SSD Parvex SAS

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DIGIVEX *µmicro* **Drive**

DIGITAL SERVOAMPLIFIER

User and commissioning manual

PVD 3547 GB – 01/2004

PRODUCT RANGE

 \Rightarrow MULTIPLE-AXIS DMM

• ADJUSTMENT AND PROGRAMMING SOFTWARE PARVEX MOTION EXPLORER

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Characteristics and dimensions subject to change without notice.

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SAFETY

Servodrives present two main types of hazard :

- **Electrical hazard**

Servoamplifiers may contain non-insulated live AC or DC components. Users are advised to guard against access to live parts before installing the equipment.

Even after the electrical panel is de-energized, voltages may be present for more than a minute, until the power capacitors have had time to discharge.

Specific features of the installation need to be studied to prevent any accidental contact with live components :

- Connector lug protection ;
- Correctly fitted protection and earthing features ;
- Workplace insulation

(enclosure insulation humidity, etc.).

General recommendations :

- Check the bonding circuit;
- Lock the electrical cabinets;
- Use standardised equipment.

- Mechanical hazard

Servomotors can accelerate in milliseconds. Moving parts must be screened off to prevent operators coming into contact with them. The working procedure must allow the operator to keep well clear of the danger area.

All assembly and commissioning work must be done by **qualified** personnel who are familiar with the safety regulations (e.g. VDE 0105 or accreditation C18510).

Upon delivery

All servoamplifiers are thoroughly inspected during manufacture and tested at length before shipment.

- Unpack the servoamplifier carefully and check it is in good condition.
- Also check that data on the manufacturer's plate complies with the data on the order acknowledgement.

If equipment has been damaged during transport, the addressee must file a complaint with the carrier by recorded delivery mail within 24 hours.

Caution:

The packaging may contain essential documents or accessories, in particular :

- User Manual,
- Connectors.

Storage

Until installed, the servoamplifier must be stored in a dry place safe from sudden temperature changes so condensation cannot form.

Special instructions for setting up the equipment

1. GENERAL

1.1 Digital Servodrive

These drives comprise:

- Sinusoidal emf, permanent magnet brushless servomotors, with resolvers for position measurement (NX, LX range servomotors).
- A box-type electronic control system including:
- A power supply function that receives 230 V single-phase mains input.
- A servomotor control function (power and resolver) which is used to control axis motors.
- This module also controls energy regeneration through internal resistance.

Two connection arrangements are proposed for servomotors:

- Terminal box + resolver connector.
- • Power connector + resolver connector.

1.2 General characteristics

Input voltage: 230 V (see § 4.4.1)

1.3 Operating principle

1.3.1 Block diagram

This block diagram features two parts:

- A power supply section providing dc voltage to the power bridge and auxiliary power supplies (regulation, fans).
- A drive control and monitoring management section.
- •

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1.3.2 Power supply function

• Receives the 230 V single-phase mains supply through the terminal block B3, converts it into a 310 V dc voltage and generates the auxiliary supplies (± 5V) required for regulation.

1.3.3 Servomotor control function

1.3.3.1 Presentation

The DIGIVEX μ^{micro} Drive, D_PD, servoamplifier is a four-quadrant transistor control module for controlling (brushless) synchronous motors with resolvers.

Customization of the motor - drive unit and the setting of the servo-controlled parameters are carried out using a PC with Parvex Motion Explorer software under Windows.

These parameters are stored in an EEPROM permanent memory.

1.3.3.2 Functionalities, block diagram

The diagram shows the main drive functions and setting parameters.

• On the right of the diagram is the motor - resolver - power unit. Parameters can be set for:

- \Rightarrow motor selection, which dictates drive rating.
- \Rightarrow general resolver characteristics

The selection of the motor - drive combination automatically determines some parameters, current limitation, $I^2 = f(t)$ protection, standard servocontrol parameters.

- Ahead of current control.
	- ♦ Second order filter for reducing the effects of high frequency resonance
	- ♦ External reduction of current limitation
- Resolver digital processing (non-parametric) and the encoder emulation function (number of points adjustable from 16 to 16384).
- Regulation type selection: torque or speed.
- Speed loop unit, where the following parameters can be set:
	- \Rightarrow maximum speed for the application (limited by the maximum motor speed).
	- \Rightarrow scaling (1 V = N rpm).
	- \Rightarrow corrector type selection proportional, proportional and integral, proportional and double integration.
- Predictive action related to speed control

These actions, outside the speed loop, directly affect the torque set point. As they are outside, they have little effect on loop stability. Conversely, they allow anticipated action, without waiting for speed loop reaction.

These predictive actions (or predictors) are:

- Gravity: compensation for vertical masses.
- Dry friction: a given friction value is set, the corresponding torque set point is applied, its sign being that of the speed set point.
- Viscous friction: compensation for friction values proportional to speed (hydraulic or electrical system drive).
- Acceleration: changes in the speed set point (drift) are monitored and action is taken directly on the torque set point via a coefficient K, the inertia image.
- Analog input speed reference (13 bits + sign), non-parametric.
- On the left of the block diagram, all logic and analog inputs / outputs.

The parameter setting software is used for:

- - assigning certain functions to these inputs/outputs.
- - forcing them to a logic status. The inputs are then disconnected from the outside.

1.3.3.3 Logic input forcing

The software is used to force a logic input to a value, thus the N=0, TORQUE inputs can be:

- • - "disconnected" from the physical input.
- • - forced using the software to 0 or 1.

1.3.3.4 Stimuli / oscilloscope functions

Certain functions integrated in the drive can be used to excite the speed set point: dc voltage, square (response to scale), sine.

These stimuli are activated using a PC. The result, stored in the drive memory, can be displayed on the PC screen by using the oscilloscope function (a maximum of 4 variables can be simultaneously displayed by using the DIGIVEX *µmicro* Drive Module PME software).

