (I) data channel and a quadrature (Q) data-free channel, which improves resistance to interference, especially from pulse emitting systems in the same band as L5. Both I and Q channels are encoded with the Neuman-Hoffman Codes. The L5 signal is also Forward Error Correction (FEC) encoded. Code-Division-Multiple-Access (CDMA) techniques allow differentiating between the SVs since all SVs transmit the same L5 frequency.

The benefits of the L5 signal include:

• Signal redundancy, where the L5 signal is completely redundant to the L1 signal, creates frequency diversity and includes a direct acquisition capability so that you do not have to rely on the L1 and L2 signals for initial acquisition

- User capability to perform ionospheric delay corrections
- Higher integrity level and continuity of service
- Enhanced interference rejection capabilities
- Coherent data-free component allows the receiver to track the carrier at lower signal-to-noise ratios
- Neuman-Hoffman encoding reduces the effect of narrowband interference and improves the cross-correlation properties between SV signals

• FEC encoding permits a receiver to correct errors introduced in the transmission process due to noise or interference and makes it easier to extract the navigation message from weak signals

- 6 dB stronger signal and more robust signal structure than L1
- Greater reliability for safety-of-life applications, interference mitigation worldwide, and position accuracies are provided

^{1.} For further information on the L5 signal, you may wish to refer to: *1. NAVSAT GPS L5 Signal Specification*, Document No. RTCA/DO-261

Chapter 6 Multipath

Multipath signal reception is one of the most plaguing problems that detracts from the accuracy potential of GPS pseudorange differential positioning systems. This section provides a brief look at the problems of multipath reception and some solutions.

Multipath occurs when an RF signal arrives at the receiving antenna from more than one propagation route (multiple propagation paths), see *[Figure 9](#page-20-2)*.

 Figure 9: Illustration of GPS Signal Multipath

6.1 Why Does Multipath Occur?

When the GPS signal is emitted from the satellite antenna, the RF signal propagates away from the antenna in many directions. Because the RF signal is emitted in many directions simultaneously and is traveling different paths, these signals encounter various and differing natural and man-made objects along the various propagation routes. Whenever a change in medium is encountered, the signal is either absorbed, attenuated, refracted, or reflected.

Refraction and reflection cause the signals to change direction of propagation. This change in path directions often results in a convergence of the direct path signal with one or more of the reflected signals. When the receiving antenna is the point of convergence for these multipath signals, the consequences are generally not favorable.

Whenever the signal is refracted, some signal polarity shifting takes place. When full reflection occurs, full polarity reversal results in the propagating wave. The consequences of signal polarity shifting and reversal at the receiving antenna vary from minor to significant. As well, refracted and reflected signals generally sustain some degree of signal amplitude attenuation.

It is generally understood that, in multipath conditions, both the direct and reflected signals are present at the antenna and the multipath signals are lower in amplitude than the direct signal. However, in some situations, the direct signal may be obstructed or greatly attenuated to a level well below that of the received multipath signal. Obstruction of direct path signals is very common in city environments where many tall buildings block the line of sight to the satellites. As buildings generally contain an abundance of metallic materials, GPS signal reflections are abundant (if not overwhelming) in these settings. Obstructions of direct path signals can occur in wilderness settings as well. If the GPS receiver is in a valley with nearby hills, mountains and heavy vegetation, signal obstruction and attenuation are also very common.

6.2 Consequences of Multipath Reception

Because GPS is a radio ranging and positioning system, it is imperative that ground station signal reception from each satellite be of direct line of sight. This is critical to the accuracy of the ranging measurements. Obviously, anything other than direct line of sight reception will skew and bias the range measurements and thus the positioning triangulation (or more correctly, trilateration). Unfortunately, multipath is almost always present to some degree, due to real world conditions.

When a GPS multipath signal converges at the GPS antenna, there are two primary problems that occur:

- 1. a multiple signal with amplitude and phase shifting, and
- 2. a multiple signal with differing ranges.