1.3.3.5 Speed ramp function

A ramp function is integrated into the drive unit for versions of software above AP516V07, running with PME version 4.04 or above. This function is used to create time dependent linear speed ramps. Parameters can be set in "Servo-control settings" under the "ramp" tab:

- Times t1, t2, t3, and t4 can be programmed from 0 to 1000s.
- Speeds Vp and Vn can be programmed from 0 to 50,000 rpm.

Comment:

Vp and Vn are points on the ramp; they can be defined outside of maximum motor speed. However, servo-controls will limit the motor speed to the maximum authorized speed.

How the ramp operates:

The ramp input can either be the analog input instruction or the stimuli generator as shown below:

In the event that the input is analog, scaling is carried out by the input instruction product (V) * speed range for 1V, the speed range for 1 volt can be found in the servo-control dialogue box.

Ramp activation is validated by the information "TORQUE=1" (enable torque activated). Therefore, the ramp operates as soon as the zero torque information is unlocked and an operating direction (CW or CCW) selected. When CW or CCW is deactivated, the motor decelerates **in accordance with the pre-set ramp** which means that CW or CCW cannot be selected as mechanical stops.

Important remarks:

- **When "TORQUE" is successively deactivated and reactivated, the speed is reduced to zero prior to following the progression of the ramp.**

- **The ramp function must be deactivated when a DLD with digital control is used to carry out a check on the axis position.**

1.3.3.6 Logic output

• Speed detection

OUT logic output status complies with the table below:

NB: 19 rpm ≤ limit (OUT) ≤ 100,000 rpm

1.3.3.7 Monitoring reasons for stoppage

This monitoring can result in a number of current-related faults such as a stoppage or a reduction in performance via strategy selection.

Variables monitored:

- Mean drive current.
- Output current (short circuit).
- Dissipater temperature.
- Ambient temperature.
- Overspeed.
- No resolver.
- Maximum and minimum dc bus voltages.

1.3.3.8 DIGIVEX *µmicro* **Drive general technical characteristics**

1.4 Compliance with standards

The CE mark of this product is shown on the descriptive label affixed to the equipment.

The DIGIVEX μ^{micro} Drive products have the CE marking under the European Directive 89/336/EEC as amended by Directive 93/68/EEC on electromagnetic compatibility as well as under the Electrical Safety Directive or Low Voltage Directive 73/23/EEC amended by Directive no.93/68/EEC.

The European Directive concerning electromagnetic compatibility refers to the harmonised generic standards EN 50081-2 of December 1993 (Electromagnetic Compatibility – Generic Standard for Emissions – Industrial Environments) and EN 50082-2 of June 1995 (Electromagnetic Compatibility – Generic Standard for Immunity – Industrial Environments). These two harmonised generic standards are based on the following standards:

- EN 55011 of July 1991: Radiated and conducted emissions.
- ENV 50140 of August 1993 and ENV 50204: Immunity to radiated electromagnetic fields.
- EN 61000-4-8 of February 1994: Mains frequency magnetic fields.
- EN 61000-4-2 of June 1995: Electrostatic discharge.
- ENV 50141 of August 1993: Interference induced in cables.
- EN 61000-4-4 of June 1995: Rapid transient.

The Low Voltage Directive groups all the electrical safety standards together including the EN 60204-1 Standard which covers electrical fittings on industrial machinery.

Compliance with the reference standards above implies observance of the wiring instructions and diagrams provided in this technical documentation which accompanies all equipment.

The DIGIVEX μ^{micro} Drive complies with the CEI 1800-3 product standard ("electric power drives with variable speed") with the addition of an overvoltage protection device between phase – neutral, phase – earth, neutral – earth on the power inputs in compliance with the CEI 1004-5 standard

Incorporation in a machine

The design of this equipment allows it to be used in a machine subject to Directive 98/37/CE of 22/06/98 (Machinery Directive), provided that its integration (or incorporation and/or assembly) is done in accordance with trade practices by the machine manufacturer and in accordance with the instructions in this booklet

2. ENERGY DISSIPATION

The energy a module has to dissipate is broken down into:

- Energy generated by braking.
- • Energy from rectifier and power bridge losses

2.1 Braking energy dissipation

2.1.1 Calculating the power to be dissipated in the braking resistor

The permanent and pulse power levels given in the table below are limited by the characteristics of the "braking" resistors.

The mean power to be dissipated must be calculated for each axis when the application includes intensive cycles or long-duration decelerations.

P in Watts =
$$
\frac{J}{2} \left(\frac{N}{9.55} \right)^2 .f
$$

J: Moment of inertia of the servomotor and the related load in kgm².

N: Angular speed of the motor shaft at the start of braking in rpm.

f: Repeat frequency of braking cycles in $s⁻¹$.

This formula is for the least favourable case. For a mechanism with substantial friction or with low reverse output, the power to be dissipated can be greatly reduced.

2.1.2 Braking energy dissipation

Braking energy is dissipated through a resistor fitted in the module.

2.1.3 Braking capacity and module losses.

Definitions

Maximum current: maximum power drawn, resistance connecting is carried out at *365V*; hence, the power drawn has a maximum resistance value equal to *380*.

Pulse power: maximum power dissipated by the resistor, this power can only be drawn for a short time and in compliance with a certain cycle.

Permanent power (to 25°C): mean power that can be dissipated on a permanent basis by the resistor.

Maximum duration: maximum duration, in seconds, for which the pulse power can be required (starting from cold); the resistor must be allowed to cool down before braking again.

Module losses: losses specific to the module, the value shown in the table is that obtained when the module is used at maximum power.

Low-level consumption: consumption of the low-level power supplies in Watts.

2.2 DµD paralleling

The breaking capacity of applications requiring the use of several DuD, placed in the same electrical control cabinet, can be increased (1) (2). It is only a question of linking the DC buses from all the DµD using the B4 connector provided for this purpose. The operation quite simply comprises of combining the braking capacities of all the appliances.

- (1) If cycle simultaneity does not exist between the axes:
- There is no synchronization between the braking axes
- (2) It is possible to use the axes' synchronism according to the following cycles: Braking of one axis whilst another axis is accelerating.

(the braking energy is used to accelerate the other axis).