When a direct signal and multipath signal are intercepted by the GPS antenna, the two signals will sum according to the phase and amplitude of each. This summation of signals causes the composite to vary greatly in amplitude, depending on the degree of phase shift between the direct signal versus the multipath signal. If the multipath signal lags the direct path signal by less than 90° the composite signal will increase in amplitude (relative to the direct signal, depending on the degree of phase shift between 0° and 90°). As well, if the multipath signal lags the direct path signal by greater than 90° but less than 270° the composite signal will decrease in amplitude. Depending on the relative amplitude of the multipath signal (or signals), the composite signal being processed by the receiver correlator may experience substantial amplitude variations. A worst case scenario is when the multipath signal experiences a lag of 180° and is near the same strength as the direct path signal – this will cause the multipath signal to almost completely cancel out the direct path signal, resulting in loss of satellite phase lock or even code lock.

Because a multipath signal travels a greater distance to arrive at the GPS antenna, the two C/A code correlations are, by varying degrees, displaced in time, which in turn causes distortion in the correlation peak and thus ambiguity errors in the pseudorange (and carrier phase, if applicable) measurements.

As mentioned in previous paragraphs, it is possible that the received multipath signal has greater amplitude than the direct path signal. In such a situation the multipath signal becomes the dominant signal and receiver pseudorange errors become significant due to dominant multipath biases and may exceed 150 meters. For single point pseudorange positioning, these occasional levels of error may be tolerable, as the accuracy expectations are at the 1 to 5 meter CEP level (depending on the GPS card model and using a standard correlator). However, for pseudorange single differencing DGPS users, the accuracy expectations are at the one to 0.45 to 1 meter CEP level (depending on the GPS card

model and with no multipath). Obviously, multipath biases now become a major consideration in trying to achieve the best possible pseudorange measurements and position accuracy.

If a differential base station is subject to significant multipath conditions, this in turn will bias the range corrections transmitted to the differential rover receiver. And in turn, if the rover receiver also experiences a high level of multipath, the rover receiver position solutions will be significantly biased by multipath from both stations. Thus, when the best possible position solutions are required, multipath is certainly a phenomenon that requires serious consideration.

6.3 Hardware Solutions For Multipath Reduction

A few options exist by which GPS users may reduce the level of multipath reception. Among these include: antenna site selection, special antenna design, and ground plane options.

6.3.1 Antenna Site Selection

Multipath reception is basically a condition caused by environmental circumstances. Some of these conditions you may have a choice about and some you may not.

Many GPS reception problems can be reduced, to some degree, by careful antenna site selection. Of primary importance is to place the antenna so that unobstructed line-of-sight reception is possible from horizon to horizon and at all bearings and elevation angles from the antenna. This is, of course, the ideal situation, which may not be possible under actual operating conditions.

Try to place the antenna as far as possible from obvious reflective objects, especially reflective objects that are above the antenna's radiation pattern horizon. Close-in reflections will be stronger, and typically have a shorter propagation delay allowing for auto correlation of signals with a propagation delay of less than one C/A code chip (300 meters).

 Figure 10: GPS Signal Multipath vs. Increased Antenna Height

When the antenna is in an environment with obstructions and reflective surfaces in the vicinity, it is advantageous to mount the antenna as high as possible to reduce the obstructions, as well as reception from reflective surfaces, as much as possible. See *[Figure 10, GPS Signal Multipath vs. Increased](#page-22-2) [Antenna Height](#page-22-2)* on *Page 23* for an example.

Water bodies are extremely good reflectors of GPS signals. Because of the short wavelengths at GPS frequencies, even small ponds and water puddles can be a strong source of multipath reception, especially for low angle satellites. Thus, it can be concluded that water bodies such as lakes and oceans are among the most troublesome multipath environments for low angle signal reception. Obviously, water body reflections are a constant problem for ocean going vessels.

6.4 Antenna Designs

Low angle reflections, such as from water bodies, can be reduced by careful selection of the antenna design. For example, flat plate microstrip patch antennas have relatively poor reception properties at low elevation angles near their radiation pattern horizon.