Connections:

Connections are carried out from DC+ to DC+, DC- to DC-.

Maximum number of parallel axes: 6.

Connecting copper cables section: 1 mm² minimum (cable reference: UL 1015 AWG16)

Maximum length of connection: 300mm of connecting cable (connection to be kept as short as possible).

Every axis must remain connected to the electric mains supply (it is absolutely forbidden to connect 1 axis to the mains and then use the DC bus link as a power supply for the axes connected via this connection).

Follow the electrical connection plans on pages 25 and 26, especially with regard to all axis and line fuses.

The axes linked together by the DC buses must be connected to the same electric mains supply.

A clear 10mm must be spaced between each axis.

Plan of dimensions: see page 19

Electrical connection plans: see pages 25 and 26.

2.3 Associating DµD with DLD

It is possible to parallel DµD axes with DLD axes. The constraints are the same as those described in section 2.2.

3. DIMENSIONS, ASSEMBLY, MASS, LABELLING, CODES

3.1 Dimensions, assembly and mass

See following pages, drawings

- FELX 306714GB

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3.2 Labelling, codes

Physical identification is made using labels:

- On the DµD :
	- ∗ A descriptive label is affixed to the equipment in accordance with the model below:

Codes

4. ELECTRICAL CONNECTIONS

4.1 General Wiring Requirements

4.1.1 Appliance handling

Please refer to the safety instructions given at the beginning of this booklet. It is strongly recommended that personnel wait for the 7-segment display, situated on the front panel, to go off before undertaking any intervention of the servoamplifier or servomotor.

4.1.2 Electromagnetic compatibility

EARTHING

- Comply with all local safety regulations concerning earthing.
- Use a metal surface as an earth reference plane (e.g. control cabinet wall or assembly grid). This conducting surface is termed the TRP, potential reference plate. All the equipment of an electrical drive system is connected up to this TRP by a low impedance (or short distance) link. Ensure the connections provide good electrical conduction by scraping off any surface paint and using fan washers. The drive will therefore be earthed via a low impedance link between the TRP and the earth screw at the back of the DIGIVEX μ^{micro} Drive. If this link exceeds 30cm, a flat braid should be used instead of a conventional lead.

CONNECTIONS

- Do not run low-level cables (resolver, inputs outputs, NC or PC links) alongside what are termed power cables (power supply or motor). Do not run the power supply cable and the motor cables alongside one another otherwise mains filter attenuation will be lost. These cables should be spaced at least 10cm apart and should never cross, or only at rightangles.
- Except for the resolver signals, all low-level signals will be shielded with the shielding $\overline{}$ connected at both ends. At the DIGIVEX $\overline{}$ $\overline{}$ Drive end, the shielding is made continuous by the Sub-D plug mechanism.
- The motor cables are limited to the minimum functional length. The yellow and green motor cable must be connected to the box or front panel terminal block with the shortest possible link.
- This usually means shielded motor cable is not required. Chokes can also be inserted into the motor phase leads.

OTHER MEASURES

Self-inducting components must be protected against interference: brakes, contactor or relay coils, fans, electro-magnets etc.

4.1.3 DIGIVEX *µmicro* **Drive Sub-D plugs**

It is essential, in order to ensure the system is free from interference, for the DµD to be properly connected to the earth plane of the electrical control cabinet and for the covers of the Sub-D plugs to be EMI/RFI shielded (metal with shielding braid connection). Make sure the Sub-D plugs and their covers are properly connected (lock screws fully tight).

The shielding is connected to the inside of the Sub-D covers in the following manner:

GROUND CONNECTION

4.2 Standard connection diagram

See the following pages for drawings:

FELX 306715 FELX 306721

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4.3 Description of terminal blocks and Sub-D plugs

All the Inputs/Outputs required for operating are arranged on the front panel; they include:

- B2 motor terminal.
- B3 power supply + auxiliary power terminal.
- B4 DC Bus terminal
- X1 RESOLVER connector.
- X5 INPUTS/OUTPUTS + encoder emulation connector
- X4 RS232 connector.

Viewed from above Viewed from below

4.3.1 Terminal blocks B2, B3, B4

4.3.2 Sub-D X1, X5 and RJ9-X4 plugs

4.3.2.1 Sub-D and RJ9 plug table

Plugs with metal-plated or metallic covers.

4.3.2.2 Sub-D X1 plug: "Resolver"

DIGIVEX end connections, Sub-D 9-pin plug item ref. X1 Maximum conductor cross-section: 0.5 mm²

4.3.2.3 Sub-D X5 plug: INPUTS / OUTPUTS and encoder emulation

EA = analog input, **EL =** logic input, **SA =** analog output, **SL =** logic output

Sub-D X5 plug: INPUTS / OUTPUTS and encoder emulation (cont.)

EA = analog input, **EL =** logic input, **SA =** analog output, **SL =** logic output

4.3.2.4 RJ9 connector - X4: "RS232"

- Serial link configuration:
	- \triangleleft 9600 bauds
	- ♦ 8 data bits
	- ♦ 1 start bit, 1 stop bit
	- ♦ No parity
	- ♦ No galvanic insulation

This input is for linking with a computer (PC) for parameter loading and setting via the DIGIVEX *µmicro* Drive Module PME software.

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4.4 Connection Details

4.4.1 Mains supply characteristics

230 V single-phase modules

* To guarantee mechanical power

NB: power supplies required for regulation (±5 V, fans) are taken from the power bus internal dc voltage.

4.4.2 Power component dimensions

Applicable to the components ahead of the DµD (fuses, cables, contactors, etc.), the dimensions are based on:

- the permanent current \hat{I}_0 (sine curve peak) at the motor's slow speed, such as is given in the characteristics.
- Efficient mains power \approx 1.1 eff. U \hat{I}_0
- Eff.I power source = $\frac{\text{eff.mainsP}}{\text{eff}.\text{U}\sqrt{3}} \times \frac{1}{0.65}$ in single-phase
- Eff.I power source = $\frac{\text{eff.mainsP}}{\text{eff}.\text{U}\sqrt{3}} \times \frac{1}{0.65}$ in single-phase

• **4.4.3 R Earth connection to the chassis**

Chassis earth:

The cable cross-section must usually be identical to that of the mains connection in order to comply with standards in force.