Quadrifilar helix antennas and other similar vertically high profile antennas tend to have high radiation gain patterns at the horizon. These antennas, in general, are more susceptible to the problems resulting from low angle multipath reception. So, for marine vessels, this type of antenna encourages multipath reception. However, the advantages of good low angle reception also means that satellites can be acquired more easily while rising in the horizon. As well, vessels subject to pitch and roll conditions will experience fewer occurrences of satellite loss of lock.

Examples of the above antennas may be seen in *[Figure 11, Illustration of Quadrifilar vs. Microstrip](#page-24-1) [Patch Antennas](#page-24-1)* on *Page 25*.

A good antenna design will also incorporate some form of left hand circular polarization (LHCP) rejection. Multipath signals change polarization during the refraction and reflection process. This means that generally, multipath signals may be LHCP oriented. This property can be used to advantage by GPS antenna designers. If a GPS antenna is well designed for RHCP polarization, then LHCP multipath signals will automatically be attenuated somewhat during the induction into the antenna. To further enhance performance, antennas can be designed to increase the rejection of LHCP signals.

The Model 700 series of GPSAntennas are active antennas designed to operate at the GPS L1 and L2 frequencies, 1575.42 and 1227.60 MHz. The microstrip receiving elements are coupled to filters and a low-noise amplifier (LNA). The units are optimized to receive right-hand-circularly-polarized signals, and their radiation pattern is shaped to reduce signals arriving at low elevation angles. These features decrease the errors associated with electromagnetic interference and multipath. Also, the model 700 gain roll-off compares well to a patch antenna roll-off mounted on a large choke ring ground plane. This antenna provides comparable performance to the choke ring ground plane antenna while being much lighter and smaller.

 Figure 11: Illustration of Quadrifilar vs. Microstrip Patch Antennas

6.5 Antenna Ground Planes

Nearby objects can influence the radiation pattern of an antenna. Thus, one of the roles of the antenna ground plane is to create a stabilizing artificial environment on which the antenna rests and which becomes a part of the antenna structure and its resultant radiation pattern.

A small ground plane (relative to one wavelength at the operating frequency) may have minimal stabilizing effect, whereas a large ground plane (multiple wavelengths in size) will have a highly stabilizing effect.

Large ground planes also exhibit a shielding effect against RF signal reflections originating below the antenna's radiation pattern horizon. This can be a very effective low angle shield when the antenna is elevated on a hill or other structure above other reflecting surfaces such as vehicles, railway tracks, soil with high moisture content, water bodies, etc.

One of the drawbacks of a "flat plate" ground plane is that it gives a "hard boundary condition". This means it allows electromagnetic waves to propagate along the ground plane and diffract strongly from its edge. The "soft boundary" condition, on the other hand, will prevent the wave from propagating along the surface of the ground plane and thereby reducing the edge diffraction effects. As a result the antenna will exhibit a completely different radiation pattern. The "soft boundary" condition is typically achieved by a quarter wavelength deep, transversely corrugated ground plane surface (denoted as "choke ring ground plane"). When the depth of the corrugation (choke rings) is equal to a quarter wavelength, the surface wave vanishes, and the surface impedance becomes infinite and hence provides the "soft boundary" condition for the electromagnetic field. This results in modifications to

the antenna radiation pattern that is characterized by low back lobe levels, no ripples in the main lobe, sharper amplitude, roll-off near the horizon and better phase center stability (there are smaller variations in 2 axes). This is what makes NovAtel's GPS antennas so successful when used with the NovAtel GPSAntenna choke ring ground plane.

6.6 NovAtel's Receiver Solutions for Multipath Reduction

The multipath antenna hardware solutions described in the previous paragraphs are capable of achieving varying degrees of multipath reception reduction. These options, however, require specific conscious efforts on the part of the GPS user. In many situations, especially kinematic, few (if any) of the above solutions may be effective or even possible to incorporate. By far, the best solutions are those which require little or no special efforts in the field on the part of the GPS user. This is what makes NovAtel's internal receiver solutions so desirable and practical.

NovAtel has placed long term concerted effort into the development of internal receiver solutions and techniques that achieve multipath reduction, all of which are transparent to the receiver user. These achievements have led first to Narrow Correlator tracking technology and now PAC technology.