4.4.4 Short circuit capacity

The DµD is suitable for use with power supply circuits capable of delivering not more than 5000 rms symmetrical amperes.

(UL 508 C)

4.4.5 Connection terminals for cable with brake

Two terminals, B2/B5 and B2/6, are accessible on the motor phase connection terminal in order to simplify the cabling. These terminals are used for connecting:

- on the one hand, a +24 V DC power supply, holding brake power supply.
- on the other hand, the connection leads for the holding brake for the motor cable fitted with these two leads.

Data conveyed to terminals B2/5 and B2/6 is not used for monitoring or for DµD protection.

The brake cable shielding must be connected at both ends:

- motor connector end
- terminal B2/4 drive connector end

4.5 Servomotor connection

4.5.1 Power cable definition

Caution!!! Only use copper core cables

The power/drive connector cables must have as a minimum requirement:

- 3 x insulated conductors connected to U, V, W phases. Cross-sections as in the table below.
- 1 x earth conductor (green/yellow).
- 2 x shielded twisted pairs for connection of the holding brake (if fitted). Cross-section of about 1mm².

Power cable cross-section

Cable cross-sections shown in the table below make allowance for:

- rated drive current.
- Motor drive distance, loss in operating voltage = RI.
- ambient temperature, cable loss of Joules = $RI²$.
- standardized increase of cable cross-sections.

The cable cross-section to be used is shown in the table below:

Guidelines for long cables

- DSF01: box of three resistor controlled coils to be fitted on DIN rail placed between the DµD and the motor.
- Keep the default value (8kHz + PWM mode 1) in the window Servo-control settings / PME Hardware
- Please contact us for information on cables longer than 50 m.

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4.5.2 Motor end connection

Power connection

Connection possibilities available:

- Heavy-duty socket or output cable power connector (IP 67) for NX1, NX2 and NX3 servomotors.
- MOLEX power connector (IP 40) for NX1 and NX2 servomotors.
- •

4.5.2.1 Heavy-duty socket power connector (IP 67) for NX3

Cable and plug references

View of plug 220065R1610

F View

Permissible cable cross-section for plugs

Plug 220065R1610: Power & earth: 0.14 - 1.5 mm². Brake and thermal sensor: 0.14 - 1 mm²

Do not link the "Brake and "Thermal protection" pair shielding to the motor end. It should be linked to the earth terminal at the drive end.

4.5.2.2 Heavy-duty output cable power connector (IP 67) for NX1 and NX2

Cable and plug references

View of plug 220065R1610

F View

Permissible cable cross-section for plugs

Plug 220065R1610: Power and earth: 0.14 - 1.5 mm². Brake & thermal sensor: 0.14 - 1 mm²

Link the "Brake" and "Thermal protection" pair shielding to the metal cover of the connector at the motor end. It should be linked to the earth terminal at the drive end.

4.5.2.3 MOLEX power connector (IP 40) for NX1 and NX2

Cable and connector references

View of MOLEX connector

F View

4.5.2.4 Holding brake connection

Brushless motors can be fitted with a specially sized brake to hold the axis immobilized. If 24V+/-10% dc voltage is applied across the brake terminals, the brake disc is released and the motor can rotate.

The 24V dc supply used for brake control must be regulated and filtered.

4.5.2.5 Thermal protection connection

The two thermal sensor terminals are not used in the DIGIVEX µ*micro* Drive.

4.5.2.6 Direction of motor rotation

If the wiring instructions have been followed correctly, a positive speed set point applied to the drive will result in clockwise rotation when viewed from the power shaft end.

4.5.3 Resolver connection

The resolver is a high-precision sensor, and, therefore must be wired carefully:

- separate power cable routing.
- cable made up of three pairs; each pair twisted and shielded individually (no general shielding). The shielding must be linked to the metal Sub-D plug cover.

PARVEX can supply this cable in one of two ways:

- Cable fitted with a Sub-D plug at the drive end and a connector at the motor end:
- Heavy-duty resolver connector (IP 67)
- MOLEX resolver connector (IP 40)
- We **strongly recommend** this ready-to-use cable.
- •
- Separate cable; in this case please follow the cabling instructions in the drawings below.

• Maximum distance between resolver and DIGIVEX μ^{micro} Drive: 50m. (Please contact us for information on longer cables).

Maximum cross-sections for Sub-D plugs: 0.5 mm².

4.5.3.1 Heavy-duty resolver connector (IP 67)

NX1, NX2 NX3, NX4, NX6

Cable and plug references

View of resolver connector removable plug (ref.: 220065R4621)

F View

Maximum permissible cross-sections for connector removable plug: 0.14 - 1 mm² (solder-fit contacts).

The shielding must not be linked to the motor end.

4.5.3.2 MOLEX resolver connector (IP 40) for NX1 and NX2

Cable and connector references

View of MOLEX connector

F View

Maximum permissible cross-sections for connector removable plug: **0.35** mm² (solder-fit or crimpfit contacts) for all wires and **1.34** mm² for the shielding (B)

Link the shielding to the MOLEX connector B terminal.

4.5.4 Input/Output cable

Please refer to section 4.3 for the functions and characteristics and the FELX 306711 drawing

4.5.5 RS232 serial link cable (PC – Drive)

Please refer to section 4.4 for the functions and characteristics and the FELX 306729 drawing

5. AUTOMATIC CONTROL INPUT / OUTPUT FUNCTIONS AND CHARACTERISTICS

5.1 Input / Output Characteristics

5.1.1 Logic inputs

- 24 V dc optocoupled inputs (100 V isolation voltage)
- type 1 inputs under European standard CEI 1131-2
- these inputs can be connected directly to PNP type outputs (no external load resistor required)
- •
- •

5.1.2 Logic outputs

The outputs are fed by an external 24 V (24 V terminal 13 and 0 V terminal 25). The two 0 V outputs are linked to terminal 25.