It utilizes innovative patented correlator delay lock loop (DLL) techniques. As it is beyond the scope of this manual to describe in detail how the correlator techniques achieve the various levels of performance, the following paragraphs will provide highlights of the advantages of PAC technology.

6.6.1 Pulse Aperture Correlator Technology (PAC)

NovAtel's OEM4 family of receivers achieve a higher level of pseudorange positioning performance versus standard (wide) or narrow correlator receivers, by virtue of its celebrated PAC technology. By utilizing PAC tracking techniques, the receiver is capable of pseudorange measurement improvements better than 4:1 when compared to standard (wide) correlation techniques and 2:1 when compared to narrow correlation techniques. The PAC technology dramatically reduces multipath reception (approaching a factor of 16 compared to standard correlators and 8 compared to narrow correlators) by virtue of its very narrow correlation function.

[Figure 12, Comparison of Multipath Envelopes](#page-26-1) on *Page 27* illustrates relative multipath-induced tracking errors encountered by the different correlation technologies. As can be seen, standard correlators are susceptible to substantial multipath biases for C/A code chip delays of up to 1.5 chips, with the most significant C/A code multipath bias errors occurring at about 0.25 to 0.75 chips (approaching 80 m error). The Narrow Correlator tracking technology multipath susceptibility peaks at about 0.2 chips (about 10 m error) and remains relatively constant out to 0.95 chips where it rapidly declines to negligible error after 1.1 chips. On the other hand the PAC technology multipath susceptibility peaks at about 0.1 chips (about 5 m error) then reduces to a negligible amount at about the 0.2 chip mark.

While positioning in single point mode, the multipath and ranging improvement benefits of a PAC technology receiver versus narrow or standard correlators, are overridden by a multitude of GPS system biases and errors. In either case positioning accuracy will be in the order of 1.8 m (CEP). However the benefits of PAC technology becomes most significant during pseudorange DGPS operation, where the GPS system biases are largely removed.

Receivers operating DGPS with standard correlators typically achieve positioning accuracies in the two to five meter CEP range (low multipath environment and using a choke ring ground plane or

GPS-702 antenna). NovAtel's Narrow Correlator tracking technology receivers are able to achieve accuracies in the order of 0.75m CEP while NovAtel's PAC technology receivers are able to achieve accuracies in the 0.35 to 0.5 m CEP. PAC technology achieves this higher accuracy through a combination of low noise ranging measurements combined with a very narrow correlation window that dramatically reduces the effects of multipath interference and distortion.

Multipath Delay (C/A code-chip)

6.6.2 Summary

Any localized propagation delays or multipath signal reception cause biases to the GPS ranging measurements that cannot be differenced by traditional DGPS single or double differencing techniques. Multipath is recognized as the greatest source of errors encountered by a system operating in single-point or differential mode. It has been discussed that careful site selection and the GPSAntenna Model 700, or good antenna design combined with a choke ring ground plane, are fairly effective means of reducing multipath reception.

Internal receiver solutions for multipath elimination are achieved through various types of correlation techniques, where the "standard correlator" is the reference by which all other techniques can be compared.

PAC technology has a four fold advantage over standard correlators: improved ranging measurements due to a sharper, less noisy correlation peak, and reduced susceptibility to multipath due to rejection of C/A code delays of greater than 1.0 chip. When used with a choke ring ground plane, PAC technology provides substantial performance gains over standard or narrow correlator receivers operating in differential mode.

Chapter 7 TTFF and Satellite Acquisition

Time to First Fix, or TTFF, is the time it takes the receiver to calculate a position after a reset or upon power-up. The TTFF varies and depends on what is stored in non-volatile memory (NVM) at the time of power-up, and on what other information is available.

The speed at which the receiver locates and locks onto new satellites is improved if the receiver has approximate time and position, as well as an almanac. This allows the receiver to compute the elevation of each satellite so it can tell which satellites are visible and their Doppler offsets, improving TTFF.

Without this information, the receiver must blindly search through all possible satellite PRN codes and Doppler offsets (as in a cold start).

Re-acquisition is the resumption of tracking and measurement processing.

7.1 OEM4-based Products

Once satellites are acquired, the receiver will normally waits another 18-36 seconds before receiving broadcast ephemeris data to calculate a position. To avoid this delay, the receiver saves ephemeris data in its NVM and will use that data if it is less than 2 hours old.

Mode	Information Available to the Receiver				
	Approx. Position	Approx. Time	Almanac	Recent Ephemeris	Typical TTFF
Cold Start	no	no	no	no	50 s
Warm Start	yes	yes	yes	no	40 s
Hot Start	yes	yes	yes	yes	30 _s

 Table 1: Typical Receiver TTFF for OEM4-Based Products

 \boxtimes The TTFF numbers quoted assume an open environment. Poor satellite visibility or frequent signal blockage increases TTFF.

Upon power-up, the receiver does not know its position or time, and therefore, cannot use almanac information to aid satellite acquisition. You can set an approximate GPS time using the SETAPPROXTIME command or RTCAEPHEM message. The RTCAEPHEM message contains GPS week and seconds and the receiver will use that GPS time if the time is not yet known. Several logs provide base station coordinates and the receiver will use them as an approximate position allowing it to compute satellite visibility. Alternately, you can set an approximate position by using the SETAPPROXPOS command.

Approximate time and position must be used in conjunction with a current almanac to aid satellite acquisition. For a summary of the OEM4 family command and logs used to inject an approximated time or position into the receiver, see *[Table 2](#page-28-1)*.

Approximate	Command	Loq
Time	SETAPPROXTIME	RTCAEPHEM
Position	SETAPPROXPOS	RTCAREF or CMRREF or RTCM3

 Table 2: Approximate Time and Position Methods

Base station aiding can help in these environments. A set of ephemerides can be injected into a rover station by broadcasting the RTCAEPHEM message from a base station. This is also useful in environments where there is frequent loss of lock (GPS ephemeris is three frames long within a sequence of five frames. Each frame requires 6 seconds of continuous lock to collect the ephemeris data. This gives a minimum of 18 s and a maximum of 36 s continuous lock time.) or, when no recent ephemerides (new or stored) are available.

7.2 SUPERSTAR II-based Products

The receiver enters Navigation mode, refer to the *Operational States* section of the *SUPERSTAR II User Manual*, and provides valid outputs in less than 45 seconds after completion of the self-test and the following initialization criteria have been met:

- 1. Valid time $(\pm 10 \text{ minutes})$ and position data $(\pm 100 \text{ km})$ from actual position
- 2. Valid almanac data (less than a year old)
- 3. At least 4 satellites greater than 5° elevation above the horizon
- 4. $HDOP < 6$

The time allowed for self-test and device initialization is less than 5 seconds.

In the case where the following additional conditions are met, the TTFF is reduced to 15 seconds:

- Unit has not been off for more than a week before nominal power is re-applied
- Last navigation fix occurred within the last 2 hours
- Valid ephemeris data (less than 4 hours old) for at least 5 satellites

With no initialization, the time from power application to valid navigation output is typically 2 minutes.

There is no disruption of navigation data output when a satellite signal is lost unless there is a power interruption for a period of less than or equal to 200 ms. Also, the receiver re-acquires the satellite signal within 0.3 seconds after satellite visibility has been restored.

When a satellite signal is lost due to signal masking, the signal is typically re-acquired within 2-3 seconds after the satellite signal meets the minimum input levels. The vehicle dynamics during the masking period are assumed to be less than or equal to 0.5 g acceleration and 100 m/s velocity.

When total signal masking occurs, navigation resumes within 3-5 seconds of a Navigation mode criteria being met.

The receiver is capable of acquiring satellite signals with a minimum input carrier-to-noise density ratio (C/N0) to the correlator of 34 dB-Hz. Once a signal has been acquired, the receiver is capable of tracking satellite signals with a minimum input carrier-to-noise density ratio (C/N0) to the correlator of 31 dB-Hz.

 \boxtimes Website addresses are subject to change however they are accurate at the time of posting.

NOVATEL INC.

Contact your local NovAtel dealer first for more information. To locate a dealer in your area or if the problem is not resolved, contact NovAtel Inc. directly.