- Maximum authorized output current (level 1) \blacksquare : 50 mA
- Residual current (level 0) in the set of the
- Response time : 1 ms
- Voltage drop : 2 V
- •

Opto-isolated output, the load being for connection to the 0 V logic (i.e.: between the two contacts allocated to this output).

5.1.3 Speed set point input

5.1.4 Current limitation input

5.1.5 Analog output

5.1.6 Encoder emulation

Electrical characteristics

The electrical output interface meets standard RS 422 for differential serial links. The circuit used is an MC26C31 "LINE DRIVER". The electrical characteristics are, therefore, closely related to the use of this component.

Short-circuit capability

A single output can be short-circuited at 0 V at any given time

Signal form

Signal levels:

U high $≥$ 2.5 V for I high $≥$ -20mA

Switching time:

Rise or fall time defined from 10% to 90% of the magnitude in question, without cable and without load.

 $tr = tf = 4$ ns (typical value)

Time delay between direct and complemented channels

Time delay defined at 50% of magnitudes in question without cable and without load.

 -6 ns \leq ta \leq 6ns (maximum)

Time delay between channels A, B and the zero mark 0

Time delay defined at 50% of magnitudes in question without cable and without load.

 -6 ns \leq td \leq 6ns (maximum)

Encoder emulation

The resolver is above all a position sensor. It is used to measure the position of the rotor relative to the stator.

This function allows the transformation of the signal from the resolver into a series of pulses identical to those from an incremental encoder: A, B, 0 and their complement.

Programming resolution and the zero mark position

This is done using PME software.

Resolution

Adjustable between 16 and 16384, either by +/- keys, or by entering the number directly (off-line only).

Zero mark setting

Setting by teaching with the PC working "on-line".

When the operator judges the position is suitable, he/she confirms by acknowledging the zero mark.

5.2 RESET and DRV OK output

A 24 V status applied to X5/5 relative to X5/17 induces the reset after a drive fault.

It is worth noting that the reset can also be carried out by turning the power supply to the drive off completely.

This control has no effect during normal operating conditions. The system must be "reset" after any active fault.

- This logic output is at 1 when the drive is operating correctly (motor operational).
- This logic output is at 0 when the drive shows an operating fault or when the drive power supply voltage is below the minimum operating voltage (140 V dc).
- This logic output shifts from 1 to 0 in the following cases:
	- on drive fault
	- on normal stoppage, obtained by turning the power supply to the drive off.
- This logic output shifts from 0 to 1 in the following cases:
	- when the drive is powered-up
	- when the reset control is used, if the cause of the drive fault is no longer present.

5.3 Initialization Sequence

After the power supply has built up:

 τ To τ mains supply present T_0 \rightarrow Motor operational \rightarrow Motor operational

5.4 Stop sequence

5.4.1 Normal stoppage

Normal stoppage is achieved by deliberately opening the main contactor.

5.4.2 Stoppage due to a fault

6. SERVOCONTROL PARAMETER FUNCTION AND SETTING

6.1 Servocontrol Parameter Functions

6.1.1 List of parameters

Regulation selection:

- Speed Proportional: P
	- ⇒ Proportional and integral: PI
	- \Rightarrow Proportional and double integral: Pl²
- Current regulation

- Filtering frequency 20 Hz 800 Hz
-
- Current limitation 0 A 1 pulse drive

For speed regulation (P, PI, PI²)

- Maximum speed 100 rpm 100,000 rpm
-
- Proportional gain I pulse drive/156 I pulse drive x 210
- Integration stop 0.1 Hz 100 Hz

• Speed for 1V 10 rpm 14,150 rpm

Minimum value Maximum value

0ffset - 3.4% V max. + 3.4% V max.

• **6.1.2 Regulation selection: current, proportional, PI, PI²**

Current regulation

Selecting "current" means current can be controlled directly (therefore, the motor torque through the torque coefficient Kt). This then gives 10 V = pulse peak current of the drive selected beforehand.

In this mode, the PI/PI² settings and predictors are neutralized. The only functions operative are:

- Current limitation (often reduced below the permanent drive current, so as not to trip in mean or rms values.
- The second order low pass filter (filtering frequency) for reducing the effect of any resonance.
- •

Selecting P

The drive is used in a speed loop with purely proportional gain. This gain is the ratio between the output current and the speed error. It is expressed in mA / rpm.

For the same current I, if the gain increases, the error ε is reduced, the rapidity of the system increases as does its bandwidth.

An increase in gain can lead to instability because of the other components in the loop (resonances, second order filter).

The use of proportional action P alone has the drawback of giving zero rigidity because there is no integration ahead of the current section.

Selecting PI (proportional and integral action)

Compared with P action alone, PI provides the following two modifications:

- The gain (open loop) at zero frequency is infinite. If there is a torque surge, there will be an angular discrepancy of the motor shaft in relation to idle status. This angle will be proportional to the applied torque and there will not be any permanent speed drift. The system can be said to be "rigid". This rigidity is strictly proportional to the integration stop frequency.
- The proportional gain P sets the bandwidth f_0 (system rapidity). The integral action entails a -90° phase shift which creates instability. This phase shift is not troublesome at low frequencies, but it can make the system unstable at higher frequencies. It is therefore best to adjust the "integral stop frequency" correctly (0.2 - 0.3 times the bandwidth f_0).

Selecting PI² action (proportional and double integration action)

Compared with P action alone, PI² provides the following two modifications:

- Rigidity when stopped is infinite. When motor torque surges, and after a transient period, the motor shaft returns to the position it was in for idle status (there is no longer any permanent position discrepancy).
- The double integral action entails a -180° phase shift at low frequencies. Poor adjustment of the integral stop frequency can entail instability in the system. Settings should be restricted to 0.1 or 0.2 times the bandwidth f_0 .
- •

6.1.3 Integration stoppage

Please refer to the previous paragraph for the function of this parameter. Its definition according to the Bode graphs (gain/frequency and phase/frequency) is given below

6.1.4 Speed scaling

The motor - drive unit selection determines the maximum possible speed.