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Phone :1-800-NOVATEL (U.S. & Canada), or 403-295-4900Fax: 403-295-4901

[E-mail:](mailto:support@novatel.ca) support@novatel.ca Website:<http://www.novatel.com>

RTCM STANDARDS REFERENCE

For detailed specifications of RTCM, refer to RTCM SC104 Recommended Standards for Differential GNSS (Global Navigation Satellite Systems) Service, Version 2.3

Radio Technical Commission For Maritime Services 1800 North Kent St., Suite 1600 Arlington, VA 22209, USA Phone: +1-703-527-2000 Fax: +1-703-351-9932

RTCA STANDARDS REFERENCE

For copies of the Minimum Aviation System Performance Standards DGNSS Instrument Approach System: Special Category-1 (SCAT-1), contact:

RTCA, Inc. 1828 L Street, NW Suite 805 Washington, DC 20036

Phone: 202-833-9339 Fax: 202-833-9434

E-Mail: info@rtca.org Website: http://www.rtca.org

GPS SPS SIGNAL SPECIFICATION REFERENCE

For copies of the Interface Control Document (ICD)-GPS-200, contact:

ARINC Research Corporation 2551 Riva Road Annapolis, MD 21401-7465

Phone: 800-633-6882 Fax: 410-573-3300

Website: http://www.arinc.com

NMEA REFERENCE

National Marine Electronics Association, 0183 Standard for Interfacing Marine Electronic Devices

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Chapter 9 Unit Conversion

Sections [9.1](#page-32-1) to *[9.4](#page-32-4)* list commonly used equivalents between the SI (Système Internationale) units of weights and measures used in the metric system, and those used in the imperial system. A complete list of hexadecimal values with their binary equivalents is given in *Section [9.5](#page-33-0)* while an example of the conversion from GPS time of week to calendar day is shown in *Section [9.6](#page-34-0)*.

9.1 Distance

- 1 meter (m) = 100 centimeters (cm) = 1000 millimeters (mm)
- 1 kilometer (km) $= 1000$ meters (m)
- 1 nautical mile $= 1852$ m
- 1 international foot $= 0.3048$ m
- 1 statute mile = 1609.344 m
- 1 US survey foot = 0.3048006096 m
- 1 inch = 25.4 mm

9.2 Volume

1 liter (1) = 1000 cubic centimeters (cc)

- 1 gallon (Imperial) $=$ 4.546 liters
- 1 gallon $(US) = 3.785$ liters

9.3 Temperature

degrees Celsius = (5/9) x [(degrees Fahrenheit) - 32] degrees Fahrenheit = $[(9/5) \times (degrees Celsius)] + 32$

9.4 Weight

- 1 kilogram (kg) $= 1000$ grams
- 1 pound $= 0.4536$ kilogram (kg)

9.5 Hexadecimal, Binary and Decimal Equivalents

a.These binary to decimal equivalents only go up to decimal 100 for the purpose of example. Please use a calculator for other conversions.

9.6 GPS Time Conversions

The following sections provided examples for converting to and from GPS time.

9.6.1 GPS Time of Week To Day of Week with Time of Day

The value given for GPS Time of Week represents the number of seconds into the week. Therefore, to determine the day and time from that value, calculations are performed to break down the number of seconds into day, hour, minute, and second values.

For example, starting with a GPS Time of Week of *511200 seconds*, the calculations are done as follows:

Therefore, 511200 seconds represents *day 5 (Thursday) + 22 hours, 0 minutes, 0 seconds into Friday*.

9.6.2 Calendar Date to GPS Time

Converting a calendar date to GPS Time is calculated as shown in the example below, using the calendar date *13:30 hours, January 28, 2005*.

The resulting value for GPS Time is *Week 1307, 480,600 seconds*.

Chapter 10 Electrostatic Discharge Control (ESD) Practices

10.1 Overview

Static electricity is electrical charge stored in an electromagnetic field or on an insulating body. This charge can flow as soon as a low-impedance path to ground is established. Static-sensitive units can be permanently damaged by static discharge potentials of as little as 40 volts. Charges carried by the human body, which can be thousands of times higher than this 40 V threshold, can accumulate through as simple a mechanism as walking across non-conducting floor coverings such as carpet or tile. These charges may be stored on clothing, especially when the ambient air is dry, through friction between the body and/or various clothing layers. Synthetic materials accumulate higher charges than natural fibers. Electrostatic voltage levels on insulators may be very high, in the order of thousands of volts.

Various electrical and electronic components are vulnerable to electrostatic discharge (ESD). These include discrete components, hybrid devices, integrated circuits (ICs), and printed circuit boards (PCBs) assembled with these devices.

10.2 Handling ESD-Sensitive Devices

ESD-sensitive devices must only be handled in static-controlled locations. Some recommendations for such handling practices follow:

- • Handling areas must be equipped with a grounded table, floor mats, and wrist strap.
- A relative humidity level must be maintained between 20% and 80% non-condensing.
- No ESD-sensitive board or component should be removed from its protective package, except in a static-controlled location.
- A static-controlled environment and correct static-control procedures are required at both repair stations and maintenance areas.
- ESD-sensitive devices must be handled only after personnel have grounded themselves via wrist straps and mats.
- Boards or components should never come in contact with clothing, because normal grounding cannot dissipate static charges on fabrics.
- A circuit board must be placed into an anti-static plastic clamshell before being removed from the work location and must remain in the clamshell until it arrives at a staticcontrolled repair/test center.
- Circuit boards must not be changed or moved needlessly. Handles may be provided on circuit boards for use in their removal and replacement; care should be taken to avoid contact with the connectors and components.
- On-site repair of ESD-sensitive equipment should not be undertaken except to restore service in an emergency where spare boards are not available. Under these circumstances repair station techniques must be observed. Under normal circumstances a faulty or suspect circuit board must be sent to a repair center having complete facilities, or to the manufacturer for exchange or repair.
- Where protective measures have not been installed, a suitable alternative would be the use of a Portable Field Service Grounding Kit (for example, 3M Kit #8501 or #8507). This consists of a portable mat and wrist strap which must be attached to a suitable ground.
- A circuit board in a static-shielding bag or clamshell may be shipped or stored in a cardboard carton, but the carton must not enter a static-controlled area such as a grounded or dissipative bench top or repair zone. Do not place anything else inside the bag (for example, repair tags).
- • Treat all PCBs and components as ESD sensitive. Assume that you will damage the PCB or component if you are not ESD conscious.
- Do not use torn or punctured static-shielding bags. A wire tag protruding through the bag could act as a "lightning rod", funneling the entire charge into the components inside the bag.
- Do not allow chargeable plastics, such as binders, within 0.6 m of unshielded PCBs.
- Do not allow a PCB to come within 0.3 m of a computer monitor.

10.3 Prime Static Accumulators

[Table 3](#page-36-1) provides some background information on static-accumulating materials.

Work Surfaces	formica (waxed or highly resistive) finished wood synthetic mats writing materials, note pads, etc.	
Floors	wax-finished vinyl	
Clothes	common cleanroom smocks personal garments (all textiles) non-conductive shoes	
Chairs	finished wood vinyl fiberglass	
Packing and handling	common polyethylene bags, wraps, envelopes, and bubble pack pack foam common plastic trays and tote boxes	
Assembly, cleaning, and repair areas	spray cleaners common solder sucker common soldering irons common solvent brushes (synthetic bristles) cleaning, drying and temperature chambers	

 Table 3: Static-Accumulating Materials

10.4 Handling Printed Circuit Boards

ESD damage to unprotected sensitive devices may occur at any time. ESD events can occur far below the threshold of human sensitivity. Follow this sequence when it becomes necessary to install or remove a circuit board:

- 1. After you are connected to the grounded wrist strap, remove the circuit board from the frame and place it on a static-controlled surface (grounded floor or table mat).
- 2. Remove the replacement circuit board from the static-shielding bag or clamshell and insert it into the equipment.
- 3. Place the original board into the shielding bag or clamshell and seal it with a label.
- 4. Do not put repair tags inside the shielding bag or clamshell.
- 5. Disconnect the wrist strap.

Chapter 11 Acronyms

Chapter 12 Glossary

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