The "Maximum" speed parameter can be used to reduce this maximum speed for the application. This parameter is external to the speed loop, and modifying it does not modify gain.

The "Speed for 1 volt" parameter determines the speed "gradient" (e.g. maximum speed can be obtained for 10 V, 9 V or 7 V, depending on the position control).

6.1.5 Filtering frequency

Resonance phenomenon

Many systems have one or more resonance frequencies related most of the time to mechanical phenomena: inertia or mass, associated with the rigidity of the mechanical components (belts, screws, reducing gear, frames, etc.).

In a zone of reduced frequency around the resonance frequency there occurs:

- Marked variations in loop gain.
- Marked variations in the closed loop phase.

This leads to instabilities or "squeaking", with more or less violent oscillation.

Second order filter

This phenomenon cannot be dealt with by P/PI/PI² adjustment. If the resonance cannot be dealt with mechanically, the frequencies concerned must be eliminated. This is the function of the second order low pass filter.

6.1.6 Predictors

Purpose of predictors

Four physical phenomena:

- Vertical mass.
- Dry friction
- Friction proportional to speed.
- Acceleration.

are direct and calculable causes of modification of motor torque.

The purpose of predictors is, by calculation, to act directly on the current set point, without recourse to the speed loop and without waiting for the speed error produced by these phenomena (see block diagram).

The principle of predictor setting and work is to minimize the current set point part from the P, PI, PI² branch and therefore to reduce the speed error.

These predictors do not affect stability as they are outside the speed loop which must be adjusted first. They provide an appreciable improvement on response time.

The acceleration predictor improves stability and allows gain to be increased in any position loop superimposed on the speed loop.

However, it should be noticed that many speed servocontrols do not require the use of these predictors.

General characteristics of each predictor

• Mass or gravity compensation (vertical axis)

The current value, in amps, required by the motor to move the mass at constant speed (average between the up and the down) is introduced directly into the parameter.

• Dry or "static" friction

The friction force is fixed, whatever the speed. Its direction is opposed to motion; the sign therefore depends on the speed set point sign.

In this case too, the values are entered directly in amps, for the required motor current to overcome friction.

The "threshold" expressed in rpm defines a speed "band" within which this compensation is zero.

The threshold is of the order of $1/1000th$ of maximum speed. This zone allows torque oscillation to be reduced during rapid and repeated changes of the speed sign. This is the case, in particular, at stoppage when there is a position loop.

• "Dynamic" friction compensation

Friction proportional to speed, encountered on some mechanical components using fluids.

Value to enter: coefficient in amps / rpm

• Acceleration prediction

Depending on the total inertia (load and motor rotor) and on the desired acceleration, the torque necessary is equal to: $C = \Sigma J \cdot d\omega / dt$.

The set point is monitored therefore in order to send a set point that is proportional to inertia (fixed) and to acceleration to the current control. This is one of the limits of the system; there is no point in having a variation in the speed set point that is greater than the maximum possible acceleration of the motor, given by d_ω /dt = peak torque / Σ J. Acceleration prediction is only useful if there is a ramp on the speed reference.

The parameter used is t_{pr} , prediction time, in milliseconds; t_{pr} can vary between:

- 0 ms (no prediction).
- \bullet t = td, start-up time from 0 to maximum speed with full drive current. There is then 100% correction.
- •

6.2 Entering parameters

Customization parameters for the motor - drive unit are entered on start-up using a PC with the PME software under WINDOWS.

Transfer of this customization to a drive with a different rating leads to the generation of a fault. The parameters contained in the EEPROM are saved.

6.3 Parameter setting via DIGIVEX *µmicro* **Drive Module PME software**

6.3.1 Outline

6.3.2 Internal variables

Internal variables accessible via DIGIVEX *µmicro* **Drive Module PME software** The following internal variables can be selected:

Reference

- ♦ 11 Phase current U in amps: iu-measure
- ♦ 12 Phase current W in amps: iw-measure
- Access via the name of the variable, this is valid for the 11 above plus the following variables:
- Temperature in °C: heatsink-temperature-measure
- Bus voltage in Volts: ubus-measure
- Active I in amps: id-output
- Reactive I in amps: ig-output
- Id current in amps: id-measure
- Iq current in amps: iq-measure
- Ud voltage in volts: ud-command
- Uq voltage in volts: uq command
- Auxiliary input in volts: auxiliary-input
- Position filtered in degrees: position-filtered-measure
- Speed filtered: speed-filtered-measure
- Drive thermal load in %; thermic-drive-load
- Motor thermal load in %: thermic-motor-load
- Recovery thermal load in %: thermic-break-load

It should be noted that these variables can be assigned to the analog output which means that a separate oscilloscope can be used.

The "ibus-measure", "ibus-filtered-measure" and "power-bus-measure" variables cannot be accessed using the DµD drive.

6.3.3 Entering parameters via DIGIVEX *µmicro* **Drive Module PME software**

Please refer to the DIGIVEX μ^{micro} Drive Module PME software instructions:

- Selecting rating
- Selecting motor (standard or special)
- Selecting resolver
- Entering servocontrol parameters (global transfer)
- Assigning inputs/outputs and variables
- Using the oscilloscope function
- Using the stimuli function

6.3.4 Setting loop parameters for speed regulation

This can be done by using the "Setting Assistant" menu or directly with the stimuli and oscilloscope.

Speed for 1 V and maximum speed

The maximum possible speed is set when the motor - drive selection is made. Here, it can only be reduced.

To control the result:

- Select a "dc" stimulus of say 1 volt.
- Check the value obtained for the "measure speed in rpm" variable using the variable watcher or oscilloscope functions.

Proportional gain adjustment

Initial status

- Switch to proportional gain P alone.
- Filtering frequency fc to maximum (800 Hz) and low gain.
- System ready to run, no predictor.

Proportional gain and filter frequency are adjusted simultaneously. If, by increasing proportional gain, the system starts to resonate, the resonance must be eliminated by reducing the filter frequency, then increasing P etc. until a compromise is found.

Maximum recommended for P

There is a maximum recommended proportional gain, depending on the drive rating, and corresponding to maximum current oscillation.

NB: This gain can be exceeded under certain circumstances. Please ask for details.

Generate a speed set point scale (0.5 to 1V).

Use the oscilloscope function to display

- Channel $1 \Rightarrow$ the input set point.
- Channel $2 \Rightarrow$ the speed measurement.
- Trigger on channel 1 at 5 or 10% of N max, leading edge.

Increase proportional gain

The stimulus is excited on-line. The response is collected at one scale of speed set point.

Dipl43gb.D/W

A response must be obtained without overshooting and oscillation. For example, increase gain until oscillations gradually appear; then, reduce it by 20 to 30%.

If the maximum value shown in the table is reached with proportional gain, without reducing the filtering frequency, then:

- Stop increasing P
- Reduce the filtering frequency until the limit of oscillation

Filtering frequency setting

Oscillations can appear on the response obtained above (even when speed is increasing).

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This gives a frequency resonance (probably of mechanical origin) of $fr = 1/T$, greater than 100Hz.

Then reduce the filtering frequency until the oscillation disappears almost completely. If that cannot be done, the maximum gain is reached.

If it is possible, gain can be increased again until a response is obtained without oscillation. Oscillation can reappear, in which case, reduce the filtering frequency a little more.

Notice that it is essentially P and the filtering frequency that determine the bandwidth.

If the resonance frequency is too low, adjust the filter frequency to a high value.

PI / PI² - integral stop frequency setting

Initial status

- P gain alone. P and filtering frequency setting completed.
- Integration stop frequency = 0.
- Still no integration.
- System ready to run.
	- ◆ Select PI or PI².
	- ♦ Use the same stimuli as before (index analysis).
	- ♦ "On-line", increase the integration stop frequency until overshoot is obtained in the order of:

 $v_T v_U 25 - 30\%$ in PI $v_{\tau}N_{\mu}$ 15 - 20% in Pl²

Without oscillation.

If the frequency is too high, fairly low frequency oscillations occur (< 50Hz). Frequency must then be reduced (never readjust the proportional gain).

Do not change PI to PI² without setting the integral frequency to 0.

6.3.5 Setting predictors

Initial conditions

- All loop parameters (P, integral and filtering frequency, maximum speed, current limitation) are set (without predictors).
- The system is ready to run.

Setting the Gravity and Static Friction predictors

Notice that the gravity factor is zero for a horizontal axis.

- Take a square stimulus, offset = 0, peak-to-peak value = 3 to 5% of maximum speed in rpm, frequency 0.2 to 1Hz.
- Using the oscilloscope function, display:
	- ♦ The input set point
	- ♦ The current set point

NB: I+ and I- are to be taken with their sign. In general, I- is negative.

In principle:

- Gravity = $\frac{I_+ + I}{2}$ 2 $+\frac{+1}{2}$ in amps (horizontal motion, gravity = 0).
- Static friction = $\frac{I_+ I}{I_-}$ 2 $+\frac{-I_{-}}{2}$ in amps.
- Enter these values into the parameters.
- Enter the threshold value (e.g. threshold = maximum speed $/$ 1000).
- After introducing the values, the result obtained can be checked with the same stimuli.
- Check the input set point on one channel and the P, PI, PI² output on the other channel. This should give a result close to:
- •

Setting the dynamic friction and acceleration predictors. (It is assumed that the dry friction and gravity predictors have been set).

- Use a sine stimulus, offset 0 peak-to-peak value 10 to 20% of the maximum speed, frequency 0.2 to 1Hz.
- Using the oscilloscope function, display:
	- ♦ The input set point on one channel.
	- ♦ P, PI, PI² output on the other channel.
- Acceleration predictor setting. Increase the predictor until the P , PI , $PI²$ output is minimized. Too high a value increases P, PI, PI² with a phase change.
- •

Très forte différence entre réglage optimum et pas de prédicteur.

Very marked difference between optimum setting and no predictor.

The correct setting corresponds to minimum amplitude P, PI, PI² output. The predictor must allow the P, PI, PI² output to be reduced in a ratio of at least 5 to 10.

Remember that the value of t_{pr} (prediction time in ms) is close to td (start-up time), with:

$$
td = \frac{(\text{Load inertia} + \text{Motor inertia}) \cdot \omega \text{ max}}{\text{Maximum torque}}
$$

td is the acceleration time from 0 to maximum speed with maximum torque td in seconds, inertia in kgm², maximum ω in rd/s, torque in Nm,

• Setting the dynamic friction predictor. Once all the other predictors have been adjusted, increase the dynamic predictor to minimize the P, PI, PI² output signal.

When the setting is correct, this output should be minimum and in phase with the input set point.

6.3.6 Setting current regulation parameters

If the "current" option has been selected, the only adjustments needed are:

- Current limitation; take care in this type of application that it does not trip with mean or rms current monitoring. Current limitation is often equal to permanent current.
- Second order filter frequency. This can only be done with the "superior" regulation loop giving the current set point.

6.3.7 Other characterization parameters

Logic and analog inputs / outputs

Access via:

I/O, servocontrol parameter adjustment function.

This means that it is possible to:

- assign one of the internal variables to the 5 V analog output.
- assign a constant value (between -5 V and +5 V) to the analog output
- force the logic inputs to 0 or 1.

The logic inputs / outputs are assigned permanently.

Encoder emulation

- Selection of the number of marks between 16 and 16384 per revolution *(*off-line)*.*
- Validation by teaching of zero mark position (on-line).

Miscellaneous choices

• Selection of processing strategy for mean or rms current monitoring: current reduction or switching to "DRV OK".

7. COMMISSIONING - SERVOCONTROL PARAMETER SETTING - DETECTING REASONS FOR STOPPAGE

7.1 Commissioning sequence

7.1.1 Preliminary checks

Wiring check

- Power connections.
- Reset wiring to terminal X5
- Check the resolver connections.
	- ♦ Motor end
	- ♦ DµD end
- Check the power and brake connections.
	- ♦ Motor end
	- ♦ DµD end

Power supply type check

• Power: 50/60Hz, 230 V single-phase.

Caution: Make sure that the power bus is at 0 V before doing any work on the system. After total stoppage of the motors, wait for at least three minutes before starting work. **Wait for the 7 segment display to go off.**

7.1.2 Commissioning with the DIGIVEX *µmicro* **Drive Module PME software**

- Connect the PC via the RS232 serial link
- Energize the DµD
- Go "on-line" via the PC, with the PC in interactive mode. Connect with the parameter setting functions. If this connection is not carried out:
	- \bullet Check the compatibility of the serial link configuration (PORT, BAUD RATE, etc.)
	- \triangleleft Check the serial link cable.
	- ♦ Check that you are using the correct interface (PC, DµD).

Once "on-line", all the parameters in the DIGIVEX *µmicro* Drive can be read.

- Check the TORQUE input status. $N = 0$
- Then configure the drive. This can be done "off-line" in a file and then transferred or modified "on-line".
	- ♦ Motor selection.
	- ♦ Servocontrol parameter selection (without the power part, their validity cannot be checked).
	- ♦ Ancillary selections: analog output, safety strategy, etc.
- Use the software to force the drive to zero torque.
- Remove "zero torque" locking using the software or via hardware contact (set "TORQUE" input to 24 V)
- Carry out system adjustment using the stimuli function.
	- \bullet "dc" stimuli (square with peak-to-peak = 0). Check maximum N.
	- ♦ "Square" stimuli or setting procedure for adjusting servocontrol parameters.
	- ♦ DIGIVEX *µmicro* Drive Module PME software for setting the predictors if necessary.

Check the driven mechanism can operate freely.

7.2 Detecting reasons for stoppage

7.2.1 Fault display - Drive function

Incidents with the drive operation can be displayed in two ways.

- On the 7-segment display situated **on the front panel of the drive**
- Via the PME software which indicates in uncoded language the nature of the problem and gives advice on corrective action.

7.2.1.1 Handling operational malfunctions

There are two types of malfunction:

• Malfunctions requiring a stoppage of the system

As a result of these malfunctions:

- the drive shifts to zero torque.
- \bullet the fault is displayed on the 7-segment display.
- ◆ the DRV OK output shifts to 0.
- \bullet the fault is stored in the axis.
- Malfunctions leading to a reduction in the system's dynamic characteristics such as:
- •
- ♦ an excessive DµD dissipater temperature.
- ♦ an excessive mean current drive or excessive rms motor current, if the drive parameter setting allows the operation to continue. The selection of continuing the operation with reduced current or stopping is made by selecting the "current protection strategy in the "servocontrol" window of the parameter setting software.

As a result of these malfunctions:

- \bullet the motor current is reduced
- \bullet the front panel displays the data (7-segment display flashes).

7.2.1.2 Current monitoring

RMS motor current

The drive monitors the rms current $[I^2 = f(t)]$ to monitor the thermal status of the motor.

The rms current is compared to the permanent permissible current at slow rotation by the motor \hat{I}_0 (after first order filtering following motor thermal time constant). This data which is characteristic of the motor is known to the drive when the motor - drive selection is made.

As before there is a choice between two strategies:

- ♦ Strategy 1: Stoppage due to the "DRV OK" output shifting to logic 0.
- \bullet Strategy 2: Reduction of the drive pulse current to 0.9 \hat{I}_0 motor. The 7-segment display flashes.

Mean current drive

A monitoring of the mean current, filtered by a time constant of 2.4s, $[I = f(t)]$ is carried out.

The fault is detected when the mean current is equal to or greater than the drive permanent permissible current.

Depending on the strategy adopted, this fault can:

- ♦ Lead the 0 V Drive OK output to shift to 0
- ♦ Reduce the drive current to 90% of the drive permissible current. The parameters for the strategy selection are to be found in the "Servocontrol settings" window.

Drive output current

♦ Excessive output current (I maximum): the drive determines whether or not the measured current exceeds the pulse current by 30%.

There is stoppage due to the "DRV OK" output shifting to logic 0.

7.2.1.3 Temperature monitoring

Temperature measured in the vicinity of the DµD power bridge components

- \bullet If the temperature is less than 75°C at the dissipater, nothing happens.
- ♦ Between 75 and 99°C, there is a reduction in the pulse current which can release the drive (the "7-segment" display flashes at low frequency).
- ◆ At 100°C, the drive stops

Ambient temperature

This is measured between the electronic boards and operations are stopped when it exceeds 70°C.

7.2.1.4 Monitoring the DC Bus voltage

Recovery fault:

Drive electrical breaking capacity needs updating, cycle too restricting.

Bus overvoltage

Drive breaking capacity much too low with regard to the application.

7.2.1.5 Other monitoring

No resolver

Resolver fault or wiring fault.

Overspeed

Speed > 1.15 times the maximum motor - drive setting.

These two cases entail a fault with:

• Data displayed on the 7-segment display

7.2.1.6 7-segment display

•

Function: to provide information on DµD status discriminating between faults. Description:

7.2.1.7 Corrective actions

The following incidents can arise from wiring errors or mishandling:

- Resolver fault
	- ♦ Check the resolver connection.
- Drive overcurrent
	- ♦ Poor motor connection (motor phase missing).
	- ♦ Programmed motor does not correspond with the connected motor.
- Overspeed
	- ♦ Nmax. incorrectly set.
	- ♦ Accidental transition to torque regulation.
- Motor fails to run and remains without torque
	- ♦ System is set to zero torque (hardware or software input TORQUE = 0). In particular, the torque has been forced to zero during a global transfer. Reset system torque (see software manual).
	- ♦ Motor is not connected.
- Motor fails to run but torque present
	- ♦ N=0 input is set to zero (hardware or software). Check with software.

7.3 Fault description

